

**MARTIN MARIETTA**

**NUREG/CR-4360**  
**Volume 2**  
**ORNL/ENG/TM-31/V2**

# **Calculational Methods for Analysis of Postulated UF<sub>6</sub> Releases**

W. R. Williams

Prepared for the  
U.S. Nuclear Regulatory Commission  
Office of Nuclear Regulatory Research  
Division of Risk Analysis  
Transportation and Materials Risk Branch  
under Interagency Agreement DOE 40-550-75

OPERATED BY  
MARTIN MARIETTA ENERGY SYSTEMS, INC.  
FOR THE UNITED STATES  
DEPARTMENT OF ENERGY

### NOTICE

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, or any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for any third party's use, or the results of such use, of any information, apparatus product or process disclosed in this report, or represents that its use by such third party would not infringe privately owned rights.

Available from

Superintendent of Documents  
U.S. Government Printing Office  
Post Office Box 37082  
Washington, D.C. 20013-7982

and

National Technical Information Service  
Springfield, VA 22161

NRC FORM 335 (11 81)		U.S. NUCLEAR REGULATORY COMMISSION <b>BIBLIOGRAPHIC DATA SHEET</b>		1. REPORT NUMBER (Assigned by DDC) NUREG/CR-4360, Vol. 2 ORNL/ENG/TM-31/V2	
4. TITLE AND SUBTITLE (Add Volume No., if appropriate) Calculational Methods for Analysis of Postulated UF <sub>6</sub> Releases				2. (Leave blank)	
7. AUTHOR(S) W. R. Williams				3. RECIPIENT'S ACCESSION NO.	
9. PERFORMING ORGANIZATION NAME AND MAILING ADDRESS (Include Zip Code) Oak Ridge National Laboratory Post Office Box X Oak Ridge, TN 37831				5. DATE REPORT COMPLETED MONTH August   YEAR 1984	
12. SPONSORING ORGANIZATION NAME AND MAILING ADDRESS (Include Zip Code) Division of Risk Analysis and Operations Office of Nuclear Regulatory Research U.S. Nuclear Regulatory Commission Washington, DC 20555				DATE REPORT ISSUED MONTH September   YEAR 1985	
13. TYPE OF REPORT Topical				6. (Leave blank)	
15. SUPPLEMENTARY NOTES				8. (Leave blank)	
16. ABSTRACT (200 words or less) <p>           Calculational methods and computer programs for the analysis of source terms for postulated releases of UF<sub>6</sub> are presented. Required thermophysical properties of UF<sub>6</sub>, HF, and H<sub>2</sub>O are described in detail. UF<sub>6</sub> reacts with moisture in the ambient environment to form HF and H<sub>2</sub>O. The coexistence of HF and H<sub>2</sub>O significantly alters their pure component properties, and HF vapor polymerizes. A release rate model of UF<sub>6</sub> is presented that considers the transient conditions inside containment and the flashing, multiphase flow of UF<sub>6</sub> along the release pathway. Transient compartment models for simulating UF<sub>6</sub> releases inside rooms ventilated by forced- and induced-draft systems are also described. The basic compartment model mass and energy balances are supported by simple heat transfer, ventilation system, and deposition models. A model that can simulate either a closed compartment or a steady-state ventilation system is also discussed. Listings of all main programs (including two plotting routines) and subroutines are included. Example problems illustrate the analysis of postulated releases using the described programs.         </p>				10. PROJECT/TASK/WORK UNIT NO.	
17. KEY WORDS AND DOCUMENT ANALYSIS uranium hexafluoride (UF <sub>6</sub> ) accidents scenarios releases analysis				11. FIN NO. B0495	
17a DESCRIPTORS cylinder cold trap pigtail fuel cycle modeling				13. PERIOD COVERED (Inclusive dates)	
17b IDENTIFIERS: OPEN-ENDED TERMS				14. (Leave blank)	
18 AVAILABILITY STATEMENT unlimited		19 SECURITY CLASS (This report) unclassified		21 NO. OF PAGES 312	
		20 SECURITY CLASS (This page) unclassified		22 PRICE \$ 98.95	



NUREG/CR-4360  
Volume 2  
ORNL/ENG/TM-31/V2  
Dist.Cat.RZ

**Martin Marietta Energy Systems, Inc., Engineering  
Process Engineering**

## **Calculational Methods for Analysis of Postulated UF<sub>6</sub> Releases**

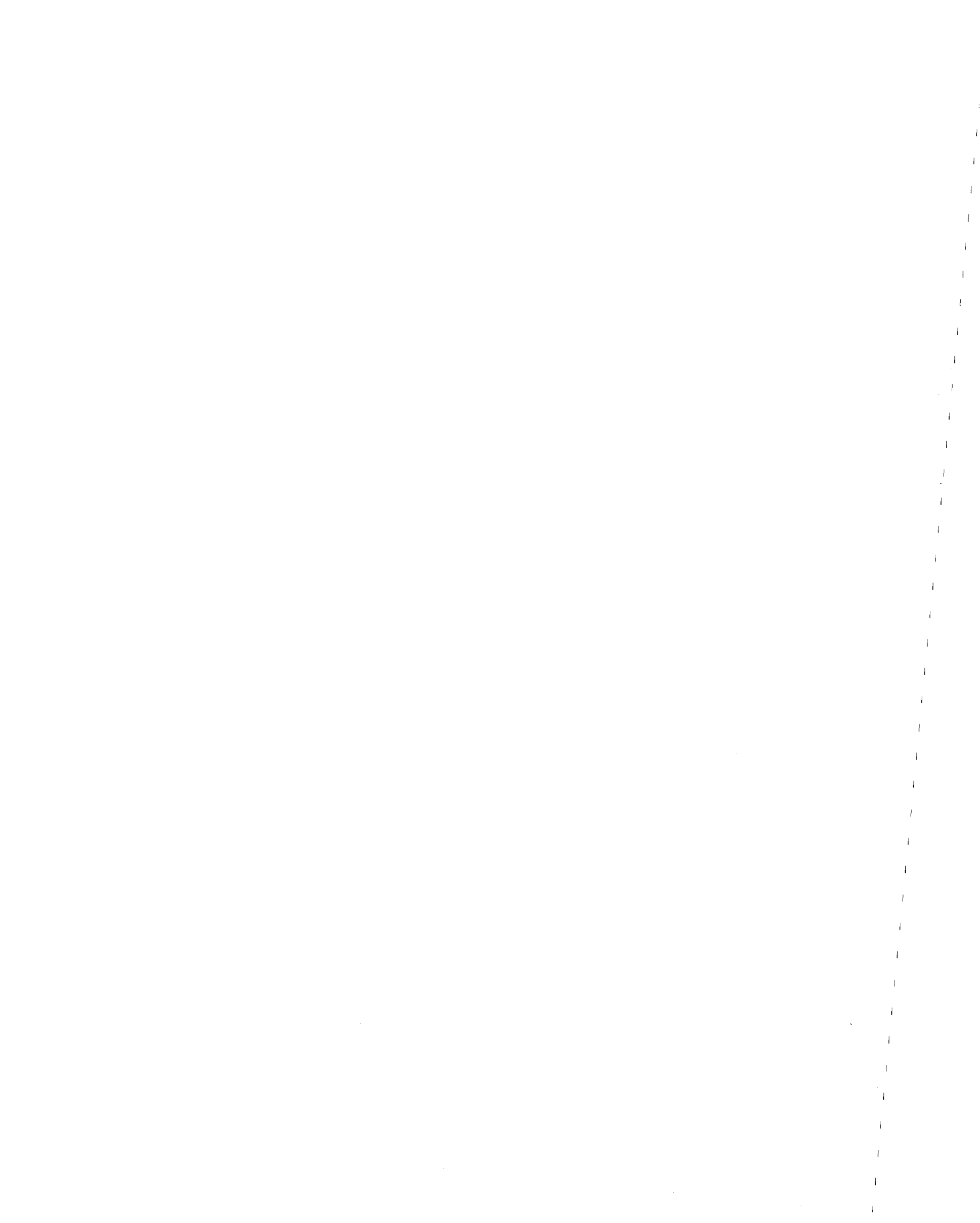
W. R. Williams

Manuscript Completed: August 1984

Date of Issue: September 1985

Prepared for the  
U.S. Nuclear Regulatory Commission  
Office of Nuclear Regulatory Research  
Division of Risk Analysis  
Transportation and Materials Risk Branch  
(T. Clark, Project Manager)  
Washington, DC 20555  
under Interagency Agreement  
DOE 40-550-75  
FIN B0495

Oak Ridge National Laboratory  
P.O. Box X  
Oak Ridge, Tennessee 37831  
operated by  
MARTIN MARIETTA ENERGY SYSTEMS, INC.  
for the  
U.S. DEPARTMENT OF ENERGY  
under Contract No. DE-AC05-84OR21400



# CONTENTS

## Volume 1

Acknowledgement .....	vii
Executive Summary .....	ix
Abstract .....	xi
1. INTRODUCTION AND SUMMARY .....	1
2. PHYSICAL AND THERMODYNAMIC PROPERTIES MODELS .....	3
2.1 Uranium Hexafluoride .....	3
2.1.1 Vapor Pressure .....	4
2.1.2 Equation of State and Vapor Compressibility Factor .....	6
2.1.3 Density .....	6
2.1.4 Viscosity .....	7
2.1.5 Thermal Conductivity .....	9
2.1.6 Heat Capacity .....	11
2.1.7 Enthalpy .....	13
2.1.8 Entropy .....	14
2.1.9 Other Properties .....	16
2.1.10 UF <sub>6</sub> Reaction with H <sub>2</sub> O .....	16
2.1.11 Flashing .....	17
2.1.12 Subroutines .....	19
2.2 HF-H <sub>2</sub> O System .....	20
2.2.1 Self-Association of HF Vapor .....	20
2.2.2 Partial Vapor Pressure of HF .....	23
2.2.3 Partial Vapor Pressure of H <sub>2</sub> O .....	25
2.2.4 Enthalpy of HF-H <sub>2</sub> O Vapor Mixtures .....	29
2.2.5 Enthalpy of HF-H <sub>2</sub> O Liquid Mixtures .....	31
2.2.6 HF-H <sub>2</sub> O Vapor-Liquid Equilibrium .....	31
2.2.7 Subroutines .....	34
2.3 Other Components .....	35
2.4 Mixture Enthalpies .....	35
3. RELEASE RATE MODELS .....	37
3.1 Containment (Cylinder) Subroutines .....	37
3.1.1 Internal Mass and Energy Balance .....	37

3.1.2 Liquid-Vapor Interface Level and Phase Composition of UF <sub>6</sub> Leaving Containment .....	41
3.2 Flow Rate Subroutines .....	45
3.2.1 Flow Through a Ruptured Piping System .....	46
3.2.2 Flow Rates Through a Breach in Containment .....	52
3.3 Main Program for Evaluating Release Rates from a Cylinder .....	53
3.4 Cylinder Model Plotting Program .....	57
<b>4. COMPARTMENT MODELS .....</b>	<b>59</b>
4.1 Main Program Structure .....	62
4.1.1 Initial Statements .....	62
4.1.2 Input Data Requirements .....	67
4.1.3 Steady-State Conditions .....	69
4.1.4 Transient Analysis .....	71
4.1.5 Other Considerations .....	74
4.2 Ventilation System Subroutines .....	74
4.2.1 Steady-State Analysis .....	74
4.2.2 Transient Analysis .....	76
4.2.3 Stream Mixing .....	77
4.3 Source-Term Subroutine .....	78
4.4 Condensate Deposition Subroutine .....	79
4.5 Compartment Mass and Energy Balance Subroutines .....	79
4.5.1 Initial Conditions .....	81
4.5.2 Transient Behavior .....	83
4.6 Compartment Model Main Programs .....	86
4.6.1 Forced-Draft Compartment .....	86
4.6.2 Induced-Draft Compartment .....	89
4.6.3 Closed Compartment/Ventilation System .....	92
4.7 Compartment Model Plotting Program .....	93
<b>5. EXAMPLE PROBLEMS .....</b>	<b>95</b>
5.1 Release from a Cylinder .....	95
5.1.1 Release through a Breach in Containment .....	95
5.1.2 Release through a Ruptured Piping System .....	106
5.2 Release Inside a Compartment .....	112
5.3 Release into a Ventilation System .....	119
<b>REFERENCES .....</b>	<b>123</b>



## Volume 2

Appendix A. LISTINGS OF MAIN PROGRAMS .....	1
A.1 FODRFT - A Forced-Draft Compartment Model .....	4
A.2 INDRFT - An Induced-Draft Compartment Model .....	19
A.3 BATCH - A Closed Compartment/Ventilation System Model .....	36
A.4 CYLIND - A Cylinder Release Model .....	45
A.5 COMPLT - A Plotting Program for FODRFT and INDRFT Results .....	55
A.6 CYLPLT - A Plotting Program for CYLIND Results .....	59
Appendix B. LISTINGS OF SUBROUTINES .....	67
B.1 BREACH .....	68
B.2 COMPRT .....	75
B.3 CPUF6 .....	81
B.4 DENTHL .....	82
B.5 DENUF6 .....	85
B.6 DPFLOW .....	86
B.7 EQTUF6 .....	89
B.8 FLASH .....	91
B.9 HCOEFF .....	97
B.10 HFPOLY .....	98
B.11 HHFH2O .....	100
B.12 HUF6 .....	103
B.13 HUMID .....	104
B.14 INTMEB .....	105
B.15 LEVEL .....	109
B.16 MIXFLW .....	114
B.17 PHASE .....	117
B.18 PHFH2O .....	122
B.19 PIPSYS .....	125
B.20 REMOVE .....	134
B.21 RESIST .....	135
B.22 ROOM .....	137
B.23 SETRAY .....	138
B.24 SSBLOW .....	141
B.25 STERM .....	142
B.26 SUF6 .....	146
B.27 THCUF6 .....	147
B.28 TRBLOW .....	148
B.29 VISUF6 .....	149
B.30 VPRUF6 .....	150
B.31 ZUF6 .....	152

Appendix C. EXAMPLE PROBLEM OUTPUT .....	153
Example 1 .....	154
Case 1 .....	154
Case 2 .....	156
Case 3 .....	159
Case 4 .....	162
Example 2 .....	163
Case 1 .....	163
Case 3 .....	165
Example 3 .....	166
Case 1 .....	166
Case 2 .....	167
Case 3 .....	168
Example 4 .....	169
Case 1 .....	169
Case 2 .....	176
Case 3 .....	183
Case 4 .....	190
Example 5 .....	197

## **Appendix A**

### **LISTINGS OF MAIN PROGRAMS**

This appendix contains listings of the main programs described in Chaps. 3 and 4. These programs include the transient compartment model programs FODRFT (Appendix A.1) and INDRFT (Appendix A.2), the closed compartment/ventilation system model BATCH (Appendix A.3), a program for simulating releases from a cylinder through a breach in containment or a piping system, BYLIND (Appendix A.4), and the plotting programs COMPLT (Appendix A.5) and CYLPLT (Appendix A.6). COMPLT plots output from FODRFT and INDRFT, while CYLPLT plots output from CYLIND.

Table A.1 lists the subroutines required for the execution of each main program, excluding the plotting programs. COMPLT and CYLPLT require the availability of DISSPLA version 9.0\* on the user's system. These subroutines are listed in Appendix B. Table A.2 identifies the input/output device numbers used in each main program.

---

\*For information on DISSPLA, contact Integrated Software Systems Corporation, 10505 Sorrento Valley Road, San Diego, CA, 92121.

Table A.1. Main program subroutine requirements

Subroutines	Main Programs			
	FODRFT	INDRFT	BATCH	CYLIND
BREACH				*
COMPRT	*	*	*	
CPUF6				
DENTHL	*	*	*	
DENUF6	*	*	*	*
DPFLOW	*	*		
EQTUF6	*	*	*	*
FLASH	*	*	*	*
HCOEFF	*	*		
HFPLY	*	*	*	
HHFH2O	*	*	*	
HUF6	*	*	*	*
HUMID	*	*	*	
INTMEB				*
LEVEL				*
MIXFLW			*	
PHASE	*	*	*	
PHFH2O	*	*	*	
PIPSYS				*
REMOVE	*	*		
RESIST	*	*		
ROOM	*	*	*	
SETRAY	*	*	*	
SSBLOW	*	*		
STERM	*	*	*	
SUF6	*	*	*	*
THCUF6				
TRBLOW		*		
VISUF6				*
VPRUF6	*	*	*	*
ZUF6	*	*	*	*

Table A.2. I/O device numbers

Program	Input Files	Output files	
		To others programs	For printing/plotting
FODRFT	40,22 <sup>a</sup>	48 <sup>b</sup> ,49	41,42,43,44,45,46,47 <sup>c</sup>
INDRFT	40,22 <sup>a</sup>	48 <sup>b</sup> ,40	41,42,43,44,45,46,47 <sup>c</sup>
BATCH	5		6
CYLIND	20	22,30,31	30
COMPLT	48 <sup>b</sup> ,49		<i>d</i>
CYLPLT	30,31		<i>d</i>

<sup>a</sup>Input device number 22 is an optional input file to FODRFT and INDRFT.

<sup>b</sup>The file written to device 48 by FODRFT or INDRFT for use by COMPLT is unformatted.

<sup>c</sup>FODRFT and INDRFT output files provide conditions in the compartment (41), inlet flow conditions (42), source term conditions (43), outlet flow conditions (44), deposition rate information (45), condensate accumulation on the floor (46), and release summary (47).

<sup>d</sup>Compressed data files are generated via an initial call to the subroutine COMPRS.

### A.1 FODRFT - A Forced-Draft Compartment Model

C THIS PROGRAM MODELS A RELEASE OF UF6 OR HF INTO A COMPARTMENT  
 C HAVING A FORCED DRAFT VENTILATION SYSTEM. NODE NUMBERS AND  
 C STREAM DEFINITIONS FOR THIS MODEL ARE AS FOLLOWS.

C  
 C 1 COMPARTMENT  
 C 2 INLET AIR BLOWER  
 C 3 SOURCE TERM  
 C 4 FORCED DRAFT EXHAUST  
 C 5 CONDENSATE FALLOUT  
 C 6 COMPARTMENT FLOOR  
 C 7 AMBIENT

C THE FOLLOWING VARIABLES ARE USED.

C COMMON BLOCK VARIABLES

C /LBMASS/

C MASS (30,9) NODE MASS, LB, OR MASS FLOW RATE, LB/(DELT)  
 C RH RELATIVE HUMIDITY, % (AS INPUT) OR FRACTION  
 C (INTERNAL)

C /COMPTP/

C TC (30) NODE TEMPERATURE, DEG F  
 C PC (30) NODE PRESSURE, PSIA  
 C TSURF (30) NODE HEAT TRANSFER SURFACE TEMPERATURE, DEG F

C /MOLWT/

C WMOL (9) COMPONENT MOLECULAR WEIGHTS, LB/LB MOLE

C /VOLUME/

C VOL (30) NODE VOLUME, FT\*\*3  
 C KRCOEF (30) RESISTANCE COEFFICIENT, --, OR RESISTANCE TERM,  
 C RESISTANCE TERM, PSI-SEC\*\*2/LB-FT\*\*3  
 C DPAREA (30) DEPOSITION AREA, FT\*\*2  
 C DEPVEL DEPOSITION VELOCITY, FT/SEC

C /ENTHAL/

C H (30) NODE ENTHALPY, BTU, OR ENTHALPY RATE, BTU/(DELT)  
 C QRATE (30) HEAT TRANSFER RATE, BTU/SEC OR BTU/(DELT)  
 C QCOOL (30) COOLING RATE, BTU/HR (INPUT) OR BTU/SEC  
 C (INTERNAL)  
 C HTCDEF (30) HEAT TRANSFER COEFFICIENT, BTU/SEC-FT\*\*2-DEG F  
 C HTAREA (30) HEAT TRANSFER AREA, FT\*\*2

C /ISTRMS/

C IIN (30,4) INLET STREAM NODE NUMBER

C IOUT (30,4) OUTLET STREAM NODE NUMBER  
 C  
 C /CONTRL/  
 C  
 C AMINLN NATURAL LOG OF MINIMUM NUMBER ACCEPTED BY THE  
 C COMPUTER  
 C TIME CUMULATIVE SIMULATION TIME, SEC  
 C DELT TIME INTERVAL USED FOR TRANSIENT SIMULATION, SEC  
 C MAXTIM MAXIMUM SIMULATION TIME, SEC  
 C IFLAG FLAG TO CONTROL PRINTING OF OUTPUT  
 C TRELS TOTAL RELEASE TIME, SEC  
 C  
 C /POLYMR/  
 C  
 C C1 WEIGHT FRACTION OF HF MONOMER TO TOTAL HF VAPOR  
 C C3 WEIGHT FRACTION OF HF TRIMER TO TOTAL HF VAPOR  
 C C6 WEIGHT FRACTION OF HF HEXAMER TO TOTAL HF VAPOR  
 C WMBHF MOLECULAR WEIGHT OF HF MONOMER, LB/LB MOLE  
 C  
 C /MISCEL/  
 C  
 C ITYPE VARIABLE TO SPECIFY TYPE OF RELEASE, SEE CARD 5  
 C SOURCE TOTAL MASS OF RELEASE, LB  
 C ISEN VARIABLE TO SPECIFY ISENTROPIC OR ISENTHALPIC  
 C RELEASE, SEE CARD 5  
 C  
 C /RVFLOW/  
 C  
 C TSTART (30) START OF REVERSE FLOW (NOT USED)  
 C TSTOP (30) END OF REVERSE FLOW (NOT USED)  
 C  
 C EQUIVALENCED VARIABLES  
 C  
 C VOL ACFM (30) VOLUMETRIC FLOW RATE, FT\*\*3/MIN  
 C FLAREA (30) FLOW AREA FOR PRESSURE-DROP-CONTROLLED  
 C NODE, FT\*\*2  
 C  
 C OTHER DIMENSIONED VARIABLES  
 C  
 C RATE (9) COMPONENT MASS FLOW RATE, LB/SEC  
 C MSOURC (5) INCREMENTAL SOURCE MASS, LB  
 C TSOURC (5) INCREMENTAL RELEASE TIME, SEC  
 C TEMP (5) TEMPERATURE OF INCREMENTAL SOURCE, DEG F  
 C PRES (5) PRESSURE OF INCREMENTAL SOURCE, PSIA  
 C NAME (9) COMPONENT IDENTIFIER  
 C TITLE (10) TITLE ARRAY  
 C DWGNUM (6,4) PLOT NUMBER ARRAY  
 C  
 C UNDIMENSIONED VARIABLES  
 C  
 C INODES MAXIMUM NUMBER OF NODES ALLOWED BY CODING OF  
 C SUBROUTINES  
 C INOUT MAXIMUM NUMBER OF INLET STREAMS AND OUTLET  
 C STREAMS

C IRELST NUMBER OF INCREMENTAL RELEASES IN TOTAL RELEASE  
 C (MAXIMUM OF 5)  
 C MW MOLECULAR WEIGHT, LB/LB MOLE  
 C MWURAN MOLECULAR WEIGHT OF URANIUM, LB/LB MOLE  
 C MRELS TOTAL MASS OF SOURCE MATERIAL RELEASED, LB  
 C PTEST VAPOR PRESSURE OF SOURCE, PSIA  
 C PRINT PRINT INTERVAL, SEC  
 C RATIO RATIO OF MOLES OF WATER VAPOR TO TOTAL MOLES OF  
 C MOIST AIR  
 C UA PRODUCT OF HEAT TRANSFER COEFFICIENT AND AREA,  
 C BTU/SEC-DEG F  
 C ICOUNT COUNTER TO CONTROL PRINTING OF OUTPUT  
 C IRELS CURRENT INCREMENT OF TOTAL RELEASE  
 C DELTAT SOURCE TERM INPUT INTERVAL, SEC  
 C SOLIDS MASS FLOW RATE OF UF6 SOLIDS ONTO THE FLOOR,  
 C LB/(DELT)  
 C IDEV OUTPUT DEVICE  
 C HRATE ENTHALPY RATE, BTU/SEC  
 C DENU COMPARTMENT CONCENTRATION OF URANIUM, LB/FT\*\*3  
 C DENHF COMPARTMENT CONCENTRATION OF HF, LB/FT\*\*3  
 C UF6REL CUMULATIVE MASS OF UF6 RELEASED TO THE  
 C ATMOSPHERE, LB  
 C UOFREL CUMULATIVE MASS OF UO2F2 RELEASED TO THE  
 C ATMOSPHERE, LB  
 C UTOT CUMULATIVE MASS OF URANIUM RELEASED TO THE  
 C ATMOSPHERE, LB  
 C HFREL CUMULATIVE MASS OF HF RELEASED TO THE  
 C ATMOSPHERE, LB  
 C HFUF6 CUMULATIVE MASS OF HF THAT CAN BE FORMED FROM  
 C UF6 RELEASED TO THE ATMOSPHERE, LB  
 C HFTOT CUMULATIVE MASS OF HF RELEASED TO OR FORMED IN  
 C THE ATMOSPHERE, LB

C LOGICAL VARIABLES

C CHECK FLAG IN ESTABLISHING INITIAL STEADY STATE  
 C CONDITIONS ABOUT NODE 2

C THE FOLLOWING SUBROUTINES ARE CALLED BY FODRFT.

C COMPRT  
 C DENTHL  
 C DPFLOW  
 C HCOEFF  
 C HUMID  
 C PHFH2O  
 C REMOVE  
 C RESIST  
 C ROOM  
 C SETRAY  
 C SSBLOW  
 C STERM  
 C VPRUF6



```

C THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED.
C
C          DENUF6
C          EQTUF6
C          FLASH
C          HFPOLY
C          HHFH20
C          HUF6
C          PHASE
C          SUF6
C          ZUF6
C
C*****
C
C INITIAL STATEMENTS
C =====
C
C          IMPLICIT REAL*8 (A-H,J-Z)
C
C          LOGICAL CHECK
C
C          DIMENSION FLAREA(30), ACFM(30), RATE(9), MSOURC(5), TSOURC(5),
*          TEMP(5), PRES(5)
C          DIMENSION NAME(9), TITLE(10), DWGNUM(6,4)
C
C          COMMON /LBMASS/ MASS(30,9), RH
C          COMMON /COMPTP/ TC(30), PC(30), TSURF(30)
C          COMMON /MOLWT/ WMOL(9)
C          COMMON /VOLUME/ VOL(30), KRCOEF(30), DPAREA(30), DEPVEL
C          COMMON /ENTHAL/ H(30), QRATE(30), QCOOL(30), HTCDEF(30),
*          HTAREA(30)
C          COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C          COMMON /CONTRL/ AMINLN, TIME, DELT, MAXTIM, IFLAG, TRELS
C          COMMON /POLYMR/ C1, C3, C6, WMBHF
C          COMMON /MISCEL/ ITYPE, SOURCE, ISEN
C          COMMON /RVFLOW/ TSTART(30), TSTOP(30)
C
C          EQUIVALENCE (VOL(1),ACFM(1),FLAREA(1))
C
C          DATA NAME /8HAIR   U , 8HH20   L , 8HH20   U , 8HHF   L ,
*          8HHF   U , 8HUF6   S , 8HUF6   L , 8HUF6   U , 8HU02F2 S /
C
C          CALL SETRAY(INODES, INOUT)
C
C NODE ASSIGNMENT
C =====
C
C          IIN(1,1) = 2
C          IIN(1,2) = 3
C          IIN(2,1) = 7
C          IIN(4,1) = 1
C          IIN(5,1) = 1
C          IIN(6,1) = 5
C

```

```

IOUT(1,1) = 4
IOUT(1,2) = 5
IOUT(4,1) = 7
IOUT(5,1) = 6

```

```

C
C READ STATEMENTS
C =====
C
C ALL INPUT DATA EXCEPT THAT ON CARDS 1 AND 9 ARE READ IN FREE FORMAT.
C ON CARDS 1 AND 9, COUNT CHARACTERS STARTING IN COLUMN 1.
C
C
C /-----
C /
C/ CARD 1.  READ TITLE (MAXIMUM OF 80 CHARACTERS).
C
C     READ (40,4000) TITLE
C
C /-----
C /
C/ CARD 2.  READ AMBIENT TEMPERATURE (F), PRESSURE (PSIA), AND RELATIVE
C           HUMIDITY (%).
C
C     READ (40,*) TC(7), PC(7), RH
C
C     IF (RH.GT.1.D0) RH = RH/1.D2
C
C /-----
C /
C/ CARD 3.  READ COMPARTMENT TEMPERATURE (F), PRESSURE (PSIA), VOLUME
C           (FT**3), AND FLOOR (DEPOSITION) AREA (FT**2).
C
C     READ (40,*) TC(1), PC(1), VOL(1), DPAREA(1)
C
C /-----
C /
C/ CARD 4.  READ INLET AIR BLOWER FLOW RATE (ACFM).
C
C     READ (40,*) ACFM(2)
C
C /-----
C /
C/ CARD 5.  READ HEAT TRANSFER SURFACE AREA IN COMPARTMENT (FT**2),
C           HEAT TRANSFER SURFACE TEMPERATURE (F), AND COOLING RATE
C           (BTU/HR). A NEGATIVE COOLING RATE IMPLIES A HEATING RATE.
C           WHILE THE VALUE OF THE SURFACE AREA IS NOT PARTICULARLY
C           IMPORTANT BECAUSE THE PRODUCT OF THE SURFACE AREA AND THE
C           HEAT TRANSFER COEFFICIENT TO BE CALCULATED WILL BE
C           CONSTANT, A SURFACE TEMPERATURE GREATER THAN THE
C           COMPARTMENT TEMPERATURE MUST BE SPECIFIED.
C
C     READ (40,*) HTAREA(1), TSURF(1), QCOOL(1)
C
C     QCOOL(1) = QCOOL(1)/3.603
C

```

```

C
C /
C/ CARD 6.  READ SOURCE TYPE, NUMBER OF RELEASES, BASIS FOR FLASH, AND
C           MOLECULAR WEIGHT. SOURCE TYPE IS GIVEN BY THE FOLLOWING:
C
C           4  LIQUID HF
C           5  VAPOR HF
C           7  LIQUID UF6 (VAPOR SOURCE TERM GENERATED)
C          -7  LIQUID UF6 (VAPOR/SOLID SOURCE TERM GENERATED)
C           8  VAPOR UF6
C          22  INPUT PROVIDED IN FOR22.DAT
C
C           IF SOURCE TYPE 22 IS SPECIFIED, SET NUMBER OF RELEASES TO
C           ZERO. NO MORE THAN FIVE RELEASES MAY BE SPECIFIED, WHICH
C           ARE TO RUN CONSECUTIVELY. THE BASIS FOR THE FLASH IS GIVEN
C           BY THE FOLLOWING:
C
C           0  ISENTROPIC
C           1  ISENTHALPIC
C
C           THE DEFAULT MOLECULAR WEIGHT FOR UF6 IS 352.025; ENTER A
C           VALUE LESS THAN 100 IF THAT VALUE IS ACCEPTABLE.
C
C           READ (40,*) ITYPE, IRELST, ISEN, MW
C
C           IF (MW.LT.100.D0) GO TO 10
C
C           WMOL(9) = WMOL(9) - WMOL(6) + MW
C           WMOL(6) = MW
C           WMOL(7) = MW
C           WMOL(8) = MW
C
C          10 CONTINUE
C
C           MWURAN = WMOL(6) - 113.99D0
C
C           IF (ITYPE.EQ.22) GO TO 30
C
C /
C/ CARD 7.  -- DO NOT USE "CARD 7" CARDS IF ITYPE = 22. --
C
C           READ FOR EACH INCREMENTAL RELEASE THE DURATION (SEC), MASS
C           (LB), TEMPERATURE (DEG F), AND PRESSURE (PSIA). SPECIFY AS
C           MANY SETS OF DATA AS THE NUMBER OF RELEASES (IRELST). IF
C           THE PRESSURE GIVEN IS LESS THAN OR EQUAL TO ZERO OR GREATER
C           THAN THE VAPOR PRESSURE, THE PRESSURE IS SET EQUAL TO THE
C           VAPOR PRESSURE FOR THAT INCREMENT.
C
C           READ (40,*) (TSOURC(I), MSOURC(I), TEMP(I), PRES(I), I=1,IRELST)
C
C           TRELS = 0.D0
C
C           MRELS = 0.D0

```

```

C
C   DO 20 I20=1,IRELST
C
C       TRELS = TRELS + TSOURC(I20)
C
C       MRELS = MRELS + MSOURC(I20)
C
C       IF (ITYPE.EQ.5) CALL PHFH20(TEMP(I20), 1.D0, 0.D0, PTEST,
*           0.D0, 0.D0)
C       IF (ITYPE.EQ.8) CALL VPRUF6(TEMP(I20), PTEST)
C
C       IF (PRES(I20).GT.PTEST .OR. PRES(I20).LE.0.D0)
*           PRES(I20) = PTEST
C
C   20 CONTINUE
C
C   30 CONTINUE
C
C
C /-----
C / CARD 8.  READ TIME INTERVAL FOR CALCULATIONS (SEC), DURATION OF
C           SIMULATION (SEC), AND PRINT INTERVAL (SEC).
C
C           READ (40,*) DELT, MAXTIM, PRINT
C
C           IFLAG = IDINT(PRINT/DELT+0.01D0)
C
C /-----
C / CARD 9.  -- THESE CARDS ARE OPTIONAL. --
C
C           READ DRAWING NUMBERS FOR PLOTS (LIMITED TO 20 CHARACTERS--
C           THE LAST CHARACTER MUST BE A DOLLAR SIGN ($)).
C
C           1ST CARD 9 = CUMULATIVE URANIUM RELEASED
C           2ND CARD 9 = CUMULATIVE HF RELEASED
C           3RD CARD 9 = URANIUM CONCENTRATION IN COMPARTMENT
C           4TH CARD 9 = HF CONCENTRATION IN COMPARTMENT
C           5TH CARD 9 = TEMPERATURE IN COMPARTMENT
C           6TH CARD 9 = PRESSURE IN COMPARTMENT
C
C   DO 40 I40=1,6
C
C       READ (40,4010,END=50) (DWGNUM(I40,I), I=1,4)
C       WRITE (49,4010) (DWGNUM(I40,I), I=1,4)
C
C   40 CONTINUE
C
C   50 CONTINUE
C
C       WRITE (49,4020)
C
C *****
C

```

```

C  STEADY STATE CONDITIONS
C  =====
C
C  SET STEADY-STATE CONDITIONS FOR THE COMPARTMENT, EXHAUST, AND INLET
C  AIR NODES.
C
C      CALL HUMID(7, RH, RATIO)
C
C      VOL(7) = 1.D9
C
C      CALL ROOM(7, RATIO)
C
C      CALL ROOM(1, RATIO)
C
C      CALL SSBLOW(2, RATIO)
C
C      MASS(4,1) = MASS(2,1)
C      MASS(4,3) = MASS(2,3)
C
C      TC(4) = TC(1)
C      PC(4) = PC(1)
C
C      KRCOEF(4) = 0.D0
C
C      CALL RESIST(4)
C
C      CALL DENTHL(TC(4), PC(4), 4, H(4))
C
C      CALL HCOEFF(1)
C
C      UA = HTCDEF(1) * HTAREA(1)
C
C *****
C
C  TITLE BLOCKS
C  =====
C
C  WRITE TITLE AND PROGRAM IDENTIFIER.
C
C      DO 60 I60=1,7
C
C          IDEV = 40 + I60
C
C          WRITE (IDEV,4030) TITLE
C
C  60 CONTINUE
C
C  WRITE NODE NAMES AND IMPORTANT CONSTANTS FOR EACH FILE.
C
C      WRITE (41,4100) VOL(1), UA, TSURF(1), QCOOL(1)
C
C      WRITE (42,4200) ACFM(4), TC(7), PC(7)
C
C      IF (ITYPE.EQ.4) WRITE (43,4304)

```

```
IF (ITYPE.EQ.5) WRITE (43,4305)
IF (IABS(ITYPE).EQ.7) WRITE (43,4307)
IF (ITYPE.EQ.8) WRITE (43,4308)
C
IF (ITYPE.NE.22) WRITE (43,4310)
C
IF (ITYPE.EQ.4) WRITE (43,4320) (TSOURC(I), MSOURC(I),
*   TEMP(I), I=1,5)
C
IF (ITYPE.EQ.5) WRITE (43,4330) (TSOURC(I), MSOURC(I),
*   TEMP(I), PRES(I), I=1,5)
C
IF (IABS(ITYPE).EQ.7) WRITE (43,4340) (TSOURC(I), MSOURC(I),
*   TEMP(I), I=1,3)
C
IF (IABS(ITYPE).EQ.7 .AND. ISEN.EQ.0) WRITE (43,4341) TSOURC(4),
*   MSOURC(4), TEMP(4)
C
IF (IABS(ITYPE).EQ.7 .AND. ISEN.EQ.1) WRITE (43,4342) TSOURC(4),
*   MSOURC(4), TEMP(4)
C
IF (IABS(ITYPE).EQ.7) WRITE (43,4343) WMOL(6), TSOURC(5),
*   MSOURC(5), TEMP(5)
C
IF (ITYPE.EQ.8) WRITE (43,4350) (TSOURC(I), MSOURC(I),
*   TEMP(I), PRES(I), I=1,3)
C
IF (ITYPE.EQ.8 .AND. ISEN.EQ.0) WRITE (43,4351) TSOURC(4),
*   MSOURC(4), TEMP(4), PRES(4)
C
IF (ITYPE.EQ.8 .AND. ISEN.EQ.1) WRITE (43,4352) TSOURC(4),
*   MSOURC(4), TEMP(4), PRES(4)
C
IF (ITYPE.EQ.8) WRITE (43,4353) WMOL(6), TSOURC(5), MSOURC(5),
*   TEMP(5), PRES(5)
C
IF (ITYPE.NE.22) WRITE (43,4360) TRELS, MRELS
C
IF (ITYPE.EQ.7) WRITE (43,4370)
C
IF (ITYPE.EQ.22) WRITE (43,4380)
C
WRITE (44,4400) KRCOEF(4)
C
WRITE (45,4500) DEPVEL, DPAREA(1)
C
WRITE (46,4600)
C
WRITE (47,4700)
C
WRITE COLUMN HEADINGS.
C
WRITE (41,4110) NAME
C
```

```

      DO 70 I70=2,4
C
      IDEV = 40 + I70
C
      WRITE (IDEV,4210) NAME
C
70 CONTINUE
C
      WRITE (45,4510) NAME
C
      WRITE (46,4610) NAME
C
      WRITE (47,4710)
C
C*****
C
C TRANSIENT ANALYSIS
C =====
C BEGIN TRANSIENT ANALYSIS.
C
      TIME = 0.00
C
      ICOUNT = IFLAG
C
      IRELS = 1
C
      TRELS = 0.00
C
C
C
C /
C/ OPTIONAL SOURCE TERM INPUT: CARD 1. ENTER TIME INTERVAL FOR SOURCE
C   TERM INPUT (SEC).
C
      IF (ITYPE.EQ.22) READ (22,*) DELTAT
C
80 CONTINUE
C
C EVALUATE SOURCE TERM
C =====
C
      IF (TIME.LT.TRELS) GO TO 120
C
      IF (ITYPE.NE.22) GO TO 100
C
C
C
C /
C/ OPTIONAL SOURCE TERM INPUT: CARD 2. ENTER INITIAL TIME FOR RELEASE
C   INTERVAL (SEC); MASS FLOW RATE (LB/SEC) FOR EACH OF THE NINE
C   COMPONENTS IN THE FOLLOWING ORDER: AIR, H2O(L), H2O(V),
C   HF(L), HF(V), UF6(S), UF6(L), UF6(V), UO2F2; SOURCE TERM
C   TEMPERATURE FOR INTERVAL (DEG F); AND SOURCE TERM PRESSURE
C   FOR THE INTERVAL (PSIA).
C

```

```

      READ (22,*,END=120) TRELS, (RATE(I),I=1,9),TC(IIN(1,2)),
*      PC(IIN(1,2))
C
      DO 90 I90=1,9
C
          MASS(IIN(1,2),I90) = RATE(I90)*DELT
C
      90 CONTINUE
C
          CALL DENTHL(TC(IIN(1,2)),PC(IIN(1,2)),IIN(1,2),H(IIN(1,2)))
C
          TRELS = TRELS + DELTAT
C
          GO TO 120
C
      100 CONTINUE
C
          IF (IRELS.GT.IRELST) GO TO 120
C
          TRELS = TSOURC(IRELS)
C
          SOURCE = MSOURC(IRELS)
C
          TC(3) = TEMP(IRELS)
C
          PC(3) = PRES(IRELS)
C
          CALL STERM(3, 1, SOLIDS)
C
          TRELS = 0.00
C
          DO 110 I110=1,IRELS
C
              TRELS = TRELS + TSOURC(I110)
C
      110 CONTINUE
C
          IRELS = IRELS + 1
C
      120 CONTINUE
C
          IF (TIME.GE.TRELS) IIN(1,2) = INODES
C
      EVALUATE FLOW RATES
C
      =====
C
      "CALL TRBLOW(2)" -- NOT CALLED SINCE INLET BLOWER PRODUCES
C
                       CONSTANT FLOW RATES THROUGHOUT TRANSIENT
C
                       ANALYSIS.
C
C
          CALL DPFLOW(4)
C
          IF (PC(1).LE.PC(7)) WRITE (44,4410) TIME

```



```

C
C CALCULATE DEPOSITION RATE.
C
C     CALL REMOVE(1, 5)
C
C     IF (ICOUNT.LT.IFLAG) GO TO 150
C
C OUTPUT NODE DATA
C =====
C
C WRITE COMPARTMENT DATA.
C
C     WRITE (41,4120) TIME, (MASS(1,I),I=1,9), TC(1), PC(1)
C
C WRITE DATA FOR FLOWING STREAMS.
C
C     DO 140 I140=2,5
C
C         IF (TIME.GE.TRELS .AND. I140.EQ.3) GO TO 140
C
C         DO 130 I130=1,9
C
C             RATE(I130) = MASS(I140,I130)/DELT
C
C 130     CONTINUE
C
C         IDEV = 40 + I140
C
C         HRATE = H(I140)/DELT
C
C         IF (I140.LE.4) WRITE (IDEV,4120) TIME, RATE, TC(I140),
*           PC(I140)
C         IF (I140.GT.4) WRITE (IDEV,4120) TIME, RATE
C
C 140 CONTINUE
C
C WRITE MASSES OF CONDENSED MATERIALS ON FLOOR.
C
C     WRITE (46,4120) TIME, (MASS(6,I),I=1,9)
C
C     ICOUNT = 0
C
C WRITE SUMMARY DATA ON RELEASE.
C
C     WRITE (47,4720) TIME, UF6REL, UOFREL, UTOT, HFREL, HFUF6, HFTOT,
*     DENU, DENHF
C
C WRITE SUMMARY DATA FOR PLOTTING.
C
C     IF (TIME.GT.TRELS) WRITE (48,*) TIME, UTOT, HFTOT, DENU, DENHF,
*     TC(1), PC(1)
C
C 150 CONTINUE
C

```

```

      IF (TIME.LE.60.D0 .AND. TIME.LE.TRELS) WRITE (48,*) TIME, UTOT,
*       HFTOT, DENU, DENHF, TC(1), PC(1)
C
      IF (TIME.GT.60.D0 .AND. TIME.LE.TRELS .AND.
*       10*(ICOUNT/10).EQ.ICOUNT)
*       WRITE (48,*) TIME, UTOT, HFTOT, DENU, DENHF, TC(1), PC(1)
C
C  EVALUATE COMPARTMENT CONDITIONS
C  =====
C
      TIME = TIME + DELT
C
      IF (TIME.GT.MAXTIM) STOP
C
      ICOUNT = ICOUNT + 1
C
C  PERFORM MASS AND ENERGY BALANCE FOR THE COMPARTMENT.
C
      CALL COMPRT(1, 2, INODES)
C
C  CALCULATE COMPARTMENT CONCENTRATIONS OF URANIUM AND HF.
C
      DENU = ((MASS(1,6) + MASS(1,7) + MASS(1,8))/WMOL(6)
*          + MASS(1,9)/WMOL(9))*MWURAN/VOL(1)
C
      DENHF = (MASS(1,4) + MASS(1,5))/VOL(1)
C
C  ACCUMULATE SOLID PARTICLES AND LIQUID DROPLETS ON THE FLOOR.
C
      DO 160 I160=1,9
C
          MASS(6,I160) = MASS(6,I160) + MASS(5,I160)
C
160 CONTINUE
C
      IF (ITYPE.EQ.7 .AND. TIME.LE.TRELS) MASS(6,6) = MASS(6,6)
*      + SOLIDS
C
C  ACCUMULATE TOTAL MASS QUANTITIES OF URANIUM AND HF RELEASED TO THE
C  ATMOSPHERE.
C
      UF6REL = UF6REL + MASS(4,6) + MASS(4,7) + MASS(4,8)
C
      UOFREL = UOFREL + MASS(4,9)
C
      UTOT = (UF6REL/WMOL(6) + UOFREL/WMOL(9))*MWURAN
C
      HFREL = HFREL + MASS(4,4) + MASS(4,5)
C
      HFUF6 = 4.D0*UF6REL*WMOL(4)/WMOL(6)
C
      HFTOT = HFREL + HFUF6
C
      GO TO 80

```

```

C
C*****
C
C  FORMAT STATEMENTS
C  =====
C
C  4000 FORMAT (10A8)
C
C  4010 FORMAT (4A5)
C
C  4020 FORMAT (6(1H$,/))
C
C  4030 FORMAT ('1  TITLE: ',10A8,/, '0  DATA GENERATED BY FODRFT -- ',
*          'A FORCED DRAFT VENTILATION SYSTEM TRANSIENT',
*          ' COMPARTMENT MODEL.')
```

```

C
C  4100 FORMAT ('0  COMPARTMENT CONDITIONS',T60,'COMPARTMENT VOLUME =',
*          F11.0,' FT**2',/,T60,'U*A PRODUCT          =',
*          1PE11.3,' BTU/SEC-DEG F',/,T60,'SURFACE TEMPERATURE =',
*          0PF11.1,' DEG F',/,T60,'COOLING RATE          =',1PE11.3,
*          ' BTU/SEC')
```

```

C
C  4110 FORMAT ('0  TIME',42X,'COMPONENT MASS (LB)',39X,
*          'TEMPERATURE PRESSURE',/, '      (SEC)',9(3X,A8),
*          ' (DEG F)   (PSIA)',/,1H )
```

```

C
C  4120 FORMAT (F10.1,1P9E11.3,0P2F10.4)
```

```

C
C  4200 FORMAT ('0  INLET AIR BLOWER',T60,'FLOW RATE          =',F11.1,
*          ' ACFM',/,T60,'AMBIENT TEMPERATURE =',F11.3,' DEG F',/,
*          T60,'AMBIENT PRESSURE   =',F11.3,' PSIA')
```

```

C
C  4210 FORMAT ('0  TIME',35X,'COMPONENT MASS FLOW RATE (LB/SEC)',
*          32X,'TEMPERATURE PRESSURE',/'      (SEC)',9(3X,A8),
*          ' (DEG F)   (PSIA)',/,1H )
```

```

C
C  4304 FORMAT ('0  SOURCE TERM: HF LIQUID',T60,
*          'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

```

C
C  4305 FORMAT ('0  SOURCE TERM: HF VAPOR',T60,
*          'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

```

C
C  4307 FORMAT ('0  SOURCE TERM: UF6 LIQUID',T60,
*          'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

```

C
C  4308 FORMAT ('0  SOURCE TERM: UF6 VAPOR',T60,
*          'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

```

C
C  4310 FORMAT (T60,' MENT      (SEC)   (LB)      (DEG F)      (PSIA)')
```

```

C
C  4320 FORMAT (1H0,T60,'  1',F11.1,F8.1,F11.3,' LIQUID',/,
*          T60,'  2',F11.1,F8.1,F11.3,' LIQUID',/,
*          T60,'  3',F11.1,F8.1,F11.3,' LIQUID',/,
*          T60,'  4',F11.1,F8.1,F11.3,' LIQUID',/,
```

```

      *   T60,'   5',F11.1,F8.1,F11.3,'   LIQUID')
C
4330 FORMAT (1H0,T60,'   1',F11.1,F8.1,2F11.3,/,
      *   T60,'   2',F11.1,F8.1,2F11.3,/,
      *   T60,'   3',F11.1,F8.1,2F11.3,/,
      *   T60,'   4',F11.1,F8.1,2F11.3,/,
      *   T60,'   5',F11.1,F8.1,2F11.3)
C
4340 FORMAT (1H0,T60,'   1',F11.1,F8.1,F11.3,'   LIQUID',/,
      *   T60,'   2',F11.1,F8.1,F11.3,'   LIQUID',/,
      *   T60,'   3',F11.1,F8.1,F11.3,'   LIQUID')
C
4341 FORMAT ('   FLASH BASIS:   ISENTROPIC',
      *   T60,'   4',F11.1,F8.1,F11.3,'   LIQUID')
C
4342 FORMAT ('   FLASH BASIS:   ISENTHALPIC',
      *   T60,'   4',F11.1,F8.1,F11.3,'   LIQUID')
C
4343 FORMAT ('   UF6 MOLECULAR WEIGHT =',F8.3,
      *   T60,'   5',F11.1,F8.1,F11.3,'   LIQUID')
C
4350 FORMAT (1H0,T60,'   1',F11.1,F8.1,2F11.3,/,
      *   T60,'   2',F11.1,F8.1,2F11.3,/,
      *   T60,'   3',F11.1,F8.1,2F11.3)
C
4351 FORMAT ('   FLASH BASIS: ISENTROPIC',
      *   T60,'   4',F11.1,F8.1,2F11.3)
C
4352 FORMAT ('   FLASH BASIS: ISENTHALPIC',
      *   T60,'   4',F11.1,F8.1,2F11.3)
C
4353 FORMAT ('   UF6 MOLECULAR WEIGHT =',F8.3,
      *   T60,'   5',F11.1,F8.1,2F11.3)
C
4360 FORMAT (T60,' TOTAL',F9.1,F8.1)
C
4370 FORMAT ('0   SOLIDS FORMED BY FLASHING UF6 LIQUID ARE ASSUMED',
      *   ' TO ACCUMULATE ON THE FLOOR.',/, ' THESE SOLIDS ARE NOT',
      *   ' INVOLVED IN ENERGY BALANCES ABOUT THE COMPARTMENT.')
C
4380 FORMAT ('0   SOURCE TERM: SOURCE TERM MASS FLOW RATES',
      *   ' TEMPERATURE, AND PRESSURE WERE READ FROM DATA FILE.')
C
4400 FORMAT ('0   EXHAUST STREAM (FORCED DRAFT)',T60,
      *   ' RESISTANCE TERM   =',1PE11.3,' PSI-SEC**2/LB/FT**3')
C
4410 FORMAT (F10.1,'   REVERSE FLOW OCCURING')
C
4500 FORMAT ('0   CONDENSATE FALLOUT',T60,' DEPOSITION VELOCITY =',
      *   F10.4,' FT/SEC',/,T60,' DEPOSITION AREA   =',F10.0,' FT**2')
C
4510 FORMAT ('0   TIME',35X,' COMPONENT MASS FLOW RATE (LB/SEC)',
      *   ', (SEC)',9(3X,A8),/,1H )
C

```

```

4600 FORMAT ('0 CONDENSATE ACCUMULATED ON FLOOR')
C
4610 FORMAT ('0 TIME',42X,'COMPONENT MASS (LB)',/,
*          '(SEC)',9(3X,A8),/,1H )
C
4700 FORMAT ('0 URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT',
*          'CONCENTRATIONS')
C
4710 FORMAT (1H0,T86,'COMPARTMENT CONCENTRATIONS',/, ' TIME ',
*          'CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED',
*          ' MATERIAL (LB)',T94,'(LB/FT**3)',/, ' (SEC) ',
*          ' UF6 UO2F2 TOTAL U HF HF FROM UF6',
*          ' TOTAL HF URANIUM HF',/,1H )
C
4720 FORMAT (F10.1,5X,1P6E11.3,5X,2E11.3)
C
C*****
C
END

```

## A.2 INDRFT - An Induced-Draft Compartment Model

```

C THIS PROGRAM MODELS A RELEASE OF UF6 OR HF INTO A COMPARTMENT
C HAVING AN INDUCED DRAFT VENTILATION SYSTEM. NODE NUMBERS AND
C STREAM DEFINITIONS FOR THIS MODEL ARE AS FOLLOWS.
C
C     1     COMPARTMENT
C     2     INLET AIR
C     3     SOURCE TERM
C     4     EXHAUST BLOWER
C     5     CONDENSATE FALLOUT
C     6     COMPARTMENT FLOOR
C     7     AMBIENT
C
C THE FOLLOWING VARIABLES ARE USED.
C
C     COMMON BLOCK VARIABLES
C
C     /LBMASS/
C
C     MASS    (30,9)  NODE MASS, LB, OR MASS FLOW RATE, LB/(DELT)
C     RH      (30,9)  RELATIVE HUMIDITY, % (AS INPUT) OR FRACTION
C                   (INTERNAL)
C
C     /COMPTP/
C
C     TC      (30)    NODE TEMPERATURE, DEG F
C     PC      (30)    NODE PRESSURE, PSIA
C     TSURF   (30)    NODE HEAT TRANSFER SURFACE TEMPERATURE, DEG F
C
C     /MOLWT/
C
C     WMOL    (9)     COMPONENT MOLECULAR WEIGHTS, LB/LB MOLE

```

C  
 C /VOLUME/  
 C  
 C VOL (30) NODE VOLUME, FT\*\*3  
 C KRCOEF (30) RESISTANCE COEFFICIENT, --, OR RESISTANCE TERM,  
 C RESISTANCE TERM, PSI-SEC\*\*2/LB-FT\*\*3  
 C DPAREA (30) DEPOSITION AREA, FT\*\*2  
 C DEPVEL DEPOSITION VELOCITY, FT/SEC  
 C  
 C /ENTHAL/  
 C  
 C H (30) NODE ENTHALPY, BTU, OR ENTHALPY RATE, BTU/(DELTA)  
 C QRATE (30) HEAT TRANSFER RATE, BTU/SEC OR BTU/(DELTA)  
 C QCOOL (30) COOLING RATE, BTU/HR (INPUT) OR BTU/SEC  
 C (INTERNAL)  
 C HTCDEF (30) HEAT TRANSFER COEFFICIENT, BTU/SEC-FT\*\*2-DEG F  
 C HTAREA (30) HEAT TRANSFER AREA, FT\*\*2  
 C  
 C /ISTRMS/  
 C  
 C IIN (30,4) INLET STREAM NODE NUMBER  
 C IOUT (30,4) OUTLET STREAM NODE NUMBER  
 C  
 C /CONTRL/  
 C  
 C AMINLN NATURAL LOG OF MINIMUM NUMBER ACCEPTED BY THE  
 C COMPUTER  
 C TIME CUMULATIVE SIMULATION TIME, SEC  
 C DELT TIME INTERVAL USED FOR TRANSIENT SIMULATION, SEC  
 C MAXTIM MAXIMUM SIMULATION TIME, SEC  
 C IFLAG FLAG TO CONTROL PRINTING OF OUTPUT  
 C TRELS TOTAL RELEASE TIME, SEC  
 C  
 C /POLYMR/  
 C  
 C C1 WEIGHT FRACTION OF HF MONOMER TO TOTAL HF VAPOR  
 C C3 WEIGHT FRACTION OF HF TRIMER TO TOTAL HF VAPOR  
 C C6 WEIGHT FRACTION OF HF HEXAMER TO TOTAL HF VAPOR  
 C WMBHF MOLECULAR WEIGHT OF HF MONOMER, LB/LB MOLE  
 C  
 C /MISCEL/  
 C  
 C ITYPE VARIABLE TO SPECIFY TYPE OF RELEASE, SEE CARD 5  
 C SOURCE TOTAL MASS OF RELEASE, LB  
 C ISEN VARIABLE TO SPECIFY ISENTROPIC OR ISENTHALPIC  
 C RELEASE, SEE CARD 5  
 C  
 C /RVFLOW/  
 C  
 C TSTART (30) START OF REVERSE FLOW IN NODE  
 C TSTOP (30) END OF REVERSE FLOW IN NODE

C  
 C EQUIVALENCED VARIABLES  
 C

C VOL ACFM (30) VOLUMETRIC FLOW RATE, FT\*\*3/MIN  
 C FLAREA (30) FLOW AREA FOR PRESSURE-DROP-CONTROLLED  
 C NODE, FT\*\*2  
 C

## OTHER DIMENSIONED VARIABLES

C RATE (9) COMPONENT MASS RELEASE RATE, LB/SEC  
 C MSOURC (5) INCREMENTAL SOURCE MASS, LB  
 C TSOURC (5) INCREMENTAL RELEASE TIME, SEC  
 C TEMP (5) TEMPERATURE OF INCREMENTAL SOURCE, DEG F  
 C PRES (5) PRESSURE OF INCREMENTAL SOURCE, PSIA  
 C NAME (9) COMPONENT IDENTIFIER  
 C TITLE (10) TITLE ARRAY  
 C DWGNUM (6,4) PLOT NUMBER ARRAY  
 C

## UNDIMENSIONED VARIABLES

C INODES MAXIMUM NUMBER OF NODES ALLOWED BY CODING OF  
 C SUBROUTINES  
 C INOUT MAXIMUM NUMBER OF INLET STREAMS AND OUTLET  
 C STREAMS  
 C IRELST NUMBER OF INCREMENTAL RELEASES IN TOTAL RELEASE  
 C (MAXIMUM OF 5)  
 C MW MOLECULAR WEIGHT, LB/LB MOLE  
 C MWURAN MOLECULAR WEIGHT OF URANIUM, LB/LB MOLE  
 C MRELS TOTAL MASS OF SOURCE MATERIAL RELEASED, LB  
 C PTEST VAPOR PRESSURE OF SOURCE, PSIA  
 C PRINT PRINT INTERVAL, SEC  
 C RATIO RATIO OF MOLES OF WATER VAPOR TO TOTAL MOLES OF  
 C MOIST AIR  
 C MASS2 MASS FLOW RATE THROUGH NODE 2, LB/(DELT)  
 C DENS DENSITY, LB/FT\*\*3  
 C DELP PRESSURE DROP, PSI  
 C UA PRODUCT OF HEAT TRANSFER COEFICIENT AND AREA,  
 C BTU/SEC-DEG F  
 C ICOUNT COUNTER TO CONTROL PRINTING OF OUTPUT  
 C IRELS CURRENT INCREMENT OF TOTAL RELEASE  
 C DELTAT SOURCE TERM INPUT INTERVAL, SEC  
 C SOLIDS MASS FLOW RATE OF UF6 SOLIDS ONTO THE FLOOR,  
 C LB/(DELT)  
 C V1 VOLUME OCCUPIED BY CONTENTS OF THE COMPARTMENT  
 C AT AMBIENT PRESSURE, FT\*\*3  
 C V2 MAXIMUM VOLUME TO BE RELEASED BY REVERSE FLOW  
 C THROUGH NODE 2 OVER A SPECIFIC TIME INTERVAL,  
 C FT\*\*3/(DELT)  
 C FRAC VOLUME FRACTION (-V2/V1) USED TO OBTAIN MASS  
 C FLOW AND ENTHALPY RATES WHEN LIMITING EXHAUST  
 C RATE THROUGH NODE 2  
 C IDEV OUTPUT DEVICE  
 C HRATE ENTHALPY RATE, BTU/SEC  
 C DENU COMPARTMENT CONCENTRATION OF URANIUM, LB/FT\*\*3  
 C DENHF COMPARTMENT CONCENTRATION OF HF, LB/FT\*\*3  
 C UF6REL CUMULATIVE MASS OF UF6 RELEASED TO THE  
 C ATMOSPHERE, LB

C UOFREL CUMULATIVE MASS OF UO2F2 RELEASED TO THE  
 C ATMOSPHERE, LB  
 C UTOT CUMULATIVE MASS OF URANIUM RELEASED TO THE  
 C ATMOSPHERE, LB  
 C HFREL CUMULATIVE MASS OF HF RELEASED TO THE  
 C ATMOSPHERE, LB  
 C HFUF6 CUMULATIVE MASS OF HF THAT CAN BE FORMED FROM  
 C UF6 RELEASED TO THE ATMOSPHERE, LB  
 C HFTOT CUMULATIVE MASS OF HF RELEASED TO OR FORMED IN  
 C THE ATMOSPHERE, LB

C LOGICAL VARIABLES

C CHECK FLAG IN ESTABLISHING INITIAL STEADY STATE  
 C CONDITIONS ABOUT NODE 2

C THE FOLLOWING SUBROUTINES ARE CALLED BY INDRFT.

C COMPRT  
 C DENTHL  
 C DPFLOW  
 C HCOEFF  
 C HUMID  
 C PHFH20  
 C REMOVE  
 C RESIST  
 C ROOM  
 C SETRAY  
 C SSBLOW  
 C STERM  
 C TRBLOW  
 C VPRUF6

C THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED.

C DENUF6  
 C EQTUF6  
 C FLASH  
 C HFPOLY  
 C HHFH20  
 C HUF6  
 C PHASE  
 C SUF6  
 C ZUF6

C\*\*\*\*\*

C INITIAL STATEMENTS

C =====

C IMPLICIT REAL\*8 (A-H,J-Z)

C LOGICAL CHECK

C



```

DIMENSION FLAREA(30), ACFM(30), RATE(9), MSOURC(5), TSOURC(5),
*   TEMP(5), PRES(5)
DIMENSION NAME(9), TITLE(10), DWGNUM(6,4)
C
COMMON /LBMASS/ MASS(30,9), RH
COMMON /COMPTP/ TC(30), PC(30), TSURF(30)
COMMON /MOLWT/ WMOL(9)
COMMON /VOLUME/ VOL(30), KRCOEF(30), DPAREA(30), DEPVEL
COMMON /ENTHAL/ H(30), QRATE(30), QCOOL(30), HTCDEF(30),
*   HTAREA(30)
COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
COMMON /CONTRL/ AMINLN, TIME, DELT, MAXTIM, IFLAG, TRELS
COMMON /POLYMR/ C1, C3, C6, WMBHF
COMMON /MISCEL/ ITYPE, SOURCE, ISEN
COMMON /RVFLOW/ TSTART(30), TSTOP(30)
C
EQUIVALENCE (VOL(1),ACFM(1),FLAREA(1))
C
DATA NAME /8HAIR  V , 8HH20  L , 8HH20  V , 8HHF  L ,
*   8HHF  V , 8HUF6  S , 8HUF6  L , 8HUF6  V , 8HU02F2 S /
C
CALL SETRAY(INODES, INOUT)
C
C  NODE ASSIGNMENT
C  =====
C
IIN(1,1) = 2
IIN(1,2) = 3
IIN(2,1) = 7
IIN(4,1) = 1
IIN(5,1) = 1
IIN(6,1) = 5
C
IOUT(1,1) = 4
IOUT(1,2) = 5
IOUT(2,1) = 1
IOUT(5,1) = 6
C
C  READ STATEMENTS
C  =====
C
C  ALL INPUT DATA EXCEPT THAT ON CARDS 1 AND 9 IS READ IN FREE FORMAT.
C  ON CARDS 1 AND 9, COUNT CHARACTERS STARTING IN COLUMN 1.
C
C
C /
C / CARD 1.  READ TITLE (MAXIMUM OF 80 CHARACTERS).
C
READ (40,4000) TITLE
C
C
C /
C / CARD 2.  READ AMBIENT TEMPERATURE (F), PRESSURE (PSIA), AND RELATIVE
C  HUMIDITY (%).

```

```

C
C   READ (40,*) TC(7), PC(7), RH
C
C   IF (RH.GT.1.D0) RH = RH/1.D2
C
C
C /-----
C /
C / CARD 3.  READ COMPARTMENT TEMPERATURE (F), PRESSURE (PSIA), VOLUME
C            (FT**3), AND FLOOR (DEPOSITION) AREA (FT**2). IF THE
C            COMPARTMENT PRESSURE IS NOT KNOWN AND IS TO BE CALCULATED,
C            SPECIFY A PRESSURE GREATER THAN OR EQUAL TO THE AMBIENT
C            PRESSURE OR LESS THAN OR EQUAL TO ZERO.
C
C            READ (40,*) TC(1), PC(1), VOL(1), DPAREA(1)
C
C /-----
C /
C / CARD 4.  READ EXHAUST FLOW RATE (ACFM), INLET FLOW AREA (FT**2), AND
C            INLET RESISTANCE COEFFICIENT (--). IF THE PROGRAM IS TO
C            CALCULATE THE RESISTANCE COEFFICIENT, A COMPARTMENT
C            PRESSURE GREATER THAN OR EQUAL TO THE AMBIENT PRESSURE OR
C            LESS THAN OR EQUAL TO ZERO MUST HAVE BEEN ENTERED, AND
C            AN INLET AREA AND RESISTANCE COEFFICIENT MUST BE GIVEN. A
C            RESISTANCE COEFFICIENT COEFFICIENT OF 1.5 REPRESENTS A
C            SUDDEN CONTRACTION FOLLOWED BY A SUDDEN EXPANSION.
C
C            READ (40,*) ACFM(4), FLAREA(2), KRCOEF(2)
C
C /-----
C /
C / CARD 5.  READ HEAT TRANSFER SURFACE AREA IN COMPARTMENT (FT**2),
C            HEAT TRANSFER SURFACE TEMPERATURE (F), AND COOLING RATE
C            (BTU/HR). A NEGATIVE COOLING RATE IMPLIES A HEATING RATE.
C            WHILE THE VALUE OF THE SURFACE AREA IS NOT PARTICULARLY
C            IMPORTANT BECAUSE THE PRODUCT OF THE SURFACE AREA AND THE
C            HEAT TRANSFER COEFFICIENT TO BE CALCULATED WILL BE
C            CONSTANT, A SURFACE TEMPERATURE GREATER THAN THE
C            COMPARTMENT TEMPERATURE MUST BE SPECIFIED.
C
C            READ (40,*) HTAREA(1), TSURF(1), QCOOL(1)
C
C            QCOOL(1) = QCOOL(1)/3.6D3
C
C /-----
C /
C / CARD 6.  READ SOURCE TYPE, NUMBER OF RELEASES, BASIS FOR FLASH, AND
C            MOLECULAR WEIGHT. SOURCE TYPE IS GIVEN BY THE FOLLOWING:
C
C            4   LIQUID HF
C            5   VAPOR HF
C            7   LIQUID UF6 (VAPOR SOURCE TERM GENERATED)
C            -7  LIQUID UF6 (VAPOR/SOLID SOURCE TERM GENERATED)
C            8   VAPOR UF6
C            22  INPUT PROVIDED IN FOR22.DAT

```

C  
C IF SOURCE TYPE IS SET EQUAL TO 22, SET NUMBER OF RELEASES  
C TO ZERO. NO MORE THAN FIVE RELEASES MAY BE SPECIFIED, WHICH  
C ARE TO RUN CONSECUTIVELY. THE BASIS FOR THE FLASH IS GIVEN  
C BY THE FOLLOWING:

C 0 ISENTROPIC  
C 1 ISENTHALPIC

C THE DEFAULT MOLECULAR WEIGHT FOR UF6 IS 352.025; ENTER A  
C VALUE LESS THAN 100 IF THAT VALUE IS ACCEPTABLE.  
C

READ (40,\*) ITYPE, IRELST, ISEN, MW

IF (MW.LT.100.D0) GO TO 10

WMOL(9) = WMOL(9) - WMOL(6) + MW  
WMOL(6) = MW  
WMOL(7) = MW  
WMOL(8) = MW

10 CONTINUE

MWURAN = WMOL(6) - 113.99D0

IF (ITYPE.EQ.22) GO TO 30

---

C /  
C / CARD 7. -- DO NOT USE "CARD 7" CARDS IF ITYPE = 22. --

C READ FOR EACH INCREMENTAL RELEASE THE DURATION (SEC), MASS  
C (LB), TEMPERATURE (DEG F), AND PRESSURE (PSIA). SPECIFY AS  
C MANY SETS OF DATA AS THE NUMBER OF RELEASES (IRELST). IF  
C THE PRESSURE GIVEN IS LESS THAN OR EQUAL TO ZERO OR GREATER  
C THAN THE VAPOR PRESSURE, THE PRESSURE IS SET EQUAL TO THE  
C VAPOR PRESSURE FOR THAT INCREMENT.  
C

READ (40,\*) (TSOURC(I), MSOURC(I), TEMP(I), PRES(I), I=1,IRELST)

TRELS = 0.D0

MRELS = 0.D0

DO 20 I20=1,IRELST

TRELS = TRELS + TSOURC(I20)

MRELS = MRELS + MSOURC(I20)

C IF (ITYPE.EQ.5) CALL PHFH20(TEMP(I20), 1.D0, 0.D0, PTEST,  
\* 0.D0, 0.D0)  
C IF (ITYPE.EQ.8) CALL VPRUF6(TEMP(I20), PTEST)

C

```

          IF (PRES(120).GT.PTEST .OR. PRES(120).LE.0.D0)
      *      PRES(120) = PTEST
C
C 20 CONTINUE
C
C 30 CONTINUE
C
C
C /-----
C /
C/ CARD 8.  READ TIME INTERVAL FOR CALCULATIONS (SEC), DURATION OF
C           SIMULATION (SEC), AND PRINT INTERVAL (SEC).
C
C           READ (40,*) DELT, MAXTIM, PRINT
C
C           IFLAG = IDINT(PRINT/DELT+0.01D0)
C
C /-----
C /
C/ CARD 9.  -- THESE CARDS ARE OPTIONAL. --
C
C           READ DRAWING NUMBERS FOR PLOTS (LIMITED TO 20 CHARACTERS--
C           THE LAST CHARACTER MUST BE A DOLLAR SIGN ($)).
C
C           1ST CARD 9 = CUMULATIVE URANIUM RELEASED
C           2ND CARD 9 = CUMULATIVE HF RELEASED
C           3RD CARD 9 = URANIUM CONCENTRATION IN COMPARTMENT
C           4TH CARD 9 = HF CONCENTRATION IN COMPARTMENT
C           5TH CARD 9 = TEMPERATURE IN COMPARTMENT
C           6TH CARD 9 = PRESSURE IN COMPARTMENT
C
C           DO 40 I40=1,6
C
C           READ (40,4010,END=50) (DWGNUM(I40,I), I=1,4)
C           WRITE (49,4010) (DWGNUM(I40,I), I=1,4)
C
C 40 CONTINUE
C
C 50 CONTINUE
C
C           WRITE (49,4020)
C
C *****
C
C STEADY STATE CONDITIONS
C =====
C
C SET STEADY-STATE CONDITIONS FOR THE COMPARTMENT, EXHAUST, AND INLET
C AIR NODES.
C
C           CALL HUMID(7, RH, RATIO)
C
C           IF (PC(1).GE.PC(7) .OR. PC(1).LE.0.D0) PC(1) = PC(7)
C
C           CHECK = .TRUE.

```

```

C      VOL(7) = 1.D9
C      CALL ROOM(7, RATIO)
C
60  CONTINUE
C      CALL ROOM(1, RATIO)
C      CALL SSBLOW(4, RATIO)
C      MASS(2,1) = MASS(4,1)
C      MASS(2,3) = MASS(4,3)
C
C      TC(2) = TC(7)
C      PC(2) = PC(7)
C
C      IF (PC(1).LT.PC(7) .AND. CHECK) GO TO 70
C      IF (CHECK) CALL RESIST(2)
C      CHECK = .FALSE.
C      MASS2 = MASS(2,1) + MASS(2,3)
C      DENS = (MASS(7,1)+MASS(7,3))/VOL(7)
C      DELP = KRCOEF(2)*MASS2*MASS2/DENS/DELT/DELT
C
C      IF (DABS(PC(7)-PC(1)-DELP).LT.1.D-6.AND.PC(1).LT.PC(7))
*      GO TO 70
C      PC(1) = PC(7) - DELP
C      GO TO 60
C
70  CONTINUE
C      KRCOEF(2) = 0.D0
C      CALL RESIST(2)
C      CALL DENTHL(TC(2), PC(2), 2, H(2))
C      CALL HCOEFF(1)
C      UA = HTCDEF(1) * HTAREA(1)
C
C*****
C  TITLE BLOCKS
C  =====
C
C  WRITE TITLE AND PROGRAM IDENTIFIER.

```

```

C
C   DO 80 I80=1,7
C
C       IDEV = 40 + I80
C
C       WRITE (IDEV,4030) TITLE
C
C 80 CONTINUE
C
C WRITE NODE NAMES AND IMPORTANT CONSTANTS FOR EACH FILE.
C
C   WRITE (41,4100) VOL(1), UA, TSURF(1), QCOOL(1)
C
C   WRITE (42,4200) KRCOEF(2), TC(7), PC(7)
C
C   IF (ITYPE.EQ.4) WRITE (43,4304)
C   IF (ITYPE.EQ.5) WRITE (43,4305)
C   IF (IABS(ITYPE).EQ.7) WRITE (43,4307)
C   IF (ITYPE.EQ.8) WRITE (43,4308)
C
C   IF (ITYPE.NE.22) WRITE (43,4310)
C
C   IF (ITYPE.EQ.4) WRITE (43,4320) (TSOURC(I), MSOURC(I),
*     TEMP(I), I=1,5)
C
C   IF (ITYPE.EQ.5) WRITE (43,4330) (TSOURC(I), MSOURC(I),
*     TEMP(I), PRES(I), I=1,5)
C
C   IF (IABS(ITYPE).EQ.7) WRITE (43,4340) (TSOURC(I), MSOURC(I),
*     TEMP(I), I=1,3)
C
C   IF (IABS(ITYPE).EQ.7 .AND. ISEN.EQ.0) WRITE (43,4341) TSOURC(4),
*     MSOURC(4), TEMP(4)
C
C   IF (IABS(ITYPE).EQ.7 .AND. ISEN.EQ.1) WRITE (43,4342) TSOURC(4),
*     MSOURC(4), TEMP(4)
C
C   IF (IABS(ITYPE).EQ.7) WRITE (43,4343) WMOL(6), TSOURC(5),
*     MSOURC(5), TEMP(5)
C
C   IF (ITYPE.EQ.8) WRITE (43,4350) (TSOURC(I), MSOURC(I),
*     TEMP(I), PRES(I), I=1,3)
C
C   IF (ITYPE.EQ.8 .AND. ISEN.EQ.0) WRITE (43,4351) TSOURC(4),
*     MSOURC(4), TEMP(4), PRES(4)
C
C   IF (ITYPE.EQ.8 .AND. ISEN.EQ.1) WRITE (43,4352) TSOURC(4),
*     MSOURC(4), TEMP(4), PRES(4)
C
C   IF (ITYPE.EQ.8) WRITE (43,4353) WMOL(6), TSOURC(5), MSOURC(5),
*     TEMP(5), PRES(5)
C
C   IF (ITYPE.NE.22) WRITE (43,4360) TRELS, MRELS
C

```

```

C      IF (ITYPE.EQ.7) WRITE (43,4370)
C      IF (ITYPE.EQ.22) WRITE (43,4380)
C      WRITE (44,4400) ACFM(4)
C      WRITE (45,4500) DEPVEL, DPAREA(1)
C      WRITE (46,4600)
C      WRITE (47,4700)
C      WRITE COLUMN HEADINGS.
C      WRITE (41,4110) NAME
C      DO 90 I90=2,4
C          IDEV = 40 + I90
C          WRITE (IDEV,4210) NAME
C      90 CONTINUE
C          WRITE (45,4510) NAME
C          WRITE (46,4610) NAME
C          WRITE (47,4710)
C
C*****
C      TRANSIENT ANALYSIS
C      =====
C      BEGIN TRANSIENT ANALYSIS.
C          TIME = 0.00
C          ICOUNT = IFLAG
C          IRELS = 1
C          TRELS = 0.00
C
C      _____
C /
C / OPTIONAL SOURCE TERM INPUT:  CARD 1.  ENTER TIME INTERVAL FOR SOURCE
C      TERM INPUT (SEC).
C
C          IF (ITYPE.EQ.22) READ (22,*) DELTAT
C      100 CONTINUE
C

```

```

C  EVALUATE SOURCE TERM
C  =====
C
C    IF (TIME.LT.TRELS) GO TO 140
C
C    IF (ITYPE.NE.22) GO TO 120
C
C
C /-----
C/  OPTIONAL SOURCE TERM INPUT:  CARD 2.  ENTER INITIAL TIME FOR RELEASE
C    INTERVAL (SEC); MASS FLOW RATE (LB/SEC) FOR EACH OF THE NINE
C    COMPONENTS IN THE FOLLOWING ORDER:  AIR, H2O(L), H2O(V),
C    HF(L), HF(V), UF6(S), UF6(L), UF6(V), UO2F2; SOURCE TERM
C    TEMPERATURE FOR INTERVAL (DEG F); AND SOURCE TERM PRESSURE
C    FOR THE INTERVAL (PSIA).
C
C    READ (22,*,END=140) TRELS, (RATE(I),I=1,9),TC(IIN(1,2)),
C    *    PC(IIN(1,2))
C
C    DO 110 I110=1,9
C
C        MASS(IIN(1,2),I110) = RATE(I110)*DELT
C
C 110 CONTINUE
C
C    TRELS = TRELS + DELTAT
C
C    GO TO 140
C
C 120 CONTINUE
C
C    IF (IRELS.GT.IRELST) GO TO 140
C
C    TRELS = TSOURC(IRELS)
C
C    SOURCE = MSOURC(IRELS)
C
C    TC(3) = TEMP(IRELS)
C
C    PC(3) = PRES(IRELS)
C
C    CALL STERM(3, 1, SOLIDS)
C
C    TRELS = 0.00
C
C    DO 130 I130=1,IRELS
C
C        TRELS = TRELS + TSOURC(I130)
C
C 130 CONTINUE
C
C    IRELS = IRELS + 1
C
C 140 CONTINUE

```



```

C      IF (TIME.GE.TRELS) IIN(1,2) = INODES
C
C      EVALUATE FLOW RATES
C      =====
C
C      CALL TRBLOW(4)
C
C      CALL DPFLOW(2)
C
C      LIMIT REVERSE FLOW EXHAUST RATE THROUGH DOOR.
C
C      IF (PC(1).LE.PC(7)) GO TO 160
C
C      V1 = PC(1)*VOL(1)/PC(7)
C
C      V2 = V1 - ACFM(4)*DELT/6.D1 - VOL(1)
C
C      IF (V2.LT.0.D0) V2 = 0.D0
C
C      FRAC = -V2/V1
C
C      IF (DABS(FRAC*MASS(1,1)).GE.DABS(MASS(2,1))) WRITE (42,4220) TIME
C
C      IF (DABS(FRAC*MASS(1,1)).GE.DABS(MASS(2,1))) GO TO 160
C
C      DO 150 I150=1,9
C
C          MASS(2,I150) = FRAC*MASS(1,I150)
C
C 150 CONTINUE
C
C      H(2) = FRAC*H(1)
C
C      TC(2) = TC(1)
C
C      PC(2) = PC(1)
C
C      WRITE (42,4230) TIME
C
C 160 CONTINUE
C
C      CALCULATE DEPOSITION RATE.
C
C      CALL REMOVE(1, 5)
C
C      IF (ICOUNT.LT.IFLAG) GO TO 190
C
C      OUTPUT NODE DATA
C      =====
C
C      WRITE COMPARTMENT DATA.
C
C          WRITE (41,4120) TIME, (MASS(1,I),I=1,9), TC(1), PC(1)

```

```

C
C WRITE DATA FOR FLOWING STREAMS.
C
C     DO 180 I180=2,5
C
C         IF (TIME.GE.TRELS .AND. I180.EQ.3) GO TO 180
C
C         DO 170 I170=1,9
C
C             RATE(I170) = MASS(I180,I170)/DELT
C
C 170     CONTINUE
C
C         IDEV = 40 + I180
C
C         HRATE = H(I180)/DELT
C
C         IF (I180.LE.4) WRITE (IDEV,4120) TIME, RATE, TC(I180),
*           PC(I180)
C         IF (I180.GT.4) WRITE (IDEV,4120) TIME, RATE
C
C 180 CONTINUE
C
C WRITE MASSES OF CONDENSED MATERIALS ON FLOOR.
C
C     WRITE (46,4120) TIME, (MASS(6,I),I=1,9)
C
C     ICOUNT = 0
C
C WRITE SUMMARY DATA ON RELEASE.
C
C     WRITE (47,4720) TIME, UF6REL, UOFREL, UTOT, HFREL, HFUF6, HFTOT,
*     DENU, DENHF
C
C WRITE SUMMARY DATA FOR PLOTTING.
C
C     IF (TIME.GT.TRELS) WRITE (48,*) TIME, UTOT, HFTOT, DENU, DENHF,
*     TC(1), PC(1)
C
C 190 CONTINUE
C
C     IF (TIME.LE.60.D0.AND.TIME.LE.TRELS) WRITE (48,*) TIME, UTOT,
*     HFTOT, DENU, DENHF, TC(1), PC(1)
C
C     IF (TIME.GT.60.D0.AND.TIME.LE.TRELS.AND.10*(ICOUNT/10).EQ.ICOUNT)
*     WRITE (48,*) TIME, UTOT, HFTOT, DENU, DENHF, TC(1), PC(1)
C
C EVALUATE COMPARTMENT CONDITIONS
C =====
C
C     TIME = TIME + DELT
C
C     IF (TIME.GT.MAXTIM) STOP
C

```

```

      ICOUNT = ICOUNT + 1
C
C   PERFORM MASS AND ENERGY BALANCE FOR THE COMPARTMENT.
C
      CALL COMPRT(1, 2, INODES)
C
C   CALCULATE COMPARTMENT CONCENTRATIONS OF URANIUM AND HF.
C
      DENU = ((MASS(1,6) + MASS(1,7) + MASS(1,8))/WMOL(6)
*           + MASS(1,9)/WMOL(9))*MWURAN/VOL(1)
C
      DENHF = (MASS(1,4) + MASS(1,5))/VOL(1)
C
C   ACCUMULATE SOLID PARTICLES AND LIQUID DROPLETS ON THE FLOOR.
C
      DO 200 I200=1,9
C
          MASS(6,I200) = MASS(6,I200) + MASS(5,I200)
C
200 CONTINUE
C
      IF (ITYPE.EQ.7 .AND. TIME.LE.TRELS) MASS(6,6) = MASS(6,6)
*       + SOLIDS
C
C   ACCUMULATE TOTAL MASS QUANTITIES OF URANIUM AND HF RELEASED TO THE
C   ATMOSPHERE.
C
      UF6REL = UF6REL + MASS(4,6) + MASS(4,7) + MASS(4,8)
*           + DABS(MASS(2,6) + MASS(2,7) + MASS(2,8))
C
      UOFREL = UOFREL + MASS(4,9) + DABS(MASS(2,9))
C
      UTOT = (UF6REL/WMOL(6) + UOFREL/WMOL(9))*MWURAN
C
      HFREL = HFREL + MASS(4,4) + MASS(4,5)
*           + DABS(MASS(2,4) + MASS(2,5))
C
      HFUF6 = 4.00*UF6REL*WMOL(4)/WMOL(6)
C
      HFTOT = HFREL + HFUF6
C
      GO TO 100
C
C*****
C
C   FORMAT STATEMENTS
C   =====
C
4000 FORMAT (10A8)
C
4010 FORMAT (4A5)
C
4020 FORMAT (6(1H#,/))
C

```

```

4030 FORMAT ('1 TITLE: ',10A8,/, '0 DATA GENERATED BY INDRFT -- ',
* 'AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT',
* ' COMPARTMENT MODEL.')
```

C

```

4100 FORMAT ('0 COMPARTMENT CONDITIONS',T60,'COMPARTMENT VOLUME =',
* F11.0,' FT**2',/,T60,'U*A PRODUCT =',
* 1PE11.3,' BTU/SEC-DEG F',/,T60,'SURFACE TEMPERATURE =',
* 0PF11.1,' DEG F',/,T60,'COOLING RATE =',1PE11.3,
* ' BTU/SEC')
```

C

```

4110 FORMAT ('0 TIME',42X,'COMPONENT MASS (LB)',39X,
* 'TEMPERATURE PRESSURE',/, ' (SEC)',9(3X,A8),
* ' (DEG F) (PSIA)',/,1H )
```

C

```

4120 FORMAT (F10.1,1P9E11.3,0P2F10.4)
```

C

```

4200 FORMAT ('0 INLET AIR STREAM (INDUCED DRAFT)',T60,
* 'RESISTANCE TERM =',1PE11.3,' PSI-SEC**2/LB/FT**3',
* /,T60,'AMBIENT TEMPERATURE =',0PF11.3,' DEG F',/,
* T60,'AMBIENT PRESSURE =',F11.3,' PSIA')
```

C

```

4210 FORMAT ('0 TIME',35X,'COMPONENT MASS FLOW RATE (LB/SEC)',
* 32X,'TEMPERATURE PRESSURE',/ ' (SEC)',9(3X,A8),
* ' (DEG F) (PSIA)',/,1H )
```

C

```

4220 FORMAT (F10.1,' REVERSE FLOW OCCURING')
```

C

```

4230 FORMAT (F10.1,' REVERSE FLOW OCCURING -- FLOW RATES LIMITED')
```

C

```

4304 FORMAT ('0 SOURCE TERM: HF LIQUID',T60,
* 'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

C

```

4305 FORMAT ('0 SOURCE TERM: HF VAPOR',T60,
* 'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

C

```

4307 FORMAT ('0 SOURCE TERM: UF6 LIQUID',T60,
* 'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

C

```

4308 FORMAT ('0 SOURCE TERM: UF6 VAPOR',T60,
* 'INCRE- DURATION MASS TEMPERATURE PRESSURE')
```

C

```

4310 FORMAT (T60,' MENT (SEC) (LB) (DEG F) (PSIA)')
```

C

```

4320 FORMAT (1H0,T60,' 1',F11.1,F8.1,F11.3,' LIQUID',/,
* T60,' 2',F11.1,F8.1,F11.3,' LIQUID',/,
* T60,' 3',F11.1,F8.1,F11.3,' LIQUID',/,
* T60,' 4',F11.1,F8.1,F11.3,' LIQUID',/,
* T60,' 5',F11.1,F8.1,F11.3,' LIQUID')
```

C

```

4330 FORMAT (1H0,T60,' 1',F11.1,F8.1,2F11.3,/,
* T60,' 2',F11.1,F8.1,2F11.3,/,
* T60,' 3',F11.1,F8.1,2F11.3,/,
* T60,' 4',F11.1,F8.1,2F11.3,/,
* T60,' 5',F11.1,F8.1,2F11.3)
```

```

C
4340 FORMAT (1H0,T60,' 1',F11.1,F8.1,F11.3,' LIQUID',/,
* T60,' 2',F11.1,F8.1,F11.3,' LIQUID',/,
* T60,' 3',F11.1,F8.1,F11.3,' LIQUID')
C
4341 FORMAT (' FLASH BASIS: ISENTROPIC',
* T60,' 4',F11.1,F8.1,F11.3,' LIQUID')
C
4342 FORMAT (' FLASH BASIS: ISENTHALPIC',
* T60,' 4',F11.1,F8.1,F11.3,' LIQUID')
C
4343 FORMAT (' UF6 MOLECULAR WEIGHT =',F8.3,
* T60,' 5',F11.1,F8.1,F11.3,' LIQUID')
C
4350 FORMAT (1H0,T60,' 1',F11.1,F8.1,2F11.3,/,
* T60,' 2',F11.1,F8.1,2F11.3,/,
* T60,' 3',F11.1,F8.1,2F11.3)
C
4351 FORMAT (' FLASH BASIS: ISENTROPIC',
* T60,' 4',F11.1,F8.1,2F11.3)
C
4352 FORMAT (' FLASH BASIS: ISENTHALPIC',
* T60,' 4',F11.1,F8.1,2F11.3)
C
4353 FORMAT (' UF6 MOLECULAR WEIGHT =',F8.3,
* T60,' 5',F11.1,F8.1,2F11.3)
C
4360 FORMAT (T60,' TOTAL',F9.1,F8.1)
C
4370 FORMAT ('0 SOLIDS FORMED BY FLASHING UF6 LIQUID ARE ASSUMED',
* ' TO ACCUMULATE ON THE FLOOR.',/, ' THESE SOLIDS ARE NOT',
* ' INVOLVED IN ENERGY BALANCES ABOUT THE COMPARTMENT.')
C
4380 FORMAT ('0 SOURCE TERM: SOURCE TERM MASS FLOW RATES',
* ' TEMPERATURE, AND PRESSURE WERE READ FROM DATA FILE.')
C
4400 FORMAT ('0 EXHAUST BLOWER',T60,'FLOW RATE =',F10.1,' ACFM')
C
4500 FORMAT ('0 CONDENSATE FALLOUT',T60,'DEPOSITION VELOCITY =',
* F10.4,' FT/SEC',/,T60,'DEPOSITION AREA =',F10.0,' FT**2')
C
4510 FORMAT ('0 TIME',35X,'COMPONENT MASS FLOW RATE (LB/SEC)',
* '/', '(SEC)',9(3X,A8),/,1H )
C
4600 FORMAT ('0 CONDENSATE ACCUMULATED ON FLOOR')
C
4610 FORMAT ('0 TIME',42X,'COMPONENT MASS (LB)',/,
* ' (SEC)',9(3X,A8),/,1H )
C
4700 FORMAT ('0 URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT',
* ' CONCENTRATIONS')
C
4710 FORMAT (1H0,T86,'COMPARTMENT CONCENTRATIONS',/, ' TIME ',
* ' CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED',

```

```

*      / MATERIAL (LB) ',T94, '(LB/FT**3) ',/, '      (SEC)      ',
*      /      UF6      UO2F2      TOTAL U      HF      HF FROM UF6',
*      /      TOTAL HF      URANIUM      HF',/,1H )
C
4720 FORMAT (F10.1,5X,1P6E11.3,5X,2E11.3)
C
C*****
C
      END

```

### A.3 BATCH - A Closed Compartment/Ventilation System Model

```

C THIS PROGRAM MODELS A RELEASE OF UF6 OR HF INTO A CLOSED COMPARTMENT
C OR A CONSTANT RELEASE OF UF6 OR HF INTO A CONSTANT VOLUME FLOW. IN
C THE LATTER CASE, THE REQUESTED COMPARTMENT VOLUME IS CONSIDERED A
C VOLUMETRIC FLOW RATE BASED ON THE SAME TIME UNIT AS THE SOURCE TERM.
C IF THE MODEL IS USED IN THE LATTER STEADY-STATE MODE, AN OPTION IS
C AVAILABLE TO PERMIT THE EVALUATION OF THE FINAL TEMPERATURE AND PHASE
C COMPOSITION AT AMBIENT PRESSURE (WHICH ASSUMES RELEASE TO THE AMBIENT
C SURROUNDINGS). THIS MODEL MAKES USE OF SUBROUTINES DEVELOPED FOR
C TRANSIENT ANALYSIS OF UF6 AND HF RELEASES IN BUILDINGS. NODE NUMBERS
C AND DEFINITIONS ARE AS FOLLOWS.

```

```

C
C      1      CLOSED COMPARTMENT
C      2      AMBIENT CONDITIONS
C      3      SOURCE TERM
C      4      OPEN COMPARTMENT (FINAL PRESSURE = AMBIENT PRESSURE)

```

```

C THE FOLLOWING VARIABLES ARE USED.

```

```

C COMMON BLOCK VARIABLES
C
C      /LBMASS/
C
C      MASS      (30,9)  NODE MASS, LB, OR MASS FLOW RATE, LB/(DELT)
C                      (INTERNAL)
C
C      /COMPTP/
C
C      TC      (30)      NODE TEMPERATURE, DEG F
C      PC      (30)      NODE PRESSURE, PSIA
C
C      /MOLWT/
C
C      WMOL      (9)      COMPONENT MOLECULAR WEIGHTS, LB/LB MOLE
C
C      /VOLUME/
C
C      VOL      (30)      NODE VOLUME, FT**3
C
C      /ENTHAL/
C
C      H      (30)      NODE ENTHALPY, BTU, OR ENTHALPY RATE, BTU/(DELT)

```

C  
 C /ISTRMS/  
 C  
 C IIN (30,4) INLET STREAM NODE NUMBER  
 C IOUT (30,4) OUTLET STREAM NODE NUMBER  
 C  
 C /CONTRL/  
 C  
 C AMINLN NATURAL LOG OF MINIMUM NUMBER ACCEPTED BY THE  
 C COMPUTER  
 C TIME CUMULATIVE SIMULATION TIME, SEC  
 C DELT TIME INTERVAL USED FOR TRANSIENT SIMULATION, SEC  
 C MAXTIM MAXIMUM SIMULATION TIME, SEC, EQUALS DELT FOR  
 C BATCH ANALYSIS  
 C IFLAG FLAG TO CONTROL PRINTING OF OUTPUT  
 C TRELS TOTAL RELEASE TIME, SEC, EQUALS DELT FOR BATCH  
 C ANALYSIS  
 C  
 C /POLYMR/  
 C  
 C C1 WEIGHT FRACTION OF HF MONOMER TO TOTAL HF VAPOR  
 C C3 WEIGHT FRACTION OF HF TRIMER TO TOTAL HF VAPOR  
 C C6 WEIGHT FRACTION OF HF HEXAMER TO TOTAL HF VAPOR  
 C WMBHF MOLECULAR WEIGHT OF HF MONOMER, LB/LB MOLE  
 C  
 C /MISCEL/  
 C  
 C ITYPE VARIABLE TO SPECIFY TYPE OF RELEASE, SEE CARD 5  
 C SOURCE TOTAL MASS OF RELEASE, LB  
 C ISEN VARIABLE TO SPECIFY ISENTROPIC OR ISENTHALPIC  
 C RELEASE, SEE CARD 5  
 C  
 C OTHER DIMENSIONED VARIABLES  
 C  
 C NAME (9) COMPONENT IDENTIFIER  
 C TITLE (6) TITLE ARRAY  
 C  
 C UNDIMENSIONED VARIABLES  
 C  
 C INODES MAXIMUM NUMBER OF NODES ALLOWED BY CODING OF  
 C SUBROUTINES  
 C INOUT MAXIMUM NUMBER OF INLET STREAMS AND OUTLET  
 C STREAMS  
 C RH RELATIVE HUMIDITY, % (AS INPUT) OR FRACTION  
 C MW MOLECULAR WEIGHT, LB/LB MOLE  
 C IWRITE CONTROL VARIABLE TO SPECIFY OUTPUT BASED ON THE  
 C ASSUMPTION OF AN OPEN COMPARTMENT  
 C RATIO RATIO OF MOLES OF WATER VAPOR TO TOTAL MOLES OF  
 C MOIST AIR  
 C SOLIDS MASS FLOW RATE OF UF6 SOLIDS ONTO THE FLOOR,  
 C LB/(DELT)  
 C MSSTOT FINAL TOTAL MASS IN COMPARTMENT, LB  
 C DENS DENSITY AT FINAL TEMPERATURE, PRESSURE, AND

```

C          VOLUME (SPECIFIC VOLUME OF CONDENSATE IS
C          NEGLECTED), LB/FT**3
C
C THE FOLLOWING SUBROUTINES ARE CALLED BY BATCH.
C
C          COMPRT
C          HUMID
C          MIXFLW
C          ROOM
C          SETRAY
C          STERM
C
C THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED.
C
C          DENTHL
C          DENUF6
C          EQTUF6
C          FLASH
C          HFPOLY
C          HHFH20
C          HUF6
C          PHASE
C          PHFH20
C          SUF6
C          VPRUF6
C          ZUF6
C
C*****
C
C INITIAL STATEMENTS
C =====
C
C      IMPLICIT REAL*8 (A-H,J-Z)
C
C      DIMENSION NAME(9), TITLE(6)
C
C      COMMON /LBMASS/ MASS(30,9), DUM1
C      COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
C      COMMON /MOLWT/ WMOL(9)
C      COMMON /VOLUME/ VOL(30), DUM3(61)
C      COMMON /ENTHAL/ H(30), DUM4(120)
C      COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C      COMMON /CONTRL/ AMINLN, TIME, DELT, MAXTIM, IFLAG, TRELS
C      COMMON /POLYMR/ C1, C3, C6, WMBHF
C      COMMON /MISCEL/ ITYPE, SOURCE, ISEN
C
C      DATA NAME /8HAIR  V ,8HH20  L ,8HH20  V ,8HHF  L ,
*      8HHF  V ,8HUF6  S ,8HUF6  L ,8HUF6  V ,
*      8HU02F2 S /
C
C SET PARAMETERS.
C
C      CALL SETRAY(INODES, INOUT)
C

```



```
      INOUT = 1
      IFLAG = 1
      IIN(1,1) = 3
      IIN(4,1) = 1
      IOUT(1,1) = INODES
      IOUT(4,1) = 2
      DELT = 6.01
      MAXTIM = DELT
      TRELS = DELT
C
C READ STAMENTS
C =====
C
C BATCH IS WRITTEN FOR INTERACTIVE EXECUTION.
C
C ALL INPUT DATA EXCEPT THAT ON CARD 1 ARE READ IN FREE FORMAT.
C ON CARD 1, COUNT CHARACTERS STARTING IN COLUMN 1.
C
C WARNING: OUTPUT APPEARS IN FOR06.DAT
C
C WRITE (5,5000)
C
C _____
C /
C/ CARD 1. -----
C
C ENTER TITLE (MAXIMUM OF 48 CHARACTERS).
C
C WRITE (5,5010)
C
C READ (5,5015) (TITLE(I5015), I5015=1,6)
C
C _____
C /
C/ CARD 2. -----
C
C ENTER COMPARTMENT TEMPERATURE (F), PRESSURE (PSIA), AND
C VOLUME (FT**3).
C
C WRITE (5,5020)
C
C READ (5,*) TC(1), PC(1), VOL(1)
C
C _____
C /
C/ CARD 3. -----
C
C ENTER AMBIENT TEMPERATURE (F), PRESSURE (PSIA), AND RELATIVE
C HUMIDITY (%)
C
C WRITE (5,5030)
C
C READ (5,*) TC(2), PC(2), RH
C
```

RH = RH/1.D2

```

C
C
C /
C/ CARD 4. -----
C
C   ENTER SOURCE TYPE (4=HF LIQUID, 5=HF VAPOR, 7=UF6 LIQUID WITH VAPOR
C   SOURCE TERM AND SOLIDS IGNORED IN HEAT BALANCE, -7=UF6 LIQUID WITH
C   VAPOR PLUS SOLID SOURCE TERM, 8=UF6 VAPOR), TEMPERATURE (F), AND
C   PRESSURE (PSIA--A NEGATIVE PRESSURE OR A LIQUID RELEASE DEFAULTS
C   TO THE VAPOR PRESSURE CORRESPONDING TO THE SOURCE TEMPERATURE).
C
C   WRITE (5,5040)
C
C   READ (5,*) ITYPE, TC(3), PC(3)
C
C   IF (ITYPE.EQ.4 .OR. ITYPE.EQ.5) GO TO 10
C
C
C /
C/ CARD 5. -----
C
C   ENTER UF6 MOLECULAR WEIGHT (A VALUE LESS THAN 100 DEFAULTS TO
C   352.025) AND BASIS FOR FLASH (0=ISENTROPIC, 1=ISENTHALPIC).
C
C   WRITE (5,5050)
C
C   READ (5,*) MW, ISEN
C
C   IF (MW.LT.1.D2) GO TO 10
C
C   WMOL(9) = WMOL(9) - WMOL(6) + MW
C   WMOL(6) = MW
C   WMOL(7) = MW
C   WMOL(8) = MW
C
C   10 CONTINUE
C
C
C /
C/ CARD 6. -----
C
C   ENTER MASS OF SOURCE TERM (LB).
C
C   WRITE (5,5060)
C
C   READ (5,*) SOURCE
C
C
C /
C/ CARD 7. -----
C
C   ENTER OUTPUT BASIS (1=CLOSED COMPARTMENT, 4=OPEN COMPARTMENT WITH
C   FINAL PRESSURE EQUAL TO AMBIENT PRESSURE).

```

```

C
C   WRITE (5,5070)
C
C   READ (5,*) IWRITE
C
C*****
C
C   BATCH ANALYSIS
C   =====
C
C     WRITE (6,6000) (TITLE(I6000), I6000=1,6)
C
C   EVALUATE INITIAL CONDITIONS.
C
C     CALL HUMID(2, RH, RATIO)
C
C     WRITE (6,6010)
C     WRITE (6,6020) TC(2)
C     WRITE (6,6030) PC(2)
C     WRITE (6,6040) RH, RATIO
C
C     CALL ROOM(1, RATIO)
C
C     WRITE (6,6050)
C     WRITE (6,6020) TC(1)
C     WRITE (6,6030) PC(1)
C     WRITE (6,6060) VOL(1)
C
C     DO 20 I20=1,9
C
C         IF (MASS(1,I20).GT.0.D0) WRITE (6,6070) NAME(I20),
*           MASS(1,I20)
C
C   20 CONTINUE
C
C   EVALUATE SOURCE TERM.
C
C     IF (ITYPE.EQ.4) WRITE (6,6090)
C     IF (ITYPE.EQ.5) WRITE (6,6100)
C     IF (IABS(ITYPE).EQ.7) WRITE (6,6110)
C     IF (ITYPE.EQ.8) WRITE (6,6120)
C
C     WRITE (6,6020) TC(3)
C
C     CALL STERM(3, 1, SOLIDS)
C
C     IF (ITYPE.EQ.5.OR.ITYPE.EQ.8) WRITE (6,6030) PC(3)
C     WRITE (6,6130) SOURCE
C
C     IF (IABS(ITYPE).EQ.7.OR.ITYPE.EQ.8) WRITE (6,6140) WMOL(6)
C
C     IF (IABS(ITYPE).EQ.7.AND.ISEN.EQ.0) WRITE (6,6150)
C     IF (IABS(ITYPE).EQ.7.AND.ISEN.EQ.1) WRITE (6,6160)
C     IF (ITYPE.EQ.8.AND.ISEN.EQ.0) WRITE (6,6170)

```

```

      IF (ITYPE.EQ.8.AND.ISEN.EQ.1) WRITE (6,6180)
C
      IF (ITYPE.EQ.7) WRITE (6,6190) SOLIDS
C
      IF (IABS(ITYPE).EQ.7) WRITE (6,6200) TC(3)
      IF (ITYPE.EQ.8) WRITE (6,6210) TC(3)
C
      DO 30 I30=1,9
C
          IF (MASS(3,I30).GT.0.D0) WRITE (6,6070) NAME(I30),
*             MASS(3,I30)
C
      30 CONTINUE
C
      EVALUATE CLOSED COMPARTMENT FINAL CONDITIONS.
C
      CALL COMPRT(1, INOUT, INODES)
C
      IF (IWRITE.EQ.1) GO TO 40
C
      EVALUATE OPEN COMPARTMENT FINAL CONDITIONS.
C
      CALL MIXFLW(4, 1, INODES)
C
      40 CONTINUE
C
      IF (IWRITE.EQ.1) WRITE (6,6220)
      IF (IWRITE.EQ.4) WRITE (6,6230)
C
      WRITE (6,6020) TC(IWRITE)
      WRITE (6,6030) PC(IWRITE)
      WRITE (6,6060) VOL(IWRITE)
C
      MSSTOT = 0.D0
C
      DO 50 I50=1,9
C
          MSSTOT = MSSTOT + MASS(IWRITE,I50)
C
          IF (MASS(IWRITE,I50).GT.0.D0) WRITE (6,6070) NAME(I50),
*             MASS(IWRITE,I50)
C
      50 CONTINUE
C
      DENS = MSSTOT/VOL(IWRITE)
C
      WRITE (6,6240) DENS
C
      STOP
C
C*****
C
C  FORMAT STATEMENTS
C  =====

```

```

C
5000 FORMAT (//, 41H      WARNING: OUTPUT APPEARS IN FOR06.DAT,
*      //)
C
5010 FORMAT ('      ENTER TITLE (MAXIMUM OF 48 CHARACTERS).')
C
5015 FORMAT (6A8)
C
5020 FORMAT (46H      ENTER COMPARTMENT TEMPERATURE (F), PRESSU,
*      14HRE (PSIA), AND, /, 20H      VOLUME (FT**3).)
C
5030 FORMAT (46H      ENTER AMBIENT TEMPERATURE (F), PRESSURE (,
*      19HPSIA), AND RELATIVE, /, 17H      HUMIDITY (%))
C
5040 FORMAT (46H      ENTER SOURCE TYPE (4=HF LIQUID, 5=HF VAPO,
*      2HR,, 24H 7=UF6 LIQUID WITH VAPOR, /, 11H      SOURCE,
*      16H TERM AND SOLIDS, 28H IGNORED IN HEAT BALANCE, -7,
*      16H=UF6 LIQUID WITH, /, 10H      VAPOR, 10H PLUS SOLI,
*      49HD SOURCE TERM, 8=UF6 VAPOR), TEMPERATURE (F), AND,
*      /, 46H      PRESSURE (PSIA--A NEGATIVE PRESSURE OR A ,
*      6HLIQUID, 17H RELEASE DEFAULTS, /, 14H      TO THE VA,
*      12HPOR PRESSURE, 32H CORRESPONDING TO THE SOURCE TEM,
*      10HPERATURE).)
C
5050 FORMAT (46H      ENTER UF6 MOLECULAR WEIGHT (A VALUE LESS ,
*      20HTHAN 100 DEFAULTS TO, /, 17H      352.025) AND,
*      16H BASIS FOR FLASH, 24H (0=ISENTROPIC, 1=ISENTH,
*      7HALPIC).)
C
5060 FORMAT (36H      ENTER MASS OF SOURCE TERM (LB).)
C
5070 FORMAT (46H      ENTER OUTPUT BASIS (1=CLOSED COMPARTMENT,
*      24H 4=OPEN COMPARTMENT WITH, /, 17H      FINAL PRESSU,
*      11HRE EQUAL TO, 19H AMBIENT PRESSURE).)
C
6000 FORMAT ('1      CASE: ',6A8)
C
6010 FORMAT ('-      AMBIENT CONDITIONS',/,1H )
C
6020 FORMAT ('      TEMPERATURE          ',F13.3,5X,
*      'DEG F')
C
6030 FORMAT ('      PRESSURE          ',F13.3,5X,
*      'PSIA')
C
6040 FORMAT ('      RELATIVE HUMIDITY          ',2PF11.1,7X,
*      '%',/,1H ,/, '      WATER VAPOR : MOIST AIR          ',0PF15.5,
*      3X,'MOLE/MOLE')
C
6050 FORMAT ('0      INITIAL COMPARTMENT CONDITIONS',/,1H )
C
6060 FORMAT ('      VOLUME          ',F11.1,7X,
*      'FT**3',/,1H )
C

```

```

6070 FORMAT (8X,'MASS OF ',A8,11X,F11.1,7X,'LB')
C
6080 FORMAT (1H ,/, '          TOTAL ENTHALPY          ',F11.1,7X,
*      'BTU',/,1H )
C
6090 FORMAT ('0    SOURCE TERM: HF LIQUID',/,1H )
C
6100 FORMAT ('0    SOURCE TERM: HF VAPOR',/,1H )
C
6110 FORMAT ('0    SOURCE TERM: UF6 LIQUID',/,1H )
C
6120 FORMAT ('0    SOURCE TERM: UF6 VAPOR',/,1H )
C
6130 FORMAT ('          TOTAL MASS OF SOURCE          ',F11.1,7X,
*      'LB',/,1H )
C
6140 FORMAT ('          MOLECULAR WEIGHT          ',F13.3,5X,
*      'LB/LB MOLE',/,1H )
C
6150 FORMAT ('          BASIS FOR FLASHING OF LIQUID',
*      ' ISENTROPIC',/,1H )
C
6160 FORMAT ('          BASIS FOR FLASHING OF LIQUID',
*      ' ISENTHALPIC',/,1H )
C
6170 FORMAT ('          BASIS FOR EXPANSION OF VAPOR',
*      ' ISENTROPIC',/,1H )
C
6180 FORMAT ('          BASIS FOR EXPANSION OF VAPOR',
*      ' ISENTHALPIC',/,1H )
C
6190 FORMAT ('          SOLID UF6 DUMPED ON FLOOR ',F11.1,7X,
*      'LB',/,1H )
C
6200 FORMAT ('          TEMPERATURE AFTER FLASHING ',F13.3,5X,
*      'DEG F',/,1H )
C
6210 FORMAT ('          TEMPERATURE AFTER EXPANSION',F13.3,5X,
*      'DEG F',/,1H )
C
6220 FORMAT ('0    FINAL CONDITIONS (CLOSED COMPARTMENT)',/,1H )
C
6230 FORMAT ('0    FINAL CONDITIONS (OPEN COMPARTMENT)',/,1H )
C
6240 FORMAT ('0    DENSITY OF FINAL MIXTURE ',F15.5,3X,
*      'LB/FT**3')
C
C*****
C
      END

```

#### A.4 CYLIND - A Cylinder Release Model

```

C THIS PROGRAM CALCULATES THE MASS FLOW RATE FROM A UF6 CYLINDER
C TO THE SURROUNDINGS THROUGH EITHER A BREACH OR HOLE IN THE
C CYLINDER OR THROUGH A PIGTAIL CONSISTING OF A KNOWN LENGTH OF
C PIPE AND FIXTURES. THE PROGRAM AND ALL SUBROUTINES ARE WRITTEN
C IN DOUBLE PRECISION.
C
C*****
C
C INITIAL STATEMENTS
C =====
C
C     IMPLICIT REAL*8 (A-H,J-Z)
C
C COMMON BLOCKS TRANSFER INFORMATION ON THE STATE OF UF6 AND
C ON THE OPTIONS TO BE USED.
C
C     COMMON /ICOMON/ ISEN, IPIG, IBRCH, IGEXIT
C     COMMON /CONCYL/ PCYL, TCYL, XVCYL, XLCYL, MW
C     COMMON /CONENT/ PENT, TENT, XVENT, XLENT, UNTBAR
C     COMMON /GMTRY / PIGRAY
C     COMMON /CONIN / PIN, TIN, XVIN, XLIN
C     COMMON /CONVOL/ PVOL, TVOL, XVOL, XLVOL
C     COMMON /PARAM / VOL, DELT, Q
C     COMMON /MASS / MSFLRT, MIN, MTOT
C     COMMON /CYLIND/ DIACYL, LCYL, RHOLE, DHOLE, ALPHA, IVERT
C     COMMON /TRIPLE/ TTRIPL, PTRIPL
C
C     DIMENSION TITLE(16)
C     DIMENSION PIGRAY(99,3), DUMMY(99)
C     DIMENSION TOTM(6), TOTV(6), CYLD(6), CYLL(6), HOLR(6), HOLD(6)
C     DIMENSION DWGNUM(4,4)
C
C THE FOLLOWING DATA STATEMENTS PROVIDE DEFAULT VALUES FOR VARIABLES
C REQUIRED BY THE SUBROUTINE LEVEL. THE USER MAY SPECIFY A COMPLETE
C SET OF VALUES BY SPECIFYING ICYL = 0 THEN ENTERING THE REQUIRED
C INFORMATION ON THE FOLLOWING LINE OF INPUT.
C
C MODEL NUMBER      5A      8A      12B      30B      48X      48Y
C
C VALUE OF ICYL     1      2      3      4      5      6
C
C     DATA TOTM / 55.D0, 255.D0, 460.D0, 5020.D0, 21030.D0, 27560.D0/
C     DATA TOTV / 0.284D0, 1.319D0, 2.38D0, 26.D0, 108.9D0, 142.7D0/
C     DATA CYLD / 5.D0, 8.D0, 12.D0, 29.D0, 48.D0, 48.D0/
C     DATA CYLL / 24.99D0, 45.34D0, 36.36D0, 68.02D0, 103.99D0, 136.27D0/
C     DATA HOLR / 1.375D0, 1.375D0, 1.375D0, 9.D0, 17.D0, 17.D0/
C     DATA HOLD / 0.375D0, 0.375D0, 0.375D0, 0.875D0, 0.875D0, 0.875D0/
C
C ANY PROGRAM USING THE BREACH AND PIGTAIL SUBROUTINES OR THE
C LIQUID LEVEL AND MASS/ENERGY BALANCE SUBROUTINES USED HERE
C MUST SUPPLY SIMILAR DATA AND TRANSFER BLOCK COMMON STATEMENTS.
C

```

C READ STATEMENTS

C =====

C

C

C

C /  
C/ CARD 1. READ TITLE (LIMITED TO 80 CHARACTERS).

C

READ (20,2000) TITLE

C

C

C /

C/ CARD 2. READ FLASH BASIS, CYLINDER TYPE, CYLINDER ORIENTATION,  
C AND NUMBER OF ELEMENTS IN RELEASE PATHWAY.

C

C

FLASH BASIS (ISEN)

C

C

0 ISENTROPIC

C

1 ISENTHALPIC

C

C

ISEN = 1 IS RECOMMENDED SINCE THE FLASHING PROCESS WAS  
ASSUMED TO BE ISENTHALPIC IN THE DERIVATION OF THE  
CORRELATION USED IN THE SUBROUTINE PIPSYS FOR PRESSURE  
DROP IN A PIPE.

C

C

CYLINDER TYPE (ICYL)

C

C

0 USER SPECIFIED

C

1 TYPE 5A CYLINDER

C

2 TYPE 8A CYLINDER

C

3 TYPE 12B CYLINDER

C

4 TYPE 30B CYLINDER (2.5 TON)

C

5 TYPE 48X CYLINDER (10 TON)

C

6 TYPE 48Y CYLINDER (14 TON)

C

C

IF A NEGATIVE VALUE OF ICYL IS READ (-1, -2, -3, -4, -5,  
-6), THE USER MAY SUBSEQUENTLY SPECIFY A TOTAL MASS OF UF6  
DIFFERENT FROM THE DEFAULT VALUE (SEE CARD 4).

C

C

CYLINDER ORIENTATION (IVERT)

C

C

-1 CYLINDER STANDS ON END -- RELEASE FROM TOP END

C

0 CYLINDER LIES ON SIDE -- RELEASE FROM END

C

1 CYLINDER STANDS ON END -- RELEASE FROM BOTTOM END

C

C

NUMBER OF ELEMENTS IN RELEASE PATHWAY (IPIG)

C

C

IF IPIG = 2, THE RELEASE PATHWAY IS A BREACH IN THE  
CYLINDER. IF THE RELEASE PATHWAY IS A PIPING SYSTEM, IPIG  
IS GREATER THAN 2.

C

C

READ (20,\*) ISEN, ICYL, IVERT, IPIG

C

IF(ICYL.GE.-6.AND.ICYL.LE.6) GO TO 10

C



```

WRITE (5,500) ICYL
C
STOP
C
10 CONTINUE
C
IF (IABS(ICYL).GT.0) GO TO 20
C


---


C/ CARD 3. -- USE THIS CARD ONLY IF ICYL = 0 --
C
READ MASS OF UF6 IN THE CYLINDER (LB); VOLUME (FT**3),
INTERNAL DIAMETER (IN), AND INTERNAL LENGTH (IN) OF THE
CYLINDER; RADIUS FROM THE CYLINDER CENTERLINE TO THE VALVE
(BREACH) (IN); AND THE VALVE (BREACH) DIAMETER (IN).
C
READ (20,*) MTOT, VOL, DIACYL, LCYL, RHOLE, DHOLE
C
GO TO 30
C
20 CONTINUE
C
MTOT = TOTM(IABS(ICYL))
VOL = TOTV(IABS(ICYL))
DIACYL = CYLD(IABS(ICYL))
LCYL = CYLL(IABS(ICYL))
RHOLE = HOLR(IABS(ICYL))
DHOLE = HOLD(IABS(ICYL))
C


---


C/ CARD 4. -- USE THIS CARD ONLY IF ICYL IS NEGATIVE --
C
READ MASS OF UF6 IN CYLINDER (LB).
C
IF (ICYL.LT.0) READ (20,*) MTOT
C
30 CONTINUE
C


---


C/ CARD 5. READ PRESSURE (PSIA), TEMPERATURE (DEG F), LIQUID MASS
FRACTION OF THE NONVAPOR FRACTION (--), MOLECULAR WEIGHT
(LB/LB MOLE), AND THE ANGLE MEASURED FROM A VERTICAL VECTOR
PASSING THROUGH THE CENTER OF THE END AND A VECTOR FROM THE
CENTER OF THE END AND THE ENTRANCE TO THE RELEASE PATHWAY
(DEG). IF PRESSURE IS SPECIFIED AS ZERO AND/OR TEMPERATURE
IS SPECIFIED AS NONZERO, THEN THE PRESSURE WILL BE SET EQUAL
TO THE VAPOR PRESSURE. IF PRESSURE IS SPECIFIED AS NONZERO
AND TEMPERATURE IS SPECIFIED AS ZERO, THEN THE EQUILIBRIUM
TEMPERATURE CORRESPONDING TO THE SPECIFIED PRESSURE WILL BE
CALCULATED. IF THE TRIPLE POINT TEMPERATURE IS SPECIFIED
(147.306561 DEG F), THEN A NONZERO VALUE FOR THE LIQUID MASS

```

C            FRACTION OF THE NONVAPOR FRACTION CAN BE SPECIFIED;  
 C            OTHERWISE, THE VALUE READ AS INPUT WILL BE SET BY THE  
 C            PROGRAM TO THE APPROPRIATE VALUE. THE DEFAULT VALUE FOR  
 C            MOLECULAR WEIGHT IS 352.025 -- IF THIS VALUE IS ACCEPTABLE,  
 C            A ZERO MAY BE SPECIFIED FOR THIS VARIABLE.

C            READ (20,\*) PVOL, TVOL, XLVOL, MW, ALPHA

C            CHECK SPECIFIED VALUES OF PVOL AND TVOL. TERMINATE EXECUTION IF AN  
 C            ERROR IS FOUND; OTHERWISE, CALCULATE THE APPROPRIATE VAPOR PRESSURE  
 C            OR EQUILIBRIUM TEMPERATURE.

C            IF (PVOL.GE.0.D0.AND.TVOL.GE.0.D0.AND.(PVOL+TVOL).GT.0.D0)  
 C            \*        GO TO 40

C            WRITE(5,510) PVOL, TVOL

C            STOP

C            40 CONTINUE

C            IF (TVOL.GT.0.D0) CALL VPRUF6 (TVOL,PVOL)

C            IF (TVOL.EQ.0.D0) CALL EQTUF6 (PVOL,TVOL)

C            SET THE TRIPLE POINT CONDITIONS AND CHECK THE VALUE OF THE  
 C            LIQUID/SOLID SPLIT.

C            PTRIPL = 22.04226474D0

C            TTRIPL = 147.306561D0

C            IF (TVOL.LT.TTRIPL) XLVOL = 0.D0

C            IF (TVOL.GT.TTRIPL) XLVOL = 1.D0

C            IF (XLVOL.GE.0.D0.AND.XLVOL.LE.1.D0) GO TO 50

C            WRITE (5,520) XLVOL

C            STOP

C            50 CONTINUE

C            IF (MW.EQ.0.D0) MW = 352.025D0

C            IF (IPIG.GT.2) GO TO 60

---

C/ CARD 6. -- USE THIS CARD ONLY IF IPIG = 2 --

C            READ AMBIENT PRESSURE (PSIA). A ZERO VALUE DEFAULTS TO  
 C            14.7 PSIA.

```

C
C   READ (20,*) PAMB
C
C   SET UP ELEMENTS OF PIGRAY FOR A BREACH CALCULATION.
C
C   PIGRAY(1,1) = 1.D0
C   PIGRAY(1,2) = 0.5D0
C   PIGRAY(1,3) = DHOLE/12.D0
C
C   PIGRAY(2,1) = 2.D0
C   PIGRAY(2,2) = 1.D0
C   PIGRAY(2,3) = 14.7D0
C
C   IF (PAMB.GT.0.D0) PIGRAY(2,3) = PAMB
C
C   GO TO 80
C
C   60 CONTINUE
C
C
C
C /-----
C /
C / CARD 7.  -- USE ONLY IF IPIG IS GREATER THAN 2 --
C
C   READ AS MANY CARDS AS THE VALUE OF IPIG TO SPECIFY THE
C   PIPING SYSTEM. EACH CARD CONTAINS (1) A VALUE SPECIFYING
C   ELEMENT TYPE, (2) ELEMENT LENGTH (FT) OR RESISTANCE
C   COEFFICIENT (--), AND (3) DIAMETER (IN), EXCEPT FOR THE LAST
C   CARD. THE THIRD VALUE ON THE LAST OF THE "CARD 7" CARDS IS
C   THE AMBIENT PRESSURE (PSIA).
C
C   ELEMENT TYPE (PIGRAY(I,1))
C
C   1   SPECIFIES A PIPE SEGMENT (EXCEPT FIRST "CARD 7" WHERE
C       IT SPECIFIES THE ENTRANCE)
C   2   SPECIFIES A PIPING SYSTEM FEATURE (SUDDEN EXPANSION,
C       VALVE, BEND, ETC.) FOR WHICH A RESISTANCE COEFFICIENT
C       IS SUPPLIED
C   3   SPECIFIES A SUDDEN CONTRACTION FOR WHICH A RESISTANCE
C       COEFFICIENT IS SUPPLIED
C
C   RESISTANCE COEFFICIENT (PIGRAY(I,2))
C
C   THIS VALUE MUST BE CALCULATED BY THE USER.
C
C   DIAMETER (PIGRAY(I,3))
C
C   (NOTE: PIGRAY(IPIG,3) IS THE EXHAUST PRESSURE, PSIA.)
C
C   FOR A SUDDEN CONTRACTION, SPECIFY THE DOWNSTREAM DIAMETER
C   FOLLOWING THE CONTRACTION. FOR A SUDDEN EXPANSION, SPECIFY
C   THE UPSTREAM DIAMETER BEFORE THE EXPANSION.
C
C   DO 70 I70 = 1,IPIG
C

```

```

      READ (20,*) (PIGRAY(I70,I), I=1,3)
C
C CONVERT DIAMETER FROM INCHES TO FEET FOR EACH ELEMENT OF THE
C PIGTAIL WHICH HAS A DIAMETER VALUE.
C
      IF (I70.LT.IPIG) PIGRAY(I70,3) = PIGRAY(I70,3)/12.D0
C
      70 CONTINUE
C
      80 CONTINUE
C
      PFIN = PIGRAY(IPIG,3)
C
C
C /-----
C /
C / CARD 8. READ SIMULATION TIME INTERVAL (SEC) AND MAXIMUM
C / SIMULATION TIME (SEC).
C /
      READ (20,*) DELT, MAXTIM
C
C /-----
C /
C / CARD 9. -- THESE CARDS ARE OPTIONAL --
C /
C / ENTER DRAWING NUMBERS (LIMITED TO 20 CHARACTERS--THE LAST
C / CHARACTER MUST BE A DOLLAR SIGN ($)). THESE NUMBERS ARE
C / ENTERED IN A FILE FOR CYLPLT PROCESSING.
C /
C / 1ST CARD 9 = PHASE MASSES AND TOTAL MASS OF UF6 INSIDE
C / CYLINDER
C / 2ND CARD 9 = PHASE AND TOTAL MASS RELEASE RATES FROM
C / CYLINDER
C / 3RD CARD 9 = TEMPERATURE AND PRESSURE INSIDE CYLINDER
C / 4TH CARD 9 = EXHAUST TEMPERATURE
C /
      DO 90 I90=1,4
C
      READ (20,2010,END=100) (DWGNUM(I90,I), I=1,4)
      WRITE (31,2010) (DWGNUM(I90,I), I=1,4)
C
      90 CONTINUE
C
      100 CONTINUE
C
      WRITE(31,2020)
C
C *****
C
C INITIAL CONDITIONS
C =====
C
C DENUF6 WILL CALCULATE DENSITIES OF UF6 PHASES IN THE CYLINDER
C
      CALL DENUF6 (TVOL,PVOL,MW,DENSOL,DENLIQ,DENVAP)

```

```

C
C THE VAPOR MASS FRACTION IN THE CYLINDER CAN NOW BE DETERMINED
C
      XVOL = ( VOL/MTOT - XLVOL/DENLIQ - (1.D0-XLVOL)/DENSOL)
      *      / (1.D0/DENVAP - XLVOL/DENLIQ - (1.D0-XLVOL)/DENSOL)
C
C THIS ARGUMENT TO THE LEVEL SUBROUTINE SAVES PREVIOUS VALUES OF
C LIQUID LEVEL FOR USE AS INITIAL GUESSES. IT IS INITIALLY SET EQUAL
C TO CYLINDER DIAMETER.
C
      VLFACE = DIACYL
C
C THIS DRIVER ROUTINE DOES NOT CONSIDER AN INLET STREAM TO THE
C CYLINDER. THE LEVEL AND INTMEB SUBROUTINES ARE WRITTEN TO
C HANDLE SUCH A STREAM. THEREFORE SET MASS OF THE STREAM TO
C ZERO AND OTHER STREAM PARAMETERS TO MATCH THE CYLINDER
C CONTENTS.
C
      MIN = 0.D0
C
      PIN = PVOL
C
      TIN = TVOL
C
      XVIN = XVOL
C
      XLIN = XLVOL
C
      ITRIPL = 0
C
C SET TIME STEP AND HEAT TRANSFER
C
      DELTSM = 0.D0
C
      Q = 0.D0
C
      WRITE (30,3000) TITLE
C
      WRITE (30,3010)
C
      WRITE (22,2200) DELT
C
C*****
C
C TRANSIENT ANALYSIS
C =====
C
110 CONTINUE
C
C FROM THIS POINT ON THE PROGRAM SOLVES EACH TIME STEP USING
C VALUES FROM THE PREVIOUS STEP AND FROM THE MASS AND ENERGY
C BALANCE ABOUT THE CYLINDER. STARTING VALUES FOR THE STREAM
C LEAVING THE CYLINDER DURING THE COMING TIME STEP ARE INPUT AND
C THE LEVEL SUBROUTINE IS CALLED IF NEEDED TO MODIFY THESE

```

```

C PARAMETERS AS REQUIRED. TCYL IS ALWAYS EQUAL TO TVOL, BUT
C XVCYL, XLCYL, AND PCYL MAY BE CHANGED AS THE VAPOR/LIQUID
C INTERFACE DROPS.
C
C     XVCYL = 1.D0
C
C     XLCYL = XLVOL
C
C     PCYL = PVOL
C
C     TCYL = TVOL
C
C PHASE INTERFACE LEVEL
C =====
C
C     IF (IVERT.NE.-1) CALL LEVEL (DENVAP,VLFACE)
C
C BREACH FLOW RATE ANALYSIS
C =====
C
C THE BREACH SUBROUTINE CALCULATES A MASS VELOCITY AND A SET OF
C CONDITIONS FOLLOWING THE ENTRANCE PRESSURE DROP. THOSE
C CONDITIONS ARE TRANSFERRED TO PIPSYS IF THE PIGTAIL
C SUBROUTINE IS CALLED.
C
C     IF (DELTSM.GT.0.D0 .AND. IPIG.GT.2) GO TO 120
C
C     CALL BREACH (G)
C
C THE BREACH SUBROUTINE HAS CALCULATED A MAXIMUM VALUE OF MASS
C VELOCITY.
C
C     IF(IPIG.EQ.2) GO TO 130
C
C PIPING SYSTEM FLOW RATE ANALYSIS
C =====
C
C THE PIGTAIL SUBROUTINE CALCULATES NEW VALUES OF G FOR RELEASES
C OF UF6 THROUGH PIGTAILS CONSISTING OF LENGTHS OF PIPE AND
C FIXTURES SUCH AS ELBOWS AND VALVES.
C
C 120 CONTINUE
C
C     IF (TCYL.EQ.TTRIPL .AND. XVCYL.EQ.1 .AND. ITRIPL.EQ.1) GO TO 130
C
C     CALL PIPSYS (G)
C
C SET BASIS FOR SUBSEQUENT EVALUATIONS OF G IN PIPSYS.
C
C     IBRCH = 3
C
C SET FLAG FOR SKIPPING CALL TO PIPSYS.
C
C     ITRIPL = 0

```

```

C      IF (TCYL.EQ.TTRIPL .AND. XVCYL.EQ.1.D0) ITRIPL = 1
C
C 130 CONTINUE
C
C OUTPUT DATA
C =====
C
C PHASE COMPOSITION INSIDE CYLINDER
C
C      MSOL = MTOT*(1.D0 - XVOL)*(1.D0 - XLVOL)
C      MLIQ = MTOT*(1.D0 - XVOL)*XLVOL
C      MVAP = MTOT*XVOL
C
C PHASE COMPOSITION ENTERING RELEASE PATHWAY
C
C      PHASE = ' '
C      IF (XVCYL.EQ.1.D0) PHASE = ' VAPOR '
C      IF (XVCYL.LT.1.D0.AND.XVCYL.GT.0.D0.AND.XLCYL.EQ.1.D0)
C *      PHASE = 'LIQ-VAP'
C      IF (XVCYL.LT.1.D0.AND.XVCYL.GT.0.D0.AND.XLCYL.LT.1.D0.
C *      AND.XLCYL.GT.0.D0) PHASE = '3-PHASE'
C      IF (XVCYL.EQ.0.D0.AND.XLCYL.EQ.1.D0) PHASE = 'LIQUID '
C      IF (XVCYL.EQ.0.D0.AND.XLCYL.LT.1.D0.AND.XLCYL.GT.0.D0)
C *      PHASE = 'SOL-LIQ'
C
C CONDITIONS OF UF6 EXHAUSTED AT FINAL PRESSURE
C
C      CALL FLASH (TVOL,PVOL,MW,XVCYL,XLCYL,PFIN,ISEN,XVFIN,XLFIN,TFIN)
C
C      MSFLRT = G*(PIGRAY(1,3)**2)*3.14159D0/4.D0
C
C      MSSRTS = MSFLRT*(1.D0 - XVFIN)*(1.D0 - XLFIN)
C      MSSRTL = MSFLRT*(1.D0 - XVFIN)*XLFIN
C      MSSRTV = MSFLRT*XVFIN
C
C BASIS FOR FLOW RATE CALCULATION
C
C      BASIS = 'CHOKE'
C      IF (IPIG.EQ.2.AND.IBRCH.EQ.2) BASIS = ' PDC '
C      IF (IPIG.GT.2.AND.IGEXIT.EQ.2) BASIS = ' PDC '
C
C OUTPUT TO TERMINAL FOR MONITORING PROGRESS OF PROGRAM EXECUTION
C
C      WRITE (5,530) DELTSM,MTOT,MSFLRT
C
C PROGRAM OUTPUT
C
C      WRITE (30,3020) DELTSM,MSOL,MLIQ,MVAP,MTOT,TVOL,PVOL,PHASE,
C *      PCYL,BASIS,MSSRTS,MSSRTL,MSSRTV,MSFLRT,PFIN,TFIN
C
C OUTPUT TO DATA FILE FOR INPUT TO FODRFT OR INDRFT
C
C      WRITE (22,2210) DELTSM,MSSRTS,MSSRTL,MSSRTV,TFIN,PFIN

```

```

C
C CYLINDER INTERNAL MASS AND ENERGY BALANCE
C =====
C
C     CALL INTMEB
C
C     DELTSM = DELTSM+DELT
C
C     CALL DENUF6 (TVOL,PVOL,MW,DENSOL,DENLIQ,DENVAP)
C
C     IF (TVOL.LT.TTRIPL .OR. MTOT.LT.(MSFLRT*DELT).OR.
*     DELTSM.GE.MAXTIM) STOP
C
C     GO TO 110
C
C *****
C
C     FORMAT STATEMENTS
C     =====
C
C     500 FORMAT('  VALUE OF ICYL =',I3,
*     ' NOT RECOGNIZED -- EXECUTION TERMINATED.')

```



```

      *      ' (DEG F) (PSIA)',/,1H )
C
3020 FORMAT(F7.0,1X,4F8.1,2F8.3,2X,A7,F8.3,2X,A5,1X,6F8.3)
C
C*****
C
      END

```

### A.5 COMPLT - A Plotting Program for FODRFT and INDRFT Results

```

C THIS PROGRAM PLOTS OUTPUT FROM FODRFT AND INDRFT.
C
C THIS PROGRAM USES DISSPLA (VERSION 9.0) SUBROUTINES FOR PLOTTING.
C DISSPLA IS A PRODUCT OF INTEGRATED SOFTWARE SYSTEMS CORPORATION OF
C SAN DIEGO, CALIFORNIA. DOCUMENTATION WAS COPYRIGHTED IN 1981.
C
C*****
C
C INITIAL STATEMENTS
C =====
C
      IMPLICIT REAL*4 (A-H,J-Z)
C
      DIMENSION TIME(1000), UTOT(1000), HFTOT(1000), DENU(1000),
*      DENHF(1000), T(1000), P(1000)
      DIMENSION DWGNUM(6,4), NUMBER(4)
C
C*****
C
C READ STATEMENTS
C =====
C
      IMAX = 0
C
C CODING BETWEEN "10 CONTINUE" AND "30 CONTINUE" READS AND DEVELOPS
C DATA FOR PLOTTING
C
      10 CONTINUE
C
      IMAX = IMAX + 1
C
C INPUT IS READ FROM AN UNFORMATTED OUTPUT FILE GENERATED BY EITHER
C FODRFT OR INDRFT.
C
      READ (48,*,END=30) TIME(IMAX), UTOT(IMAX), HFTOT(IMAX),
*      DENU(IMAX), DENHF(IMAX), T(IMAX), P(IMAX)
C
      IF (DENU(IMAX).LT.1.E-20) DENU(IMAX) = 1.E-20
      IF (DENHF(IMAX).LT.1.E-20) DENHF(IMAX) = 1.E-20
C
      IF (IMAX.GT.1) GO TO 20
C
      DUMAX = DENU(1)

```

```

      DUMIN = DENU(1)
C
      DHFMAX = DENHF(1)
      DHFMIN = DENHF(1)
C
      TMAX = T(1)
      TMIN = T(1)
C
      PMAX = P(1)
      PMIN = P(1)
C
      GO TO 10
C
20 CONTINUE
C
      IF (DENU(IMAX).GT.DUMAX) DUMAX = DENU(IMAX)
      IF (DENU(IMAX).LT.DUMIN) DUMIN = DENU(IMAX)
C
      IF (DENHF(IMAX).GT.DHFMAX) DHFMAX = DENHF(IMAX)
      IF (DENHF(IMAX).LT.DHFMIN) DHFMIN = DENHF(IMAX)
C
      IF (T(IMAX).GT.TMAX) TMAX = T(IMAX)
      IF (T(IMAX).LT.TMIN) TMIN = T(IMAX)
C
      IF (P(IMAX).GT.PMAX) PMAX = P(IMAX)
      IF (P(IMAX).LT.PMIN) PMIN = P(IMAX)
C
      GO TO 10
C
30 CONTINUE
C
      READ DRAWING NUMBERS.
C
      DO 40 I40=1,6
C
          READ (49,4900) (DWGNUM(I40,I), I=1,4)
C
40 CONTINUE
C
      IMAX = IMAX - 1
C
      TIMMAX = TIME(IMAX)
C
      UMAX = UTOT(IMAX)
C
      HFMAX = HFTOT(IMAX)
C
      DUMIN = AMAX1(DUMIN,5.07E-8)
C
      DHFMIN = AMAX1(DHFMIN,6.24E-8)
C
C*****
C
C PLOTTING COMMANDS

```

```

C =====
C
C   CALL COMPRS
C
C   DO 80 I80=1,6
C
C SET UP AXES.
C
C   CALL RESET('ALL')
C   CALL NOBRDR
C   CALL GRACE (0.)
C   CALL AREA2D(5.,5.)
C   CALL FRAME
C   CALL DUPLX
C   CALL XREVTK
C   CALL YREVTK
C   CALL YAXANG(0.0)
C
C   CALL MX1ALF('STANDARD','!')
C   CALL MX2ALF('L/CSTD','@')
C   CALL MX3ALF('INSTRUCTION','&')
C
C   CALL XINTAX
C   CALL XNAME ('CUMULATIVE TIME OF TRANSIENT@ (SEC)!$',100)
C   CALL AXSPLT (0.,TIMMAX,5.,XORIG,XSTEP,XAXIS)
C   XMAX = XORIG + XSTEP*XAXIS
C
C   IF(I80.EQ.3.OR.I80.EQ.4) GO TO 50
C
C PLOT LINEAR AXES FOR PLOTS 1, 2, 5, AND 6.
C
C   IF (I80.EQ.1) CALL YNAME ('CUMULATIVE URANIUM RELEASED@ (LB)!$',
*   100)
C   IF (I80.EQ.1) CALL AXSPLT (0.,UMAX,5.,YORIG,YSTEP,YAXIS)
C
C   IF (I80.EQ.2) CALL YNAME ('CUMULATIVE HF RELEASED@ (LB)!$',100)
C   IF (I80.EQ.2) CALL AXSPLT (0.,HFMAX,5.,YORIG,YSTEP,YAXIS)
C
C   IF (I80.EQ.5) CALL YNAME
*   ('TEMPERATURE IN COMPARTMENT@ (&EH.5@&EXHX!F@)!$',100)
C   IF (I80.EQ.5) CALL AXSPLT (TMIN,TMAX,5.,YORIG,YSTEP,YAXIS)
C
C   IF (I80.EQ.6) CALL YNAME ('PRESSURE IN COMPARTMENT@ (PSIA)!$',
*   100)
C   IF (I80.EQ.6) CALL AXSPLT (PMIN,PMAX,5.,YORIG,YSTEP,YAXIS)
C
C   YMAX = YORIG + YSTEP*YAXIS
C
C   CALL YINTAX
C   CALL GRAF (XORIG,XSTEP,XMAX,YORIG,YSTEP,YMAX)
C
C   GO TO 60
C
C 50 CONTINUE

```

```

C
C PLOT SEMILOG AXES FOR PLOTS 3 AND 4.
C
  CALL YTICKS (0)
  CALL YAXEND ('NOENDS')
  CALL RESET ('YINTAX')
  CALL RESET ('YNAME')
  CALL GRAF (XORIG,XSTEP,XMAX,0,1,1)
  CALL RESET ('YAXEND')
  CALL YTICKS(1)
C
  IF (I80.EQ.3) CALL ALGPLT (DUMIN,DUMAX,5.,YORIG,YCYCLE)
  IF (I80.EQ.3) CALL YLGAXS (YORIG,YCYCLE,5.,
*   'URANIUM CONCENTRATION IN COMPARTMENT@ (LB/FT&EH.8@3&EXHX@)!$',
*   100,0,0)
C
  IF (I80.EQ.4) CALL ALGPLT (DHFMIN,DHFMAX,5.,YORIG,YCYCLE)
  IF (I80.EQ.4) CALL YLGAXS (YORIG,YCYCLE,5.,
*   'HF CONCENTRATION IN COMPARTMENT@ (LB/FT&EH.8@3&EXHX@)!$',
*   100,0,0)
C
60 CONTINUE
C
  CALL THKCRV (0.05)
  CALL NOCHEK
C
C PLOT 1. CUMULATIVE URANIUM RELEASED (LB) VS CUMULATIVE TIME OF
C   TRANSIENT (SEC).
C
  IF (I80.EQ.1) CALL CURVE (TIME,UTOT,IMAX,0)
C
C PLOT 2. CUMULATIVE HF RELEASED (LB) VS CUMULATIVE TIME OF TRANSIENT
C   (SEC).
C
  IF (I80.EQ.2) CALL CURVE (TIME,HFTOT,IMAX,0)
C
C PLOT 3. URANIUM CONCENTRATION IN COMPARTMENT (LB/FT**3) VS
C   CUMULATIVE TIME OF TRANSIENT (SEC).
C
  IF (I80.EQ.3) CALL CURVE (TIME,DENU,IMAX,0)
C
C PLOT 4. HF CONCENTRATION IN COMPARTMENT (LB/FT**3) VS CUMULATIVE
C   TIME OF TRANSIENT (SEC).
C
  IF (I80.EQ.4) CALL CURVE (TIME,DENHF,IMAX,0)
C
C PLOT 5. TEMPERATURE IN COMPARTMENT (DEG F) VS CUMULATIVE TIME OF
C   TRANSIENT (SEC).
C
  IF (I80.EQ.5) CALL CURVE (TIME,T,IMAX,0)
C
C PLOT 6. PRESSURE IN COMPARTMENT (PSIA) VS CUMULATIVE TIME OF
C   TRANSIENT (SEC).
C

```

```

      IF (I80.EQ.6) CALL CURVE (TIME,P,IMAX,0)
C
C DRAWING NUMBERS.
C
      DO 70 I70=1,4
C
          NUMBER(I70)=DWGNUM(I80,I70)
C
      70 CONTINUE
C
          CALL HEIGHT (0.1)
          CALL MESSAG (NUMBER,100,3.2,5.1)
C
          CALL ENDPL(0)
C
      80 CONTINUE
C
          CALL DONEPL
C
          STOP
C
C*****
C
C  FORMAT STATEMENTS
C  =====
C
      4900 FORMAT (4A5)
C
C*****
C
      END

```

## A.6 CYLPLT - A Plotting Program for CYLIND Results

```

C THIS PROGRAM PLOTS OUTPUT FROM CYLIND.
C
C THIS PROGRAM USES DISSPLA (VERSION 9.0) SUBROUTINES FOR PLOTTING.
C DISSPLA IS A PRODUCT OF INTEGRATED SOFTWARE SYSTEMS CORPORATION OF
C SAN DIEGO, CALIFORNIA. DOCUMENTATION WAS COPYRIGHTED IN 1981.
C
C*****
C
C  INITIAL STATEMENTS
C  =====
C
      IMPLICIT REAL*4 (A-H,J-Z)
C
      DIMENSION TIME(1000), MSOL(1000), MLIQ(1000), MTOT(1000),
*          TCYL(1000), PCYL(1000), MSSRTS(1000), MSSRTL(1000),
*          MSFLRT(1000), TFIN(1000), BSLNX(2), BSLNY(2), AX(2),
*          AY(2), BX(2), BY(2), CX(2), CY(2), DX(2), DY(2)
      DIMENSION DWGNUM(4,4), NUMBER(4)
C

```

```

C*****
C
C READ STATEMENTS
C =====
C
C THE FOLLOWING DO LOOP BYPASSES HEADINGS IN THE INPUT FILE WHICH IS
C THE PRIMARY CYLIND OUTPUT FILE.
C
C     DO 10 I10=1,6
C
C         READ (30,3010) IDUM
C
C 10 CONTINUE
C
C     IMAX = 0
C
C CODING BETWEEN "20 CONTINUE" AND "40 CONTINUE" READS OR DEVELOPS DATA
C TO BE PLOTTED.
C
C 20 CONTINUE
C
C     IMAX = IMAX + 1
C
C     READ (30,3020,END=40) TIME(IMAX), MSOL(IMAX), MLIQ(IMAX),
*     MTOT(IMAX), TCYL(IMAX), PCYL(IMAX), MSSRTS(IMAX),
*     MSSRTL(IMAX), MSFLRT(IMAX), PFIN, TFIN(IMAX)
C
C     MLIQ(IMAX) = MSOL(IMAX) + MLIQ(IMAX)
C
C     MSSRTL(IMAX) = MSSRTS(IMAX) + MSSRTL(IMAX)
C
C     IF (IMAX.NE.1) GO TO 30
C
C     TMIN = TFIN(IMAX)
C     TMAX = TFIN(IMAX)
C
C     GO TO 20
C
C 30 CONTINUE
C
C     IF (TFIN(IMAX).LT.TMIN) TMIN = TFIN(IMAX)
C     IF (TFIN(IMAX).GT.TMAX) TMAX = TFIN(IMAX)
C
C     GO TO 20
C
C 40 CONTINUE
C
C READ DRAWING NUMBERS.
C
C     DO 50 I50=1,4
C
C         READ (31,3110) (DWGNUM(I50,I), I=1,4)
C
C 50 CONTINUE

```

```

C
C   IMAX = IMAX - 1
C
C   BSLNX(1) = 0.
C   BSLNX(2) = TIME(IMAX)
C   BSLNY(1) = 0.
C   BSLNY(2) = 0.
C
C*****
C
C PLOTTING COMMANDS
C =====
C
C   CALL COMPRS
C
C   DO 160 I160=1,4
C
C SET UP AXES.
C
C   CALL RESET ('ALL')
C   CALL NOBRDR
C   CALL GRACE (0.)
C   CALL AREA2D(5.,5.)
C   CALL FRAME
C   CALL DUPLX
C
C   CALL XREVTK
C   CALL YREVTK
C   CALL YAXANG(0.0)
C
C   CALL MX1ALF('STANDARD','!')
C   CALL MX2ALF('L/CSTD','@')
C   CALL MX3ALF('INSTRUCTION','&')
C
C   CALL INTAXS
C
C   CALL XNAME ('CUMULATIVE TIME OF TRANSIENT@ (SEC)!$',100)
C   CALL AXSPLT (0.,TIME(IMAX),5.,XORIG,XSTEP,XAXIS)
C   XMAX = XORIG + XSTEP*XAXIS
C
C   IF (I160.NE.1) GO TO 60
C
C   CALL YNAME ('MASS OF UF&LH.8@6&LXHX! IN CYLINDER@ (LB)!$',100)
C   CALL AXSPLT (0.,MTOT(1),5.,YORIG,YSTEP,YAXIS)
C
C   GO TO 90
C
C 60 CONTINUE
C
C   IF (I160.NE.2) GO TO 70
C
C   CALL YNAME ('MASS RELEASE RATE OF UF&LH.8@6&LXHX@ (LB/SEC)!$',100)
C   CALL AXSPLT (0.,MSFLRT(1),5.,YORIG,YSTEP,YAXIS)
C

```

```

      GO TO 90
C
70 CONTINUE
C
      IF (I160.NE.3) GO TO 80
C
      CALL YNAME ('UF&LH.8@6&LXHX! TEMPERATURE IN CYLINDER@
* (&EH.5@0&EXHX!F@)!$',100)
      CALL AXSPLT (TCYL(IMAX),TCYL(1),5.,YORIG,YSTEP,YAXIS)
C
      GO TO 90
C
80 CONTINUE
C
      CALL YNAME ('UF&LH.8@6&LXHX! EXHAUST TEMPERATURE@
* (&EH.5@0&LXHX!F@)!$',100)
C
      IF (ABS(TMAX-TMIN).LT.1.) TMIN = FLOAT(IFIX(TMIN))
      IF (ABS(TMAX-TMIN).LT.1.) TMAX = FLOAT(IFIX(TMAX + 2.))
C
      CALL AXSPLT (TMIN,TMAX,5.,YORIG,YSTEP,YAXIS)
C
90 CONTINUE
C
      YMAX = YORIG + YSTEP*YAXIS
C
      CALL GRAF (XORIG,XSTEP,XMAX,YORIG,YSTEP,YMAX)
C
      XFACT = (XMAX-XORIG)/5.
      YFACT = (YMAX-YORIG)/5.
C
      CALL THKCRV (0.03)
C
      CALL NOCHEK
C
      IF (I160.NE.1) GO TO 100
C
C PLOT 1. MASS OF UF6 IN CYLINDER (LB) VS CUMULATIVE TIME OF TRANSIENT
C (SEC).
C
      CALL CURVE (TIME,MTOT,IMAX,0)
      CALL RESET ('THKCRV')
C
      CALL DOT
      CALL CURVE (TIME,MLIQ,IMAX,0)
C
      CALL CHNDOT
      CALL CURVE (TIME,MSOL,IMAX,0)
      CALL RESET ('CHNDOT')
C
      CALL SHDPAT (45350)
      CALL SHDCRV (BSLNX,BSLNY,2,TIME,MSOL,IMAX)
      CALL SHDPAT (135190)
      CALL SHDCRV (TIME,MSOL,IMAX,TIME,MLIQ,IMAX)

```



```
      CALL SHDPAT (45590)
      CALL SHDCRV (TIME, MLIQ, IMAX, TIME, MTOT, IMAX)
C
      GO TO 110
C
100 CONTINUE
C
      IF (I160.NE.2) GO TO 120
C
C PLOT 2. MASS RELEASE RATE OF UF6 (LB/SEC) VS CUMULATIVE TIME OF
C TRANSIENT (SEC).
C
      CALL CURVE (TIME,MSFLRT,IMAX,0)
      CALL RESET ('THKCRV')
C
      CALL DOT
      CALL CURVE (TIME,MSSRTL,IMAX,0)
C
      CALL CHNDOT
      CALL CURVE (TIME,MSSRTS,IMAX,0)
      CALL RESET ('CHNDOT')
C
      CALL SHDPAT (45350)
      CALL SHDCRV (BSLNX, BSLNY, 2, TIME, MSSRTS, IMAX)
      CALL SHDPAT (135190)
      CALL SHDCRV (TIME, MSSRTS, IMAX, TIME, MSSRTL, IMAX)
      CALL SHDPAT (45590)
      CALL SHDCRV (TIME, MSSRTL, IMAX, TIME, MSFLRT, IMAX)
C
110 CONTINUE
C
C LEGEND FOR PLOTS 1 AND 2.
C
      AX(1) = 2.5*XFACT
      AX(2) = 3.4*XFACT
      AY(1) = 4.90*YFACT
      AY(2) = AY(1)
C
      BX(1) = AX(1)
      BX(2) = AX(2)
      BY(1) = 4.62*YFACT
      BY(2) = BY(1)
C
      CX(1) = AX(1)
      CX(2) = AX(2)
      CY(1) = 4.34*YFACT
      CY(2) = CY(1)
C
      DX(1) = AX(1)
      DX(2) = AX(2)
      DY(1) = 4.06*YFACT
      DY(2) = DY(1)
C
      CALL THKCRV (0.03)
```

```

CALL CURVE (AX, AY, 2, 0)
CALL RESET ('THKCRV')
CALL CURVE (DX, DY, 2, 0)
CALL DOT
CALL CURVE (BX, BY, 2, 0)
CALL CHNDOT
CALL CURVE (CX, CY, 2, 0)
C
CALL RESET ('CHNDOT')
C
CALL SHDPAT (45350)
CALL SHDCRV (DX, DY, 2, CX, CY, 2)
CALL SHDPAT (135190)
CALL SHDCRV (CX, CY, 2, BX, BY, 2)
CALL SHDPAT (45590)
CALL SHDCRV (BX, BY, 2, AX, AY, 2)
C
CALL MESSAG ('UF&LH.8@6&LXHX! VAPOR$',100,3.5,4.69)
CALL MESSAG ('UF&LH.8@6&LXHX! LIQUID$',100,3.5,4.41)
CALL MESSAG ('UF&LH.8@6&LXHX! SOLID$',100,3.5,4.13)
C
GO TO 140
C
120 CONTINUE
C
IF (I160.NE.3) GO TO 130
C
PLOT 3. CURVE 1: TEMPERATURE IN CYLINDER (DEG F) VS CUMULATIVE TIME
C OF TRANSIENT (SEC).
C
CALL CURVE (TIME,TCYL,IMAX,0)
C
LEGEND FOR PLOT 3 (CURVE 1).
C
AX(1) = 2.5*XFACT
AX(2) = 3.4*XFACT
AY(1) = 4.79*YFACT + YORIG
AY(2) = AY(1)
C
CALL CURVE (AX, AY, 2, 0)
C
CALL MESSAG ('TEMPERATURE$',100,3.5,4.72)
C
PLOT 3. CURVE 2: VAPOR PRESSURE OF UF6 IN CYLINDER (PSIA) VS
C CUMULATIVE TIME OF TRANSIENT(SEC).
C
CALL AXSPLT (PCYL(IMAX),PCYL(1),5.,YORIG,YSTEP,YAXIS)
C
YMAX = YORIG + YSTEP*YAXIS
C
CALL YGRAXS (YORIG,YSTEP,YMAX,5.,'VAPOR PRESSURE OF
* UF&LH.8@6&LXHX! IN CYLINDER@ (PSIA)!$',-100,5.,0.)
C
CALL CHNDOT

```

```

C      CALL CURVE (TIME,PCYL,IMAX,0)
C
C      LEGEND FOR PLOT 3 (CURVE 2).
C
C      AY(1) = 4.61*(YMAX-YORIG)/5. + YORIG
C      AY(2) = AY(1)
C
C      CALL CURVE (AX, AY, 2, 0)
C
C      CALL MESSAG ('PRESSURE$',100,3.5,4.51)
C
C      GO TO 140
C
C 130 CONTINUE
C
C PLOT 4.  EXHAUST TEMPERATURE (DEG F) VS CUMULATIVE TIME OF TRANSIENT
C         (SEC).
C
C      CALL CURVE (TIME,TFIN,IMAX,0)
C
C      CALL MESSAG ('EXHAUST PRESSURE$',100,3.0,4.72)
C      CALL MESSAG ('    = $',100,3.0,4.51)
C      CALL REALNO (PFIN,2,'ABUT','ABUT')
C      CALL MESSAG ('@ PSIA!$',100,'ABUT','ABUT')
C
C 140 CONTINUE
C
C DRAWING NUMBERS.
C
C      DO 150 I150=1,4
C
C          NUMBER(I150) = DWGNUM(I160,I150)
C
C 150 CONTINUE
C
C      CALL HEIGHT (0.1)
C      CALL MESSAG (NUMBER, 100, 3.2, 5.1)
C
C      CALL ENDPL(0)
C
C 160 CONTINUE
C
C      CALL DONEPL
C
C      STOP
C
C *****
C
C  FORMAT STATEMENTS
C  =====
C
C 3010 FORMAT (I1)
C

```

```
3020 FORMAT (F7.0,1X,2F8.1,8X,F8.1,2F8.3,25X,2F8.3,8X,3F8.3)
C
3110 FORMAT (4A5)
C
C*****
C
      END
```

## Appendix B LISTINGS OF SUBROUTINES

This appendix contains listings of all subroutines required by the main programs, FODRFT, INDRFT, BATCH, and CYLIND. These subroutines are arranged alphabetically by subroutine name. Several UF<sub>6</sub> physical properties subroutines described in the text but not required by the aforementioned main programs are also included in this appendix. Table B.1 is a summary of STOPS that may occur during execution of programs using these subroutines. Note that subroutines called by COMPLT and CYLPLT are DISSPLA version 9.0 subroutines.\*

---

\*For information on DISSPLA, contact Integrated Software Systems Corporation, 10505 Sorrento Valley Road, San Diego, CA, 92121.

**Table B.1. Causes for program termination**

STOP	Subroutine	Cause
STOP01	COMPRT	100 iterations without temperature-enthalpy convergence in compartment
STOP02	INTMEB	New estimate of temperature inside cyclinder exceeds 250°F (upper limit based on DOE regulations, see Table 8) or is less than the triple point when UF <sub>6</sub> condensate is known to be liquid
STOP03	INTMEB	20 iterations without temperature-enthalpy convergence; UF <sub>6</sub> condensate is liquid
STOP04	INTMEB	20 iterations without temperature-enthalpy convergence; UF <sub>6</sub> condensate is solid
STOP05	INTMEB	New estimate of temperature inside cyclinder is less than 0°F (arbitrary lower limit) or is greater than the triple point when UF <sub>6</sub> condensate is known to be solid
STOP06	LEVEL	100 iterations without convergence on UF <sub>6</sub> vapor-liquid interface level (not bounded)
STOP07	LEVEL	100 iterations without convergence on UF <sub>6</sub> vapor-liquid interface level (bounded)
STOP11	LEVEL	UF <sub>6</sub> solid-vapor interface level above hole
STOP12	LEVEL	HF-H <sub>2</sub> O equilibrium partitioning did not converge in 100 iterations
STOP13	PIPSYS	Pressure drop-pipe length calculation did not converge within 100 iterations
STOP14	PIPSYS	Pressure drop calculation across a contraction did not converge within 100 iterations
STOP15	STERM	ITYPE (release type identifier) not recognized

**B.1 BREACH**

SUBROUTINE BREACH (G)

C THIS SUBROUTINE CALCULATES THE MASS VELOCITY, IN UNITS OF LBS/SEC/  
 C FT\*\*2, OF UF6 ESCAPING FROM A VESSEL THROUGH A BREACH OR HOLE IN THE  
 C VESSEL WALL. THE INSIDE TEMPERATURE (DEG F) AND PRESSURE (PSIA), THE  
 C OUTSIDE PRESSURE (PSIA), AND THE INITIAL MASS FRACTIONS OF VAPOR,  
 C LIQUID, AND SOLID UF6 ARE KNOWN. THE MASS VELOCITY IS CALCULATED.

C  
 C ALPHA, BETA, DELTA, GAMMA ARE CONSTANTS USED IN DIFFERENT  
 C FORMS OF THE BASIC PRESSURE DROP EQUATION RELATING CHANGE  
 C IN PRESSURE TO MASS VELOCITY AND TO SPECIFIC  
 C VOLUME. THEY ARE SET IN BREACH AND PASSED TO THE CALLING  
 C PROGRAM FOR USE IN OTHER SUBROUTINES THROUGH THE LABELED  
 C BLOCK COMMON /CNSTNT/.

C  
 C EPSLN IS A CONVERGENCE CRITERION ALSO SET HERE AND PASSED  
 C THROUGH THE LABELED BLOCK COMMON /CNSTNT/.

C  
 C INPUT VARIABLES, VALUES PROVIDED BY CALLING PROGRAM.

C  
 C ISEN INDEX FOR CONSTANT ENTROPY/CONSTANT ENTHALPY  
 C ISEN=0, ASSUME CONSTANT ENTROPY FLASH  
 C ISEN=1, ASSUME CONSTANT ENTHALPY FLASH  
 C IPIG NUMBER OF ELEMENTS IN RELEASE PATHWAY:  
 C IPIG=2, PATHWAY IS A BREACH OR HOLE.  
 C IPIG>2, PATHWAY IS A PIPE AND FIXTURE SYSTEM.  
 C PIGRAY ARRAY OF VALUES DESCRIBING THE RELEASE PATHWAY.  
 C EACH PATHWAY ELEMENT CORRESPONDS TO ONE ROW OF  
 C THE ARRAY. SPECIAL VALUES INCLUDE  
 C PIGRAY(IPIG,3), THE AMBIENT PRESSURE IN PSIA.  
 C PIGRAY IS MORE FULLY DESCRIBED IN THE  
 C CALLING PROGRAM AND INPUT DATA FILES.  
 C PCYL PRESSURE OF MASS ENTERING RELEASE PATHWAY, PSIA  
 C TCYL TEMPERATURE OF MASS ENTERING PATHWAY, DEGREES F  
 C PTRIPL, PRESSURE IN PSIA AND TEMPERATURE IN DEGREES F,  
 C TTRIPL RESPECTIVELY, FOR THE TRIPLE POINT CONDITION,  
 C INPUT FROM THE CALLING PROGRAM  
 C XUCYL VAPOR MASS FRACTION ENTERING PATHWAY  
 C XLCYL MASS FRACTION OF THE NON-VAPOR MASS  
 C WHICH IS LIQUID ENTERING PATHWAY  
 C MW MOLECULAR WEIGHT OF UF6, LB MASS/LB-MOLE

C  
 C INTERNAL VARIABLES, USED ONLY IN BREACH AND ITS SUBROUTINES.

C  
 C PINT INTERMEDIATE PRESSURE, PRESSURE-DROP-CONTROLLED  
 C FLOW, PSIA  
 C TINT INTERMEDIATE TEMPERATURE, PDC FLOW, DEGREES F  
 C XVINT VAPOR MASS FRACTION AT INTERMEDIATE CONDITIONS  
 C IN PDC FLOW  
 C XLINT MASS FRACTION OF THE NON-VAPOR PHASE WHICH IS  
 C LIQUID AT INTERMEDIATE CONDITIONS IN PDC FLOW

C RHOVI, DENSITIES OF VAPOR, LIQUID, AND SOLID,  
 C RHO LI, RESPECTIVELY, AT INTERMEDIATE CONDITIONS,  
 C RHOSI LB MASS/FT\*\*3  
 C VIBAR SPECIFIC VOLUME OF MASS IN RELEASE PATHWAY AT  
 C INTERMEDIATE CONDITIONS, FT\*\*3/LB MASS  
 C ICHECK INTEGER VARIABLE WHICH CONTROLS PROGRAM FLOW  
 C PUPPER, UPPER AND LOWER LIMITS ON PRESSURE IN PSIA  
 C PLOWER FOR INTERVAL HALVING SEARCH TECHNIQUE  
 C P2 PRESSURE IN PSIA ONLY SLIGHTLY LOWER THAN  
 C THE CHOKED FLOW PRESSURE. THE SMALL PRESSURE  
 C DIFFERENCE AND THE CORRESPONDING SMALL  
 C DIFFERENCE IN SPECIFIC VOLUME ARE USED TO  
 C APPROXIMATE THE DERIVATIVE OF PRESSURE WITH  
 C RESPECT TO SPECIFIC VOLUME AT CHOKED FLOW  
 C CONDITIONS.  
 C T2 TEMPERATURE IN DEGREES F CORRESPONDING TO P2  
 C XV2 VAPOR MASS FRACTION CORRESPONDING TO P2  
 C XL2 MASS FRACTION OF THE NON-VAPOR PHASE WHICH IS  
 C LIQUID AT P2, T2  
 C V2BAR SPECIFIC VOLUME IN FT\*\*3/LB MASS CORRESPONDING  
 C TO P2  
 C GMAX CHOKED FLOW MASS VELOCITY, LB MASS/S/FT\*\*2,  
 C EVALUATED AT CURRENT GUESS FOR P1, T1 CONDITIONS  
 C PCHECK PRESSURE IN PSIA PREDICTED WHEN CHOKED FLOW MASS  
 C VELOCITY IS USED IN PDC FLOW EQUATION BETWEEN  
 C CYLINDER CONDITIONS AND P1, T1 CONDITIONS. WHEN  
 C GMAX CORRESPONDS TO P1, T1 CONDITIONS, PCHECK  
 C EQUALS P1.

C OUTPUT VARIABLES, VALUES SET BY BREACH FOR CALLING PROGRAM.

C G MASS VELOCITY THROUGH THE HOLE, LB MASS/S/FT\*\*2

C \* \* \* \* \*  
 C \* NOTE! PRESSURE-DROP-CONTROLLED MASS VELOCITY (PDC G) \*  
 C \* IS A FUNCTION OF CONDITIONS IN THE CYLINDER, \*  
 C \* INTERMEDIATE CONDITIONS, AND AMBIENT CONDITIONS. \*  
 C \* CHOKED FLOW G IS DETERMINED BY MATCHING CRITERIA FOR \*  
 C \* PDC G FROM CYLINDER CONDITIONS TO THE CHOKED FLOW \*  
 C \* CONDITIONS WITH THE CHOKED FLOW EQUATION, WHICH \*  
 C \* RELATES MAXIMUM G TO THE DERIVATIVE OF PRESSURE WITH \*  
 C \* RESPECT TO SPECIFIC VOLUME AT CHOKED FLOW CONDITIONS. \*  
 C \* THE SMALLER VALUE, PDC G OR CHOKED FLOW G, IS THEN \*  
 C \* OUTPUT AS THE BREACH MASS VELOCITY. \*  
 C \* \* \* \* \*

C T1 TEMPERATURE IN DEGREES F CORRESPONDING TO THE  
 C INTERMEDIATE OR CHOKED FLOW CONDITIONS  
 C P1 PRESSURE IN PSIA CORRESPONDING TO THE  
 C INTERMEDIATE OR CHOKED FLOW CONDITIONS  
 C XV1 VAPOR MASS FRACTION AT T1, P1  
 C XL1 MASS FRACTION OF THE NON-VAPOR PHASE AT T1, P1  
 C WHICH IS LIQUID  
 C VIBAR SPECIFIC VOLUME AT T1, P1

```

C      IBRCH      INDEX OUTPUT CHARACTERIZING BREACH MASS VELOCITY
C                  =1, CHOKED FLOW CONTROLS THE MASS VELOCITY
C                  =2, PDC FLOW CONTROLS THE MASS VELOCITY
C
C THIS SUBROUTINE IS WRITTEN IN DOUBLE PRECISION. ALL INTEGER VARIABLE
C NAMES START WITH 'I'.
C
C      IMPLICIT REAL*8 (A-H,J-Z)
C
C NAMED COMMON BLOCKS TRANSFER MOST INPUTS FROM THE CALLING PROGRAM AND
C MOST OUTPUTS CALCULATED BY THE BREACH SUBROUTINE.
C
C      COMMON /ICOMON/ ISEN, IPIG, IBRCH, IGEXIT
C      COMMON /GMTRY / PIGRAY
C      COMMON /CONCYL/ PCYL,TCYL,XVCYL,XLCYL,MW
C      COMMON /CONENT/ P1,T1,XV1,XL1,U1BAR
C      COMMON /CNSTNT/ ALPHA,BETA,DELTA,GAMMA,EPSLN
C      COMMON /TRIPLE/ TTRIPL,PTRIPL
C
C AN ARRAY IS DIMENSIONED WHICH CONTAINS DESCRIPTIVE VALUES FOR THE
C RELEASE PATHWAY, MODELED AS AN INFINITESIMAL LENGTH BETWEEN ENTRANCE
C AND EXIT PRESSURE LOSSES.
C
C      DIMENSION PIGRAY(99,3)
C
C FOUR RELATED CONSTANTS ARE USED IN THE VARIOUS PRESSURE DROP
C CORRELATIONS.
C
C      ALPHA = 4633.1D0
C      BETA  = ALPHA*4.D0/3.D0
C      DELTA = ALPHA*2.D0
C      GAMMA = ALPHA*4.D0
C
C DEFINE A SMALL NUMBER FOR CONVERGENCE TOLERANCE.
C
C      EPSLN = 1.D-6
C
C AN INTERMEDIATE PRESSURE INSIDE THE BREACH IS CALCULATED.
C
C      PINT = (PCYL*2.D0+PIGRAY(IPIG,3))/3.D0
C
C IN THE PRESENCE OF LIQUID, THIS INTERMEDIATE PRESSURE MUST BE
C AT OR ABOVE THE TRIPLE POINT. ADJUST PINT UPWARD IF NECESSARY.
C
C      IF (XVCYL.NE.1.D0.AND.
C      *   XLCYL.NE.0.D0.AND.
C      *   PINT.LT.PTRIPL) PINT = PTRIPL
C
C AT THIS PRESSURE A FLASH CALCULATION IS MADE TO DETERMINE THE
C INTERMEDIATE TEMPERATURE AND MASS FRACTIONS.
C
C      CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,PINT,ISEN,
C      *           XVINT,XLINT,TINT)
C

```



```

C  CALCULATE THE INTERMEDIATE SPECIFIC VOLUME.
C
C  THE DENSITIES OF EACH PHASE ARE REQUIRED.
C
C      CALL DENUF6 (TINT,PINT,MW,RHOSI,RHOLI,RHOVI)
C
C      VIBAR = XVINT/RHOVI+(1.00-XVINT)*XLINT/RHOLI
C      *      +(1.00-XVINT)*(1.00-XLINT)/RHOSI
C
C  CALCULATE THE MASS VELOCITY LIMITED BY PRESSURE DROP.
C
C      G      = SQRT(DELTA*(PCYL-PIGRAY(IPIG,3))/1.500/VIBAR)
C
C  THE MASS VELOCITY MIGHT BE LIMITED BY CHOKED FLOW. EQUATION 119 MAY
C  BE USED TO EVALUATE THE CHOKED FLOW MASS VELOCITY. USE THE
C  INTERMEDIATE CONDITIONS AS FIRST GUESSES FOR THE CHOKED FLOW
C  CONDITIONS. ONCE THE CHOICE BETWEEN PDC FLOW AND CHOKED FLOW IS
C  MADE, THE STORAGE LOCATIONS FIRST DEFINED HERE WILL BE UPDATED WITH
C  THE CORRECT BREACH CONDITIONS FOR OUTPUT TO THE CALLING PROGRAM.
C
C      T1      = TINT
C      P1      = PINT
C      XV1     = XVINT
C      XL1     = XLINT
C      V1BAR   = VIBAR
C
C  THE ITERATION BELOW CLOSES TO A VALUE OF P1 EQUAL TO PCHECK. THE
C  METHOD USED IS CHANGED AS REQUIRED FROM DIRECT SUBSTITUTION TO
C  INTERVAL HALVING TO REGULA FALSI. THE FOLLOWING PARAMETERS ARE
C  INITIALIZED FOR BOOKKEEPING IN THE ITERATION.
C
C  INDICES FOR PROGRAM LOGIC CONTROL
C
C      ICHECK = 0
C      IPLUS  = 0
C
C  UPPER AND LOWER BOUNDS ON PRESSURE FOR INTERVAL HALVING.
C
C      CALL VPRUF6 (TCYL, PCYLEQ)
C
C      PUPPER = PCYLEQ
C      PLOWER = 0.00
C
C  UPPER AND LOWER BOUNDS ON PRESSURE FOR REGULA FALSI.
C
C      PUCHK  = 0.00
C      PLCHK  = 0.00
C
C 10 CONTINUE
C
C  THE PROGRAM BEGINS THE DETERMINATION OF GMAX, THE CHOKED FLOW MASS
C  VELOCITY, BY SETTING A SMALL (APPROXIMATELY INFINITESIMAL) PRESSURE
C  DIFFERENCE, STARTING FROM THE MOST RECENT GUESS FOR THE CHOKED FLOW
C  PRESSURE.

```

```

C
C      P2      = P1-1.D-3
C
C      AT THIS PRESSURE A FLASH CALCULATION IS MADE TO DETERMINE THE
C      DIFFERENTIAL TEMPERATURE AND MASS FRACTIONS.
C
C      FLASH BASIS FOR CHOKE FLOW CONDITION IS ISENTROPIC.
C
C      ISNGMX = 0
C
C      CALL FLASH (T1,P1,MW,XV1,XL1,P2,ISNGMX,XV2,XL2,T2)
C
C      CALCULATE THE DIFFERENTIAL SPECIFIC VOLUME. THE DENSITIES OF EACH
C      PHASE ARE REQUIRED.
C
C      CALL DENUF6 (T2,P2,MW,RHOS2,RHOL2,RHOV2)
C
C      V2BAR = XV2/RHOV2+(1.D0-XV2)*XL2/RHOL2
C      *      +(1.D0-XV2)*(1.D0-XL2)/RHOS2
C
C      THE CHOKED FLOW MASS VELOCITY CORRESPONDING TO THE LATEST GUESSES FOR
C      CHOKED FLOW TEMPERATURE AND PRESSURE IS CALCULATED.
C
C      GMAX   = SQRT(ALPHA*(P1-P2)/(V2BAR-V1BAR))
C
C      A CHECK IS REQUIRED TO SEE IF THE GUESSED PRESSURE FOR CHOKED FLOW
C      CORRESPONDS TO THE PDCPRESSURE CALCULATED USING GMAX, THE CYLINDER
C      PRESSURE, AND THE SPECIFIC VOLUME AT THE GUESSED PRESSURE. WHEN THE
C      GUESSED PRESSURE AND THE PDC PRESSURE DIFFER BY LESS THAN SOME
C      TOLERANCE CRITERION, THE CLCULATION OF GMAX IS COMPLETE.
C
C      PCHECK = PCYL-(GMAX**2.D0*V1BAR/GAMMA)
C
C      IF (PCHECK.GT.PCYLEQ) PCHECK = PCYLEQ
C
C      IF (DABS(PCHECK-P1).LT.(100.D0*EPSLN)
C      *      .OR.DABS(PUPPER-P1).LT.(EPSLN)) GO TO 40
C
C      IF THE MAXIMUM MASS VELOCITY FOR CHOKED FLOW IS NOT COMPATIBLE WITH
C      THE PREVIOUSLY CALCULATED CHOKED FLOW CONDITIONS, AN ITERATION IS
C      NECESSARY TO FIND THE ACTUAL CHOKED FLOW CONDITIONS OF PRESSURE,
C      TEMPERATURE, AND MASS VELOCITY.
C
C      IF (PCHECK.GT.P1) GO TO 20
C
C      ICHECK = 1
C
C      IF (PCHECK.GT.0.D0.AND.PLCHK.GT.0.D0) ICHECK = 3
C
C 20 CONTINUE
C
C      IF (ICHECK.GT.0) GO TO 60
C
C      PLOWER = P1

```

```

      PLCHK = PCHECK
      P1    = PCHECK
C
C 30 CONTINUE
C
C     CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,P1,ISEN,XV1,XL1,T1)
C
C     CALL DENUF6(T1,P1,MW,RHOS1,RHOL1,RHOV1)
C
C     V1BAR = XV1/RHOV1+(1.D0-XV1)*XL1/RHOL1
*      + (1.D0-XV1)*(1.D0-XL1)/RHOS1
C
C     GO TO 10
C
C 40 CONTINUE
C
C NOW THAT THE CHOKED FLOW MASS VELOCITY HAS BEEN CALCULATED THE LOWER
C OF THE TWO VALUES FOR MASS VELOCITY WILL BE RETURNED TO THE CALLING
C PROGRAM.
C
C     IF (GMAX-G) 50,120,120
C
C 50 CONTINUE
C
C CHOKED FLOW CONTROLS THE MASS VELOCITY.  THE CHOKED FLOW CONDITIONS
C ARE THE INTERMEDIATE CONDITIONS, SO P1, ETC., NEED NOT BE CHANGED.
C
C     G = GMAX
C
C     IBRCH = 1
C
C     GO TO 130
C
C 60 CONTINUE
C
C     IF (ICHECK.GT.1) GO TO 70
C
C     PUPPER = P1
C     PUCHK  = PCHECK
C
C     P1     = (PUPPER+PLOWER)/2.D0
C
C     ICHECK = 2
C
C     GO TO 80
C
C 70 CONTINUE
C
C     IF (ICHECK.GT.2) GO TO 90
C
C     PLOWER = P1
C     PLCHK  = PCHECK
C
C     P1     = (PLOWER+PUPPER)/2.D0

```

```
C
C 80 CONTINUE
C      GO TO 30
C
C 90 CONTINUE
C      IF (P1.GT.PCHECK) GO TO 100
C
C      PLOWER = P1
C      PLCHK = PCHECK
C
C      IF (ICHECK.EQ.4) IPLUS = 1
C
C      ICHECK = 4
C
C      GO TO 110
C
C 100 CONTINUE
C      PUPPER = P1
C      PUCHK = PCHECK
C
C 110 CONTINUE
C
C      P1      = (PUPPER*PLCHK-PLOWER*PUCHK)
C      *      / (PUPPER+PLCHK-PLOWER-PUCHK)
C
C      P1PLUS = 2.D0*P1-PLOWER
C
C      IF (IPLUS.EQ.1.AND.P1PLUS.LT.PUPPER) P1 = P1PLUS
C
C      IPLUS = 0
C
C      GO TO 30
C
C 120 CONTINUE
C
C      PDC FLOW CONTROLS THE MASS VELOCITY.  THE INTERMEDIATE CONDITIONS ARE
C      THE BREACH CONDITIONS. P1, ETC., ARE RESET FOR OUTPUT.
C
C      T1      = TINT
C      P1      = PINT
C      XV1     = XVINT
C      XL1     = XLINT
C      V1BAR   = VIBAR
C
C      IBRCH = 2
C
C 130 CONTINUE
C      RETURN
C      END
```

**B.2 COMPRT**

```

SUBROUTINE COMPRT (IC, INOUT, INODES)
C
C THIS SUBROUTINE PERFORMS A MASS AND ENERGY BALANCE FOR NODE IC. IT
C DETERMINES THE TEMPERATURE, PRESSURE, AND PHASE COMPOSITION AT THE
C END OF A TIME STEP. THE MASS AND ENERGY OF INLET AND OUTLET STREAMS
C ARE ADDED OR SUBTRACTED TO THE MASS AND ENERGY OF THE COMPARTMENT
C NODE, THEN COMPONENTS WITHIN THE NODE ARE ALLOWED TO REACT BEFORE THE
C FINAL CONDITIONS ARE EVALUATED.
C
C THE FOLLOWING VARIABLES ARE USED.
C
C INPUT VARIABLES
C
C IC          NODE NUMBER OF COMPARTMENT
C INOUT       MAXIMUM NUMBER OF THE NUMBER OF INLET STREAMS
C             AND THE NUMBER OF OUTLET STREAMS (LESS THAN OR
C             EQUAL TO 4)
C INODES      MAXIMUM NUMBER OF NODES ALLOWED, CORRESPONDING
C             TO THE NULL VECTOR
C
C COMMON BLOCK VARIABLES
C
C MASS      (30,9) COMPONENT MASS OR MASS RATE, LB OR LB/(DELT)
C TC        (30)  NODE TEMPERATURE, DEG F
C PC        (30)  NODE PRESSURE, PSIA
C TSURF     (30)  HEAT TRANSFER SURFACE TEMPERATURE, DEG F
C WMOL      (9)   COMPONENT MOLECULAR WEIGHT, LB/LB MOLE
C VOL       (30)  NODE VOLUME, FT**3
C H         (30)  NODE ENTHALPY OR ENTHALPY RATE, BTU OR
C             BTU/(DELT)
C QRATE     (30)  HEAT TRANSFER RATE TO COMPARTMENT ATMOSPHERE
C             FROM HEAT TRANSFER SURFACES, BTU/(DELT)
C QCOOL     (30)  COOLING RATE, BTU/SEC
C HTCDEF    (30)  HEAT TRANSFER COEFFICIENT, BTU/SEC-FT**2-DEG F
C HTAREA    (30)  SURFACE AREA FOR HEAT TRANSFER, FT**2
C IIN       (30,4) INLET STREAM NODE NUMBERS
C IOUT      (30,4) OUTLET STREAM NODE NUMBERS
C AMINLN    NATURAL LOG OF MINIMUM NUMBER ACCEPTABLE TO THE
C             COMPUTER
C TIME      CUMULATIVE TIME OF TRANSIENT SIMULATION, SEC
C DELT      TIME INTERVAL FOR TRANSIENT SIMULATION, SEC
C
C INTERNAL VARIABLES
C
C T         (3)   ESTIMATED FINAL TEMPERATURE, DEG F
C HDIF      (3)   DIFFERENCE BETWEEN ENTHALPY AT ESTIMATED FINAL
C             TEMPERATURE AND THE ACTUAL FINAL ENTHALPY, BTU
C HRXN      HEAT RELEASED BY REACTION, BTU
C HAVAIL    FINAL ENTHALPY, BTU
C ITEMP     INDEX FOR ITERATION VARIABLES T AND HDIF
C ICOUNT    COUNTER TO LIMIT NUMBER OF ITERATIONS
C TR        ABSOLUTE TEMPERATURE, DEG R

```

```

C      PUF6          VAPOR PRESSURE OF UF6, PSIA
C      MAXVAP       MAXIMUM AMOUNT OF UF6 THAT CAN BE CONTAINED AS
C                  VAPOR IN THE COMPARTMENT VOLUME AT THE ASSUMED
C                  TEMPERATURE BASED ON THE VAPOR PRESSURE OF UF6
C      NAIR         MOLES OF AIR
C      NH2O         MOLES OF WATER VAPOR
C      NHF          MOLES OF HF VAPOR BASED ON THE EFFECTIVE
C                  MOLECULAR WEIGHT OF THE POLYMERIZED VAPOR
C      NUF6         MOLES OF UF6 VAPOR
C      NTOT         TOTAL MOLES OF VAPOR IN THE COMPARTMENT
C      PTOT         TOTAL PRESSURE IN THE COMPARTMENT, PSIA
C      HTEST        ENTHALPY AT THE ESTIMATED FINAL TEMPERATURE, BTU
C      M            APPROXIMATE SLOPE OF HDIF VS T, BTU/DEG F

```

```

C      THE FOLLOWING SUBROUTINES ARE CALLED BY COMPRT.

```

```

C          DENTHL
C          PHASE
C          UPRUF6

```

```

C      THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED TO USE COMPRT.

```

```

C          DENUF6
C          HFPOLY
C          HHFH2O
C          HUF6
C          PHFH2O
C          ZUF6

```

```

C      IMPLICIT REAL*8 (A-H,J-Z)

```

```

C      DIMENSION T(3), HDIF(3)

```

```

C      COMMON /LBMASS/ MASS(30,9), DUM1
C      COMMON /COMPTP/ TC(30), PC(30), TSURF(30)
C      COMMON /MOLWT/ WMOL(9)
C      COMMON /VOLUME/ VOL(30), DUM2(61)
C      COMMON /ENTHAL/ H(30), QRATE(30), QCOOL(30), HTCDEF(30),
*          HTAREA(30)
C      COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C      COMMON /CONTRL/ AMINLN, TIME, DELT, DUM3, IDUM1, DUM4

```

```

C      SUM INLET AND OUTLET STREAM MASSES AND ENTHALPIES FOR THE TIME STEP.

```

```

C      DO 20 I20 = 1, INOUT

```

```

C          IF ((IIN(IC,I20)+IOUT(IC,I20)).EQ.(2*INODES)) GO TO 30

```

```

C          DO 10 I10 = 1,9

```

```

C              MASS(IC,I10) = MASS(IC,I10) + MASS(IIN(IC,I20),I10)
*              - MASS(IOUT(IC,I20),I10)

```

```

C      10      CONTINUE

```

```

C
C      H(IC) = H(IC) + H(IIN(IC,I20)) - H(IOUT(IC,I20))
C
C      20 CONTINUE
C
C      30 CONTINUE
C
C      PLACE ALL COMPONENTS IN THE VAPOR PHASE.
C
C      MASS(IC,3) = MASS(IC,2) + MASS(IC,3)
C      MASS(IC,5) = MASS(IC,4) + MASS(IC,5)
C      MASS(IC,8) = MASS(IC,6) + MASS(IC,7) + MASS(IC,8)
C
C      MASS(IC,2) = 0.D0
C      MASS(IC,4) = 0.D0
C      MASS(IC,6) = 0.D0
C      MASS(IC,7) = 0.D0
C
C      REACT UF6 WITH H2O TO THE EXTENT POSSIBLE.
C
C      UF6(V) + 2 H2O(V) --> UO2F2(S) + 4 HF(V)
C
C      HRXN = 25,199 BTU/LB MOLE H2O AT 77 F AND 1 ATM
C
C      HRXN = 0.D0
C
C      IF (MASS(IC,8).EQ.0.D0.OR.MASS(IC,3).EQ.0.D0) GO TO 50
C
C      IF ((MASS(IC,8)/MASS(IC,3)).LT.(WMOL(8)/(2.D0*WMOL(3)))) GO TO 40
C
C      THE FOLLOWING MASS AND ENERGY BALANCE IS BASED ON H2O CONTROLLING THE
C      EXTENT OF REACTION.
C
C      MASS(IC,8) = MASS(IC,8) - MASS(IC,3)*WMOL(8)/(2.D0*WMOL(3))
C      MASS(IC,9) = MASS(IC,9) + MASS(IC,3)*WMOL(9)/(2.D0*WMOL(3))
C      MASS(IC,5) = MASS(IC,5) + MASS(IC,3)*2.D0*WMOL(4)/WMOL(3)
C
C      HRXN      = 25.199D3*MASS(IC,3)/WMOL(3)
C
C      MASS(IC,3) = 0.D0
C
C      GO TO 50
C
C      40 CONTINUE
C
C      THE FOLLOWING MASS AND ENERGY BALANCE IS BASED ON UF6 CONTROLLING THE
C      EXTENT OF REACTION.
C
C      MASS(IC,3) = MASS(IC,3) - MASS(IC,8)*2.D0*WMOL(3)/WMOL(8)
C      MASS(IC,9) = MASS(IC,9) + MASS(IC,8)*WMOL(9)/WMOL(8)
C      MASS(IC,5) = MASS(IC,5) + MASS(IC,8)*4.D0*WMOL(4)/WMOL(8)
C
C      HRXN      = 50.398D3*MASS(IC,8)/WMOL(8)
C

```

```

      MASS(IC,8) = 0.D0
C
C 50 CONTINUE
C
C EVALUATE HEAT TRANSFER TO THE COMPARTMENT ATMOSPHERE FROM HOT
C SURFACES.
C
      QRATE(IC) = HTCDEF(IC)*HTAREA(IC)*(TSURF(IC) - TC(IC))*DELTA
C
C CALCULATE THE TOTAL ENTHALPY IN THE COMPARTMENT AT THE END OF THE
C TIME STEP.
C
      HAVAIL = HRXN + H(IC) + QRATE(IC) - (QCOOL(IC)*DELTA)
C
C BEGIN ITERATIVE PROCEDURE TO FIND FINAL TEMPERATURE, PRESSURE, AND
C PHASE COMPOSITIONS. TEMPERATURE IS VARIED UNTIL ENTHALPY AGREES WITH
C HAVAIL.
C
      ITEMP = 1
C
      T(ITEMP) = TC(IC)
C
      HDIF(2) = 0.D0
C
      ICOUNT = 0
C
C 60 CONTINUE
C
      ICOUNT = ICOUNT + 1
C
C PLACE ALL COMPONENTS IN THE VAPOR PHASE.
C
      MASS(IC,3) = MASS(IC,2) + MASS(IC,3)
      MASS(IC,5) = MASS(IC,4) + MASS(IC,5)
      MASS(IC,8) = MASS(IC,6) + MASS(IC,7) + MASS(IC,8)
C
      MASS(IC,2) = 0.D0
      MASS(IC,4) = 0.D0
      MASS(IC,6) = 0.D0
      MASS(IC,7) = 0.D0
C
      TR = T(ITEMP) + 459.67D0
C
C DETERMINE IF ANY UF6 CONDENSES.
C
      IF (MASS(IC,8).LE.0.D0) GO TO 70
C
      CALL VPRUF6 (T(ITEMP), PUF6)
C
      MAXVAP = WMOL(8)*PUF6*VOL(IC)/10.73D0/TR
C
      IF (MASS(IC,8).LE.MAXVAP) GO TO 70
C
      IF (T(ITEMP).GT.147.306561D0) MASS(IC,7) = MASS(IC,8) - MAXVAP

```



```

C      IF (T(ITEMP).LE.147.306561D0) MASS(IC,6) = MASS(IC,8) - MAXVAP
C      MASS(IC,8) = MAXVAP
C
C 70 CONTINUE
C
C DETERMINE IF HF AND/OR H2O CONDENSE.
C
C      IF (MASS(IC,3).EQ.0.D0.AND.MASS(IC,5).EQ.0.D0) GO TO 80
C
C      CALL PHASE (T(ITEMP), IC)
C
C 80 CONTINUE
C
C ESTIMATE FINAL COMPARTMENT PRESSURE.
C
C      NAIR   = MASS(IC,1)/WMOL(1)
C      NH2O   = MASS(IC,3)/WMOL(3)
C      NHF    = MASS(IC,5)/WMOL(5)
C      NUF6   = MASS(IC,8)/WMOL(8)
C
C      NTOT   = NAIR + NH2O + NHF + NUF6
C
C      PTOT   = NTOT*10.73D0*TR/VOL(IC)
C
C EVALUATE ENTHALPY CORRESPONDING TO ESTIMATED TEMPERATURE AND COMPARE
C TO HAVAIL.
C
C      CALL DENTHL (T(ITEMP), PTOT, IC, HTEST)
C
C      HDIF(ITEMP) = HTEST - HAVAIL
C
C      IF (DABS(HDIF(ITEMP)).LT.DMAX1(1.D-3,DABS(HAVAIL*1.D-3)))
C *      GO TO 140
C
C      IF (ICOUNT.EQ.100) STOP01
C
C ESTIMATE NEW TEMPERATURE TO CONTINUE ITERATION.
C
C      IF (ITEMP.EQ.3) GO TO 120
C      IF (ITEMP.EQ.2) GO TO 100
C
C      IF (HDIF(1).LT.0.D0.AND.HDIF(2).GT.0.D0) GO TO 110
C
C      IF (HDIF(1).GT.0.D0) GO TO 90
C
C      ITEMP = 2
C
C      T(2)  = T(1) + 5.D0
C
C      GO TO 60
C
C 90 CONTINUE

```

```
C
  T(2)   = T(1)
  HDIF(2) = HDIF(1)
  T(1)   = T(2) - 5.D0
C
  GO TO 60
C
100 CONTINUE
C
  IF (HDIF(2).GT.0.D0) GO TO 110
C
  HDIF(1) = HDIF(2)
  T(1)   = T(2)
  T(2)   = T(1) + 5.D0
C
  GO TO 60
C
110 CONTINUE
C
  ITEMP  = 3
C
  M      = (HDIF(2) - HDIF(1))/(T(2) - T(1))
  T(3)   = T(2) - HDIF(2)/M
C
  GO TO 60
C
120 CONTINUE
C
  IF ((T(2) - T(1)).LT.1.D-3) GO TO 140
C
  IF (HDIF(3).GT.0.D0) GO TO 130
C
  HDIF(1) = HDIF(3)
  T(1)   = T(3)
C
  GO TO 110
C
130 CONTINUE
C
  HDIF(2) = HDIF(3)
  T(2)   = T(3)
C
  GO TO 110
C
140 CONTINUE
C
  THE MATERIAL AND ENERGY BALANCE HAS BEEN CLOSED FOR COMPARTMENT IC.
C
  TC(IC) = T(ITEMP)
  PC(IC) = PTOT
  H(IC)  = HAVAIL
C
  RETURN
C
  END
```

**B.3 CPUF6**

```

SUBROUTINE CPUF6 (TF, PSIA, MW, CPSOL, CPLIQ, CPVAP, CVVAP,
*                CPTOCV)
C
C THIS SUBROUTINE CALCULATES THE CONSTANT PRESSURE HEAT CAPACITIES OF
C UF6 SOLID, LIQUID, AND VAPOR, AS WELL AS THE CONSTANT VOLUME HEAT
C CAPACITY AND THE HEAT CAPACITY RATIO FOR THE VAPOR. THE FOLLOWING
C VARIABLES ARE USED.
C
C     TF      TEMPERATURE, DEG F
C     TR      ABSOLUTE TEMPERATURE, DEG R
C     TRSQ    TR**2
C     PSIA    PRESSURE, PSIA
C     MW      MOLECULAR WEIGHT, LB MASS/LB MOLE
C     CPSOL   CONSTANT PRESSURE HEAT CAPACITY OF THE SOLID,
C            BTU/LB MASS-DEG F
C     CPLIQ   CONSTANT PRESSURE HEAT CAPACITY OF THE LIQUID,
C            BTU/LB MASS-DEG F
C     CPVAP   CONSTANT PRESSURE HEAT CAPACITY OF THE VAPOR,
C            BTU/LB MASS-DEG F
C     CVVAP   CONSTANT VOLUME HEAT CAPACITY OF THE VAPOR,
C            BTU/LB MASS-DEG F
C     CPTOCV  HEAT CAPACITY RATIO
C     ZPSIA   VAPOR COMPRESSIBILITY FACTOR AT TF AND PSIA
C     Z1ATM   VAPOR COMPRESSIBILITY FACTOR AT TF AND 14.696 PSIA
C     ZT
C     ZP
C
C THE FOLLOWING SUBROUTINE IS CALLED.
C
C     ZUF6
C
C THE HEAT CAPACITY CORRELATIONS ARE BASED ON INFORMATION IN R. DEWITT,
C "URANIUM HEXAFLUORIDE: A SURVEY OF THE PHYSICO-CHEMICAL PROPERTIES,"
C GAT-280, GOODYEAR ATOMIC CORP., PORTSMOUTH, OHIO, JAN. 29, 1960,
C PAGES 56 - 64. THE HEAT CAPACITY OF THE VAPOR GIVEN BY THE CORRELA-
C TION IN GAT-280 IS FOR A PRESSURE OF 1 ATM. THE VAPOR CORRELATION
C GIVEN BELOW HAS BEEN MODIFIED USING THE MAGNUSON EQUATION OF STATE
C (SEE GAT-280, PAGES 97 - 101) AND THE DEPARTURE FUNCTION CORRELATIONS
C GIVEN IN R. C. REID, J. M. PRAUSNITZ, AND T. K. SHERWOOD, THE
C PROPERTIES OF GASES AND LIQUIDS, 3RD ED., MCGRAW-HILL BOOK COMPANY,
C 1977, PAGE 93, SO THAT BOTH SATURATED AND UNSATURATED VAPOR HEAT
C CAPACITIES CAN BE CALCULATED.
C
C     IMPLICIT REAL*8 (A-H,J-Z)
C
C     TR      = TF + 459.67D0
C
C     TRSQ    = TR**2
C
C THE HEAT CAPACITY OF THE SOLID IS GIVEN BY THE FOLLOWING CORRELATION
C WHICH IS ACCURATE WITHIN 1% BETWEEN -10 DEG F AND THE TRIPLE POINT
C (147.3 DEG F).

```

```

C
C     CPSOL = ( -5.70531D-2 + 2.55019D-4*TR
*           + ( 9.64563D3/TRSQ ) ) * ( 3.52D2/MW )
C
C     THE HEAT CAPACITY OF THE LIQUID IS GIVEN BY THE FOLLOWING CORRELATION
C     WHICH IS REPORTED TO HAVE AN ACCURACY OF 0.6% BETWEEN 147.3 AND 206.3
C     DEG F.
C
C     CPLIQ = ( 5.10057D-2 + 1.02633D-4*TR
*           + ( 6.13934D3/TRSQ ) ) * ( 3.52D2/MW )
C
C     CALCULATE THE VAPOR COMPRESSIBILITY FACTOR AT 14.696 PSIA AND AT
C     "PSIA" AS WELL AS ZP AND ZT AT "PSIA."
C
C     CALL ZUF6 (TF, 14.696D0, Z1ATM, 0.0D0, 0.0D0)
C
C     CALL ZUF6 (TF, PSIA, ZPSIA, ZP, ZT)
C
C     THE CONSTANT PRESSURE HEAT CAPACITY OF THE VAPOR IS GIVEN BY THE
C     FOLLOWING CORRELATION.
C
C     CPVAP = (9.21307D-2 + 1.25253D-5*TR
*           - ( 2.95171D3/TRSQ )
*           + 3.0939D-3 * ( (4.D0*ZPSIA-3.D0*ZPSIA**2)
*           - (4.D0*Z1ATM-3.D0*Z1ATM**2) ) ) * ( 3.52D2/MW )
C
C     THE CONSTANT VOLUME HEAT CAPACITY OF THE VAPOR IS GIVEN BY THE
C     FOLLOWING CORRELATION.
C
C     CVVAP = CPVAP - ( 1.9872D0 * ZT**2 ) / ( MW * ZP )
C
C     THE HEAT CAPACITY RATIO FOR THE VAPOR IS GIVEN BY
C
C     CPTOCV = CPVAP / CVVAP
C
C     RETURN
C
C     END

```

#### B.4 DENTHL

```

C     SUBROUTINE DENTHL (T, P, I, H)
C
C     THIS SUBROUTINE DETERMINES THE ENTHALPY OF A MIXTURE AT A GIVEN
C     TEMPERATURE WITH RESPECT TO A REFERENCE TEMPERATURE OF 77 F AND
C     THE FOLLOWING REFERENCE STATES:
C
C           AIR      VAPOR
C           H2O     VAPOR
C           HF      MONOMERIC VAPOR
C           UF6     VAPOR
C           UO2F2   SOLID
C

```

```

C THE FOLLOWING VARIABLES ARE USED:
C
C INPUT VARIABLES
C
C T TEMPERATURE, DEG F
C P TOTAL PRESSURE, PSIA
C I NODE NUMBER
C
C OUTPUT VARIABLE
C
C H ENTHALPY OF A MULTICOMPONENT MIXTURE WITH
C RESPECT TO THE REFERENCE TEMPERATURE AND STATES,
C BTU OR BTU/(DELT)
C
C COMMON BLOCK VARIABLES
C
C MASS (30,9) COMPONENT MASS OR MASS FLOW RATE WITHIN A NODE,
C LB (COMPARTMENT) OR LB/(DELT) (STREAM)
C WMOL (9) COMPONENT MOLECULAR WEIGHT, LB/LB MOLE
C C1 WEIGHT FRACTION OF HF MONOMER TO HF VAPOR
C C3 WEIGHT FRACTION OF HF TRIMER TO HF VAPOR
C C6 WEIGHT FRACTION OF HF HEXAMER TO HF VAPOR
C
C *****
C * * * * *
C * WARNING ! THIS SUBROUTINE RESETS THE VALUES OF C1, C3, AND *
C * C6. BE SURE THAT SUBSEQUENT CODING YIELDS APPROPRIATE VALUES *
C * OF C1, C3, AND C6 FOR LATER USE. *
C * * * * *
C *****
C
C WMBHF MOLECULAR WEIGHT OF HF MONOMER, LB/LB MOLE
C
C INTERNAL VARIABLES
C
C HA ENTHALPY OF AIR WITH RESPECT TO THE REFERENCE
C TEMPERATURE AND STATE, BTU OR BTU/(DELT)
C HMX ENTHALPY OF HF AND H2O WITH RESPECT TO THE
C REFERENCE TEMPERATURE AND STATES, BTU OR
C BTU/(DELT)
C HFH2OL COMBINED MASS OF LIQUID HF AND LIQUID H2O, LB
C OR LB/(DELT)
C HFH2OV COMBINED MASS OF HF VAPOR AND H2O VAPOR, LB
C OR LB/(DELT)
C WHFL WEIGHT FRACTION OF HF LIQUID IN A LIQUID MIXTURE
C OF HF AND H2O
C WHFV WEIGHT FRACTION OF HF VAPOR IN A VAPOR MIXTURE
C OF HF AND H2O
C HMXLT ENTHALPY OF THE HF-H2O LIQUID PHASE, BTU OR
C BTU/(DELT)
C HMXVT ENTHALPY OF THE HF-H2O VAPOR PHASE, BTU OR
C BTU/(DELT)
C HFH2OT COMBINED MASS OF HF AND H2O, LB OR LB/(DELT)
C WHFTOT WEIGHT FRACTION OF HF LIQUID AND VAPOR IN A TWO

```

```

C          PHASE MIXTURE OF HF AND H2O
C      HMXV77      REFERENCE ENTHALPY FOR THE HF-H2O SYSTEM,BTU
C                  OR BTU/(DELT)
C      UF6TOT      COMBINED MASS OF UF6 SOLID, LIQUID, AND VAPOR,I
C                  LB OR LB/(DELT)
C      H6ST        ENTHALPY OF SOLID UF6, BTU OR BTU/(DELT)
C      H6LT        ENTHALPY OF LIQUID UF6, BTU OR BTU/(DELT)
C      H6VT        ENTHALPY OF VAPOR UF6, BTU OR BTU/(DELT)
C      H6V77       REFERENCE ENTHALPY FOR UF6, BTU OR BTU/(DELT)
C      HHUF6       ENTHALPY OF UF6 WITH RESPECT TO THE REFERENCE
C                  TEMPERATURE AND STATE, BTU OR BTU/(DELT)
C      HUF2        ENTHALPY OF UO2F2 WITH RESPECT TO THE REFERENCE
C                  TEMPERATURE AND STATE, BTU OR BTU/(DELT)

```

```

C SUBROUTINES CALLED BY DENTHL ARE:

```

```

C             HHFH20
C             HUF6

```

```

C OTHER SUBROUTINES REQUIRED TO USE DENTHL ARE:

```

```

C             DENUF6
C             VPRUF6
C             ZUF6

```

```

C      IMPLICIT REAL*8 (A-H,J-Z)

```

```

C      COMMON / LBMASS / MASS(30,9)
C      COMMON / MOLWT  / WMOL(9)
C      COMMON / POLYMR / C1, C3, C6, WMBHF

```

```

C      CALCULATE THE ENTHALPY OF AIR WITH RESPECT TO THE REFERENCE
C      TEMPERATURE AND STATE.

```

```

C      HA      = MASS(I,1)*0.24073D0*(T-77.D0)

```

```

C      CALCULATE THE ENTHALPY OF THE HF-H2O SYSTEM WITH RESPECT TO THE
C      REFERENCE TEMPERATURE AND STATES.

```

```

C      HMX      = 0.D0

```

```

C      HFH20L = MASS(I,2) + MASS(I,4)
C      HFH20V = MASS(I,3) + MASS(I,5)

```

```

C      IF ((HFH20L+HFH20V) .LE. 0.D0) GO TO 30

```

```

C      IF (HFH20L.LE.0.D0) GO TO 10

```

```

C      WHFL    = MASS(I,4)/HFH20L

```

```

C      10 CONTINUE

```

```

C      IF (HFH20V.LE.0.D0) GO TO 20

```

```

      WHFV  = MASS(I,5)/HFH20V
C
20  CONTINUE
C
      CALL HHFH20 (T,WHFL,WHFV,HMXLT,HMXVT)
C
      HFH20T = HFH20L + HFH20V
C
      WHFTOT = (MASS(I,4) + MASS(I,5))/HFH20T
C
      C1     = 1.00
      C3     = 0.00
      C6     = 0.00
C
      CALL HHFH20 (77.00,0.00,WHFTOT,0.00,HMXV77)
C
      HMX    = (HFH20L*HMXLT + HFH20V*HMXVT) - HFH20T*HMXV77
C
30  CONTINUE
C
C  CALCULATE THE ENTHALPY OF UF6 WITH RESPECT TO THE REFERENCE
C  TEMPERATURE AND STATE.
C
      UF6TOT = MASS(I,6) + MASS(I,7) + MASS(I,8)
C
      CALL HUF6 (T,P,WMOL(8),H6ST,H6LT,H6VT)
C
      CALL HUF6 (77.00,14.69600,WMOL(8),0.00,0.00,H6V77)
C
      HHUF6  = (MASS(I,6)*H6ST
*           + MASS(I,7)*H6LT + MASS(I,8)*H6VT)
*           - UF6TOT*H6V77
C
C  CALCULATE THE ENTHALPY OF UO2F2 WITH RESPECT TO THE REFERENCE
C  TEMPERATURE AND STATE.
C
      HUF2   = MASS(I,9)*0.082100*(T-77.00)
C
C  CALCULATE THE ENTHALPY FOR NODE I WITH RESPECT TO THE REFERENCE
C  TEMPERATURE AND STATES.
C
      H      = HA + HMX + HHUF6 + HUF2
C
      RETURN
C
      END

```

## B.5 DENUF6

```

      SUBROUTINE DENUF6 (TF, PSIA, MW, DENSOL, DENLIQ, DENVAP)
C
C  THIS SUBROUTINE CALCULATES THE DENSITIES OF UF6 SOLID, LIQUID, AND
C  VAPOR. THE FOLLOWING VARIABLES ARE USED.

```

```

C
C   TF      TEMPERATURE, DEG F
C   TR      ABSOLUTE TEMPERATURE, DEG R
C   PSIA    PRESSURE, PSIA
C   MW      MOLECULAR WEIGHT, LB MASS/LB MOLE
C   Z       COMPRESSIBILITY FACTOR FOR THE VAPOR
C   DENSOL  DENSITY OF SOLID, LB MASS/FT**3
C   DENLIQ  DENSITY OF LIQUID, LB MASS/FT**3
C   DENVAP  DENSITY OF VAPOR, LB MASS/FT**3
C
C THE DENSITY CORRELATIONS USED ARE BASED ON R. DEWITT, "URANIUM
C HEXAFLUORIDE: A SURVEY OF THE PHYSICO-CHEMICAL PROPERTIES," GAT-280,
C GOODYEAR ATOMIC CORP., PORTSMOUTH, OHIO, JAN. 29, 1960, PAGES 17 -
C 24. A CORRELATION FOR SOLID DENSITY, BASED ON TABLE 7 OF GAT-280
C (EXCLUDING PRELIMINARY VALUES), WAS DERIVED BY W. R. WILLIAMS.
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   TR      = TF + 459.67D0
C
C THE DENSITY OF THE SOLID IS GIVEN BY THE FOLLOWING CORRELATION WHICH
C IS BASED ON DATA REPORTED OVER THE TEMPERATURE RANGE OF 69 TO 145
C DEG F.
C
C   DENSOL = ( 3.300D2 - 1.800D-1*TF ) * ( MW / 3.52D2 )
C
C THE DENSITY OF THE LIQUID IS GIVEN BY
C
C   DENLIQ = ( 2.506D2 - ( 1.241D-1 + 2.620D-4 * TF ) * TF )
C   *      * ( MW / 3.52D2 )
C
C EVALUATE THE COMPRESSIBILITY FACTOR FOR UF6 VAPOR.
C
C   CALL ZUF6 (TF, PSIA, Z, ZP, ZT)
C
C THE DENSITY OF THE VAPOR IS GIVEN BY
C
C   DENVAP = ( MW * PSIA * Z ) / ( 10.73D0 * TR )
C
C   RETURN
C
C   END

```

## B.6 DPFLOW

```

SUBROUTINE DPFLOW (IC)
C
C THIS SUBROUTINE EVALUATES THE MASS FLOW THROUGH A PRESSURE-DROP-
C CONTROLLED PATHWAY OVER A TIME STEP DELT. THE ENTHALPY CHANGE ASSOCI-
C ATED WITH THIS MASS FLOW IS ALSO DETERMINED. IF REVERSE FLOW OCCURS
C (WITH RESPECT TO THE NORMAL DIRECTION OF FLOW), THEN THE MASS IS
C TAKEN FROM THE PROPER NODE AND THE INDIVIDUAL COMPONENTS ARE ASSIGNED
C NEGATIVE VALUES.

```



C THE TOTAL MASS FLOW RATE IS ESTABLISHED USING A RESISTANCE TERM  
 C EVALUATED IN THE SUBROUTINE RESIST.  
 C  
 C NOTE THAT THIS SUBROUTINE IDENTIFIES THE TIME WHEN REVERSE FLOW  
 C BEGINS AND WHEN IT ENDS. PREVIOUS FLOW REVERSAL START AND STOP TIMES  
 C FOR A NODE ARE OVERWRITTEN AS SUBSEQUENT REVERSALS OCCUR.  
 C  
 C THIS SUBROUTINE USES THE FOLLOWING VARIABLES:  
 C  
 C INPUT VARIABLE  
 C  
 C IC                    NODE NUMBER FOR STREAM BEING EVALUATED  
 C  
 C COMMON BLOCK VARIABLES  
 C  
 C MASS    (30,9)    COMPONENT NODE MASS OR MASS FLOW RATE, LB  
 C                    (COMPARTMENT) OR LB/(DELTA) (STREAM)  
 C TC       (30)     NODE TEMPERATURE, DEG F  
 C PC       (30)     NODE PRESSURE, PSIA  
 C VOL      (30)     COMPARTMENT NODE VOLUME, FT\*\*3  
 C KRCOEF   (30)     RESISTANCE TERM, PSI-SEC\*\*2/LB-FT\*\*3  
 C H        (30)     NODE ENTHALPY OR ENTHALPY RATE, BTU OR  
 C                    BTU/(DELTA)  
 C IIN      (30,4)    NODE INPUT STREAM NUMBER  
 C IOUT     (30,4)    NODE OUTPUT STREAM NUMBER  
 C AMINLN            MINIMUM NATURAL LOG ACCEPTED BY THE COMPUTER  
 C TIME              TIME AT WHICH MASS AND ENTHALPY RATES ARE BEING  
 C                    DETERMINED, SEC  
 C DELT              TIME INTERVAL USED IN TRANSIENT SIMULATION, SEC  
 C TSTART   (30)     TIME AT WHICH FLOW REVERSAL BEGINS, SEC  
 C TSTOP    (30)     TIME AT WHICH FLOW REVERSAL ENDS, SEC  
 C  
 C INTERNAL VARIABLES  
 C  
 C CHECK    (30)     LOGICAL VARIABLE USED IN DETERMINING TSTART AND  
 C                    TSTOP  
 C DELP                PRESSURE DIFFERENCE BETWEEN NORMAL INLET AND  
 C                    OUTLET NODES, PSI  
 C INLET              ACTUAL INLET NODE TO STREAM  
 C MASS1              TOTAL MASS CONTAINED IN ACTUAL INLET NODE, LB  
 C DENS                DENSITY OF ACTUAL INLET STREAM, LB/FT\*\*3  
 C MASS2              TOTAL MASS FLOW RATE THROUGH STREAM, LB/(DELTA)  
 C FRAC                RATIO OF MASS FLOW THROUGH STREAM NODE TO TOTAL  
 C                    MASS IN ACTUAL INLET NODE -- A POSITIVE VALUE  
 C                    CORRESPONDS TO NORMAL FLOW AND A NEGATIVE VALUE  
 C                    TO REVERSE FLOW  
 C  
 C IMPLICIT REAL\*8 (A-H,J-Z)  
 C  
 C LOGICAL CHECK(30)  
 C  
 C COMMON /LBMASS/ MASS(30,9), DUM1  
 C COMMON /COMPTP/ TC(30), PC(30), DUM2(30)

```

COMMON /VOLUME/ VOL(30), KRCOEF(30), DUM3(31)
COMMON /ENTHAL/ H(30), DUM4(120)
COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
COMMON /CONTRL/ AMINLN, TIME, DELT, DUM5, IDUM1, DUM6
COMMON /RVFLOW/ TSTART(30), TSTOP(30)
C
C   IF (TIME.EQ.0.D0) CHECK(IC) = .TRUE.
C
C   DETERMINE PRESSURE DIFFERENCE ACROSS STREAM NODE, ACTUAL INLET NODE,
C   AND THE TOTAL MASS CONTAINED IN THE ACTUAL INLET NODE.
C
C     DELP  = PC(IIN(IC,1)) - PC(IOUT(IC,1))
C
C     INLET = IIN(IC,1)
C
C     IF (DELP.LT.0.D0) INLET = IOUT(IC,1)
C
C     MASS1 = 0.D0
C
C     DO 10 I10=1,9
C
C       MASS1 = MASS1 + MASS(INLET,I10)
C
C   10 CONTINUE
C
C   DETERMINE INLET DENSITY AND TOTAL MASS FLOW RATE THROUGH THE STREAM
C   NODE.
C
C     DENS  = MASS1/VOL(INLET)
C
C     MASS2 = DSQRT(DABS(DELP)*DENS/KRCOEF(IC))*DELT
C
C   DETERMINE COMPONENT MASS FLOW RATES, STREAM ENTHALPY RATE, AND STREAM
C   TEMPERATURE AND PRESSURE.
C
C     IF (DELP.LT.0.D0) MASS2 = - MASS2
C
C     FRAC  = MASS2/MASS1
C
C     DO 20 I20=1,9
C
C       MASS(IC,I20) = MASS(INLET,I20)*FRAC
C
C   20 CONTINUE
C
C     H(IC)  = H(INLET)*FRAC
C     TC(IC) = TC(INLET)
C     PC(IC) = PC(INLET)
C
C   CHECK FOR REVERSE FLOW.
C
C     IF (DELP.GE.0.D0) GO TO 30
C
C     IF (DELP.LT.0.D0.AND.CHECK(IC)) WRITE (5,100) IC, TIME

```

```

      IF (DELP.LT.0.D0.AND.CHECK(IC)) TSTART(IC) = TIME - DELT
C
      CHECK(IC) = .FALSE.
C
      RETURN
C
30  CONTINUE
C
      IF (.NOT.CHECK(IC)) WRITE (5,110) IC, TIME
      IF (.NOT.CHECK(IC)) TSTOP(IC) = TIME - DELT
C
      CHECK(IC) = .TRUE.
C
      RETURN
C
100 FORMAT (' REVERSE FLOW OCCURING IN NODE',I3,' AT',F10.5,' SEC.')
C
110 FORMAT (' NORMAL FLOW RESUMES IN NODE',I3,' AT',F10.5,' SEC.')
C
      END

```

## B.7 EQTUF6

```

      SUBROUTINE EQTUF6 (PSIA, TF)
C
C THIS SUBROUTINE CALCULATES THE EQUILIBRIUM TEMPERATURE, TF,
C CORRESPONDING TO A GIVEN PRESSURE, PSIA. THE FOLLOWING VARIABLES ARE
C USED.
C
C   PSIA    PRESSURE, PSIA
C   P1      ESTIMATED PRESSURE, PSIA
C   P2      ESTIMATED PRESSURE, PSIA
C   P3      ESTIMATED PRESSURE, PSIA
C   TF      TEMPERATURE, DEG F
C   T1      ESTIMATED TEMPERATURE, DEG F
C   T2      ESTIMATED TEMPERATURE, DEG F
C   T3      ESTIMATED TEMPERATURE, DEG F
C   LIMIT   ACCURACY REQUIRED OF P3 RELATIVE TO PSIA
C   F1      DIFFERENCE BETWEEN P1 AND PSIA
C   F2      DIFFERENCE BETWEEN P2 AND PSIA
C   F3      DIFFERENCE BETWEEN P3 AND PSIA
C   M       SLOPE OF F = M*T + B
C
      IMPLICIT REAL*8 (A-H,J-Z)
C
C THE ACCURACY REQUIRED OF P3 RELATIVE TO PSIA IS GIVEN BY LIMIT.
C
      LIMIT = PSIA/1.D8
C
C THE INITIAL GUESS OF TF, WHICH IS T1, IS BASED ON THE CORRELATION
C FOR VAPOR PRESSURE USED BETWEEN 147.3 AND 240 DEG F (22.04 AND
C 87.91 PSIA).
C

```

```

C      T1      = ( -4.66807D3 / (DLOG(PSIA) - 12.1600D0) ) - 367.533D0
C
C      IF (PSIA.GE.22.04226474D0) GO TO 40
C
C      THE FOLLOWING SEQUENCE OF EQUATIONS, THROUGH STATEMENT 40, GIVES THE
C      EQUILBRIUM TEMPERATURE FOR A PRESSURE LESS THAN 22.04 PSIA.
C
C      A SECOND ESTIMATED TEMPERATURE IS ALSO REQUIRED.
C
C      T2      = T1 + 1.0D0
C
C      IF (T2.GT.147.306561D0) T2 = 147.306561
C
C      10 CONTINUE
C
C      CALCULATE VAPOR PRESSURES CORRESPONDING TO T1 AND T2.
C
C      CALL VPRUF6 (T1, P1)
C      CALL VPRUF6 (T2, P2)
C
C      20 CONTINUE
C
C      EVALUATE T3, AN IMPROVED ESTIMATE OF TF.
C
C      F1      = P1 - PSIA
C      F2      = P2 - PSIA
C      M      = ( F2 - F1 ) / ( T2 - T1 )
C      T3      = T2 - F2/M
C
C      CHECK ACCURACY OF T3 BY CHECKING ACCURACY OF P3.
C
C      CALL VPRUF6 (T3, P3)
C
C      F3      = P3 - PSIA
C
C      IF (DABS(F3).LT.LIMIT) GO TO 30
C
C      T1      = T2
C      T2      = T3
C      P1      = P2
C      P2      = P3
C
C      GO TO 20
C
C      30 CONTINUE
C
C      TF      = T3
C
C      RETURN
C
C      40 CONTINUE
C
C      IF (PSIA.GT.87.91333852D0) GO TO 50
C

```

```

C THE ESTIMATED TEMPERATURE, T1, CORRESPONDS TO TF BETWEEN 147.3 AND
C 240 DEG F (22.04 AND 87.91 PSIA).
C
C     TF     = T1
C
C     RETURN
C
C 50 CONTINUE
C
C     IF (PSIA.GT.135.403989400) GO TO 60
C
C THE FOLLOWING SEQUENCE OF EQUATIONS, THROUGH STATEMENT 60, GIVES THE
C EQUILBRIUM TEMPERATURE FOR PRESSURES BETWEEN 87.91 AND 135.4 PSIA.
C
C CHECK T1 TO ENSURE THAT IT DOES NOT EXCEED 275.8 DEG F. A SECOND
C ESTIMATED TEMPERATURE IS ALSO REQUIRED.
C
C     IF (T1.GT.275.800) T1 = 275.8
C
C     T2     = T1 + 0.200
C
C RETURN TO 10 TO EVALUATE TF CORRESPONDING TO PSIA.
C
C     GO TO 10
C
C 60 CONTINUE
C
C THE FOLLOWING EQUATION GIVES TF FOR PRESSURES EXCEEDING 135.4039894
C PSIA (276 DEG F).
C
C     TF     = ( -6.97611D3 / (DLOG(PSIA) - 13.7627D0) ) - 511.866D0
C
C     RETURN
C
C     END

```

## B.8 FLASH

```

SUBROUTINE FLASH (TINIT, PINIT, MW, XVINIT, XLINIT, PFIN, ISEN,
*                XVFIN, XLFIN, TFIN)

```

```

C THIS SUBROUTINE DETERMINES THE VAPOR MASS FRACTION FOR A GIVEN FINAL
C PRESSURE BASED ON THE INITIAL TEMPERATURE, PRESSURE, VAPOR MASS
C FRACTION, AND LIQUID MASS FRACTION OF THE NON-VAPOR FRACTION AS WELL
C AS WHETHER THE FLASH IS ISENTROPIC OR ISENTHALPIC. THE FOLLOWING
C VARIABLES ARE USED.

```

```

C INPUT VARIABLES:
C
C TINIT    INITIAL TEMPERATURE, DEG F
C PINIT    INITIAL PRESSURE, PSIA
C MW       MOLECULAR WEIGHT, LB MASS/LB MOLE
C XVINIT   INITIAL VAPOR MASS FRACTION

```

C XLINIT INITIAL LIQUID MASS FRACTION OF THE NON-VAPOR FRACTION  
 C PFIN FINAL PRESSURE, PSIA  
 C ISEN VARIABLE SPECIFYING BASIS FOR FLASH CALCULATION  
 C ISEN = 0, ISENTROPIC FLASH  
 C ISEN = 1, ISENTHALPIC FLASH

C OUTPUT VARIABLES:

C XVFIN FINAL VAPOR MASS FRACTION  
 C XLFIN FINAL LIQUID MASS FRACTION OF THE NON-VAPOR FRACTION  
 C TFIN FINAL TEMPERATURE, DEG F

C \*\*\*\*\*  
 C \* \*  
 C \* WARNING! PINIT MUST BE GREATER THAN OR EQUAL TO PFIN. \*  
 C \* \*  
 C \*\*\*\*\*

C INTERNAL VARIABLES:

C SSOL ENTROPY OF THE SOLID, BTU/LB MASS-DEG F  
 C SLIQ ENTROPY OF THE LIQUID, BTU/LB MASS-DEG F  
 C SVAP ENTROPY OF THE VAPOR, BTU/LB MASS-DEG F  
 C SAVG AVERAGE ENTROPY OF THE INITIAL MIXTURE,  
 C BTU/LB MASS-DEG F  
 C  
 C HSOL ENTHALPY OF THE SOLID, BTU/LB MASS  
 C HLIQ ENTHALPY OF THE LIQUID, BTU/LB MASS  
 C HVAP ENTHALPY OF THE VAPOR, BTU/LB MASS  
 C HAVG AVERAGE ENTHALPY OF THE INITIAL MIXTURE, BTU/LB MASS  
 C  
 C F1, F2, F3 VALUES OF THE FUNCTION  $F = M \cdot T + B$  CORRESPONDING  
 C TO T1, T2, AND T3  
 C  
 C THE FUNCTION F CORRESPONDS TO THE TEST VALUE  
 C MINUS THE AVERAGE VALUE OF THE PROPERTY.  
 C  
 C S1, S2, S3 TEST ENTROPIES CORRESPONDING TO T1, T2, AND T3  
 C  
 C H1, H2, H3 TEST ENTHALPIES CORRESPONDING TO T1, T2, AND T3  
 C  
 C T1, T2, T3 TEST TEMPERATURES  
 C  
 C M SLOPE OF THE FUNCTION F  
 C LIMIT ACCURACY REQUIRED IN ESTIMATING THE AVERAGE PROPERTY  
 C IN SELECTING THE FINAL TEMPERATURE  
 C TMAX MAXIMUM TEMPERATURE A SUBCOOLED LIQUID CAN ATTAIN AT  
 C THE FINAL PRESSURE, DEG F

C THE FOLLOWING SUBROUTINES ARE USED.

C SUF6 CALCULATES UF6 ENTROPIES  
 C EQTUF6 CALCULATES TEMPERATURE CORRESPONDING TO A GIVEN  
 C VAPOR PRESSURE

```

C      HUF6      CALCULATES UF6 ENTHALPIES
C
C      THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED.
C
C              DENUF6
C              VPRUF6
C              ZUF6
C
C      IMPLICIT REAL*8 (A-H,J-Z)
C
C      A THREE PHASE INITIAL RELEASE CAN ONLY EXIST AT THE TRIPLE POINT;
C      THEREFORE, XLINIT EQUALS 1 OR 0 EXCEPT AT THE TRIPLE POINT.
C
C      IF (TINIT.GT.147.306561D0) XLINIT = 1.0D0
C      IF (TINIT.LT.147.306561D0) XLINIT = 0.0D0
C
C      SELECT BASIS FOR FLASH CALCULATION.
C
C      IF (ISEN.EQ.1) GO TO 40
C
C      CALCULATE THE AVERAGE ENTROPY OF THE INITIAL MIXTURE.
C
C      CALL SUF6 (TINIT, PINIT, MW, SSOL, SLIQ, SVAP)
C
C      SAUG = XVINIT*SVAP + (1.D0-XVINIT)*XLINIT*SLIQ
C      *      + (1.D0-XVINIT)*(1.D0-XLINIT)*SSOL
C
C      CALCULATE THE FINAL VAPOR MASS FRACTION ASSUMING AN EQUILIBRIUM
C      FLASH.
C
C      CALL EQTUF6 (PFIN, TFIN)
C
C      CALL SUF6 (TFIN, PFIN, MW, SSOL, SLIQ, SVAP)
C
C      IF (TFIN.GE.147.306561D0) XVFIN = (SAUG-SLIQ)/(SVAP-SLIQ)
C      IF (TFIN.LT.147.306561D0) XVFIN = (SAUG-SSOL)/(SVAP-SSOL)
C
C      IF (XVFIN.GE.0.0D0) GO TO 10
C
C      A VALUE OF XVFIN LESS THAN ZERO IMPLIES A SUBCOOLED CONDENSED PHASE
C      IS RELEASED. SINCE THERE IS CURRENTLY NO PRESSURE DEPENDENCE FOR
C      LIQUID ENTROPY, TFIN = TINIT.
C
C      XLFIN = XLINIT
C      XVFIN = 0.0D0
C      TFIN = TINIT
C
C      RETURN
C
C      10 CONTINUE
C
C      THE CONDENSED PHASE RELEASED WITH THE VAPOR IS LIQUID IF THE FINAL
C      TEMPERATURE IS GREATER THAN OR EQUAL TO THE TRIPLE POINT TEMPERATURE.
C

```

```

      IF (TFIN.GE.147.306561D0) XLFIN = 1.0D0
      IF (TFIN.LT.147.306561D0) XLFIN = 0.0D0
C
      IF (XVFIN.LE.1.0D0) RETURN
C
C   A VALUE OF XVFIN GREATER THAN 1 IMPLIES THAT THE FINAL FORM OF THE
C   RELEASE IS A SUPERHEATED VAPOR. THE FOLLOWING SEQUENCE OF EQUATIONS
C   THROUGH 40 EVALUATES THE FINAL TEMPERATURE OF A SUPERHEATED VAPOR
C   HAVING PFIN AS THE FINAL PRESSURE.
C
      LIMIT = SAUG / 1.08
      S1    = SVAP
      T1    = TFIN
      T2    = T1 + 1.0D0
C
      CALL SUF6 (T2, PFIN, MW, 0.0D0, 0.0D0, S2)
C
20  CONTINUE
C
      F1    = S1 - SAUG
      F2    = S2 - SAUG
      M     = ( F2 - F1 ) / ( T2 - T1 )
      T3    = T2 - F2/M
C
      CALL SUF6 (T3, PFIN, MW, 0.0D0, 0.0D0, S3)
C
      F3    = S3 - SAUG
C
      IF (DABS(F3).LT.LIMIT) GO TO 30
C
      T1    = T2
      T2    = T3
      S1    = S2
      S2    = S3
C
      GO TO 20
C
30  CONTINUE
C
      XVFIN = 1.0D0
      TFIN  = T3
C
      RETURN
C
40  CONTINUE
C
C   CALCULATE THE AVERAGE ENTHALPY OF THE INITIAL MIXTURE.
C
      CALL HUF6 (TINIT, PINIT, MW, HSOL, HLIQ, HVAP)
C
      HAUG  = XVINIT*HVAP + (1.0D0-XVINIT)*XLINIT*HLIQ
      *     + (1.0D0-XVINIT)*(1.0D0-XLINIT)*HSOL
C
C   CALCULATE THE FINAL VAPOR MASS FRACTION ASSUMING AN EQUILIBRIUM

```



```

C FLASH.
C
C   CALL EQTUF6 (PFIN, TFIN)
C
C   TMAX   = TFIN
C
C   CALL HUF6 (TFIN, PFIN, MW, HSOL, HLIQ, HVAP)
C
C   IF (TFIN.GE.147.306561D0) XVFIN = (HAUG-HLIQ)/(HVAP-HLIQ)
C   IF (TFIN.LT.147.306561D0) XVFIN = (HAUG-HSOL)/(HVAP-HSOL)
C
C   IF (XVFIN.GE.0.0D0) GO TO 70
C
C A VALUE OF XVFIN LESS THAN ZERO IMPLIES A SUBCOOLED PHASE IS
C RELEASED.
C
C   XLFIN  = XLINIT
C   XVFIN  = 0.0D0
C
C IF XLINIT EQUALS ZERO, THAN THE SUBCOOLED PHASE IS SOLID.
C
C   TFIN   = TINIT
C
C   IF (XLINIT.EQ.0.0D0) RETURN
C
C IF XLINIT IS NOT EQUAL TO ZERO, THEN A SUBCOOLED LIQUID IS RELEASED.
C THE FOLLOWING SEQUENCE OF EQUATIONS THROUGH 60 DETERMINES THE FINAL
C TEMPERATURE OF A SUBCOOLED LIQUID HAVING PFIN AS THE FINAL PRESSURE.
C
C   XLFIN  = 1.0D0
C   LIMIT  = HAUG / 1.D8
C   T1     = TMAX
C   H1     = HLIQ
C   T2     = TINIT
C
C   CALL HUF6 (T2, PFIN, MW, 0.0D0, H2, 0.0D0)
C
C 50 CONTINUE
C
C   F1     = H1 - HAUG
C   F2     = H2 - HAUG
C   M      = ( F2 - F1 ) / ( T2 - T1 )
C   T3     = T2 - F2/M
C
C   IF (T3.GT.TMAX) T3 = (TMAX + DMAX1(T1,T2))/2.D0
C   IF (T3.LT.TINIT) T3 = (TINIT + DMIN1(T1,T2))/2.D0
C
C   CALL HUF6 (T3, PFIN, MW, 0.0D0, H3, 0.0D0)
C
C   F3     = H3 - HAUG
C
C   IF (DABS(F3).LT.LIMIT) GO TO 60
C
C   IF ((DMAX1(T1,T2,T3) - DMIN1(T1,T2,T3)).LT.1.D-3) GO TO 60

```

```

C
  T1    = T2
  T2    = T3
  H1    = H2
  H2    = H3
C
  GO TO 50
C
60 CONTINUE
C
  TFIN  = T3
C
  RETURN
C
70 CONTINUE
C
C THE CONDENSED PHASE RELEASED WITH THE VAPOR IS LIQUID IF THE FINAL
C TEMPERATURE IS GREATER THAN OR EQUAL TO THE TRIPLE POINT TEMPERATURE.
C
  IF (TFIN.GE.147.30656100) XLFIN = 1.000
  IF (TFIN.LT.147.30656100) XLFIN = 0.000
C
  IF (XVFIN.LE.1.00) RETURN
C
C A VALUE OF XVFIN GREATER THAN 1 IMPLIES THAT THE FINAL FORM OF THE
C RELEASE IS A SUPERHEATED VAPOR. THE FOLLOWING SEQUENCE OF EQUATIONS
C THROUGH THE END OF THE SUBROUTINE EVALUATES THE FINAL TEMPERATURE
C OF A SUPERHEATED VAPOR HAVING PFIN AS THE FINAL PRESSURE.
C
  LIMIT = HAVG / 1.08
  H1    = HVAP
  T1    = TFIN
  T2    = T1 + 1.00
C
  CALL HUF6 (T2, PFIN, MW, 0.000, 0.000, H2)
C
80 CONTINUE
C
  F1    = H1 - HAVG
  F2    = H2 - HAVG
  M     = ( F2 - F1 ) / ( T2 - T1 )
  T3    = T2 - F2/M
C
  CALL HUF6 (T3, PFIN, MW, 0.000, 0.000, H3)
C
  F3    = H3 - HAVG
C
  IF (DABS(F3).LT.LIMIT) GO TO 90
C
  T1    = T2
  T2    = T3
  H1    = H2
  H2    = H3
C

```

```

      GO TO 80
C
      90 CONTINUE
C
      XVFIN = 1.00
      TFIN  = T3
C
      RETURN
C
      END

```

## B.9 HCOEFF

```

      SUBROUTINE HCOEFF (IC)
C
C THIS SUBROUTINE DETERMINES THE HEAT TRANSFER COEFFICIENT GIVEN THE
C ENTHALPIES OF THE INLET STREAMS AND THE COMPARTMENT, THE MASSES IN
C THE INLET STREAMS AND THE COMPARTMENT, THE COOLING RATE AND THE TIME
C STEP, AND THE AREA AND TEMPERATURE OF HEAT TRANSFER SURFACES. THE
C HEAT TRANSFER COEFFICIENT IS BASED ON HEATING UP THE MASS BROUGHT IN
C BY THE INLET STREAMS TO THE TEMPERATURE OF THE COMPARTMENT ATMOSPHERE
C UNDER NORMAL STEADY STATE CONDITIONS. THE TEMPERATURES USED IN
C EVALUATING THE HEAT TRANSFER COEFFICIENT ARE THE ROOM TEMPERATURE
C (NOT THE INLET STREAM TEMPERATURES) AND THE HEAT TRANSFER SURFACE
C TEMPERATURES.
C
C THE FOLLOWING VARIABLES ARE USED.
C
C INPUT VARIABLES
C
C IC          NODE NUMBER OF THE COMPARTMENT FOR WHICH THE
C             HEAT TRANSFER COEFFICIENT IS BEING CALCULATED
C
C COMMON BLOCK VARIABLES
C
C MASS      (30,9) COMPONENT MASS IN A NODE, LB (FOR COMPARTMENT
C             NODES), OR LB/(DELT) (FOR STREAM NODES)
C TC        (30)  NODE TEMPERATURE, DEG F
C PC        (30)  NODE PRESSURE, PSIA
C TSURF     (30)  HEAT TRANSFER SURFACE TEMPERATURE, DEG F
C H         (30)  TOTAL ENTHALPY OR ENTHALPY RATE, BTU OR
C             BTU/(DELT)
C QRATE     (30)  AMOUNT OF HEAT ADDED TO A NODE TO MAINTAIN A
C             CONSTANT TEMPERATURE UNDER NORMAL STEADY STATE
C             CONDITIONS, BTU/SEC
C QCOOL     (30)  COOLING RATE, BTU/SEC
C HTCDEF    (30)  HEAT TRANSFER COEFFICIENT, BTU/SEC-FT**2-DEG F
C HTAREA    (30)  SURFACE AREA FOR HEAT TRANSFER, FT**2
C AMINLN    NATURAL LOG OF THE MINIMUM NUMBER ACCEPTED BY
C             THE COMPUTER
C DELT      (30)  TIME INTERVAL USED FOR THE TRANSIENT SIMULATION,
C             SEC
C IIN       (30,4) INLET STREAM NODE NUMBER

```

```

C
C   INTERNAL VARIABLES
C
C   MASSIC      TOTAL MASS IN COMPARTMENT NODE IC, LB
C   MASS1      TOTAL MASS RATE IN INLET STREAM 1, LB/(DELT)
C   MASS2      TOTAL MASS RATE IN INLET STREAM 2, LB/(DELT)
C   MASS3      TOTAL MASS RATE IN INLET STREAM 3, LB/(DELT)
C   MASS4      TOTAL MASS RATE IN INLET STREAM 4, LB/(DELT)
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   COMMON /LBMASS/ MASS(30,9), DUM1
C   COMMON /COMPTP/ TC(30), PC(30), TSURF(30)
C   COMMON /ENTHAL/ H(30), QRATE(30), QCOOL(30), HTCDEF(30),
*   HTAREA(30)
C   COMMON /CONTRL/ AMINLN, DUM2, DELT, DUM3, IDUM1, DUM4
C   COMMON /ISTRMS/ IIN(30,4), IDUM2(120)
C
C   MASSIC = 0.D0
C   MASS1  = 0.D0
C   MASS2  = 0.D0
C   MASS3  = 0.D0
C   MASS4  = 0.D0
C
C   DO 10 I10=1,9
C
C       MASSIC = MASSIC + MASS(IC,I10)
C       MASS1  = MASS1  + MASS(IIN(IC,1),I10)
C       MASS2  = MASS2  + MASS(IIN(IC,2),I10)
C       MASS3  = MASS3  + MASS(IIN(IC,3),I10)
C       MASS4  = MASS4  + MASS(IIN(IC,4),I10)
C
C   10 CONTINUE
C
C   QRATE(IC) = (H(IC)*(MASS1 + MASS2 + MASS3 + MASS4)/MASSIC
*   - (H(IIN(IC,1)) + H(IIN(IC,2)) + H(IIN(IC,3))
*   + H(IIN(IC,4))) + QCOOL(IC)*DELT)/DELT
C
C   HTCDEF(IC) = QRATE(IC)/HTAREA(IC)/(TSURF(IC) - TC(IC))
C
C   RETURN
C
C   END

```

## B.10 HFPOLY

SUBROUTINE HFPOLY (TF, PHF, MW, C1C3C6)

```

C
C   THIS SUBROUTINE IS BASED ON INFORMATION PRESENTED IN JOHN M.
C   BECKERDITE, DAVID R. POWELL, AND EMORY T. ADAMS, JR., "SELF-ASSOCI-
C   ATION OF GASES. 2. THE ASSOCIATION OF HYDROGEN FLUORIDE," J. CHEM.
C   ENG. DATA 1983, 28, 287-293. THE EQUILIBRIUM COEFFICIENTS USED BELOW
C   WERE DEVELOPED FROM STROHMEIER AND BRIEGLEB'S DATA (SEE TABLE III).

```

```

C THE FOLLOWING VARIABLES ARE USED.
C
C     TF     TEMPERATURE, DEG F
C     TR     ABSOLUTE TEMPERATURE, DEG R
C     PHF    PARTIAL PRESSURE OF HF, PSIA
C     PLIMIT CONVERGENCE LIMIT FOR PRESSURE, PSI
C     MW     AVERAGE MOLECULAR WEIGHT OF HF, LB/LB MOLE
C     WMBHF  MOLECULAR WEIGHT OF HF MONOMER, LB/LB MOLE
C     K3     EQUILIBRIUM COEFFICIENT FOR TRIMER, PSIA**-2
C     K6     EQUILIBRIUM COEFFICIENT FOR HEXAMER, PSIA**-5
C     P1     PRESSURE OF HF MONOMER, PSIA
C     P1MW1  PRESSURE-MOLECULAR WEIGHT PRODUCT FOR HF MONOMER
C     P3MW3  PRESSURE-MOLECULAR WEIGHT PRODUCT FOR HF TRIMER
C     P6MW6  PRESSURE-MOLECULAR WEIGHT PRODUCT FOR HF HEXAMER
C     PMWSUM SUM OF PRESSURE-MOLECULAR WEIGHT PRODUCTS
C     C1     MASS FRACTION OF MONOMER TO TOTAL HF, LB MONOMER/LB HF
C           VAPOR
C     C3     MASS FRACTION OF TRIMER TO TOTAL HF, LB TRIMER/LB HF
C           VAPOR
C     C6     MASS FRACTION OF HEXAMER TO TOTAL HF, LB HEXAMER/LB HF
C           VAPOR
C
C     C1C3C6 A LOGICAL VARIABLE TO INDICATE WHETHER EXISTING VALUES
C           OF C1, C3, AND C6 SHOULD BE CHANGED
C
C           .TRUE. PERMITS VALUES TO BE CHANGED
C           .FALSE. RETAINS EXISTING VALUES
C
C           THIS VARIABLE IS GENERALLY .TRUE. EXCEPT, FOR EXAMPLE,
C           WHEN ONLY THE MOLECULAR WEIGHT IS REQUIRED IN PHFH2O TO
C           ESTABLISH THE AZEOTROPIC MOLE FRACTION OF HF IN THE HF-
C           H2O SYSTEM; IN THAT CASE, A CHANGE IN THE VALUES OF
C           C1, C3, AND C6 WOULD MESS UP OTHER CALCULATIONS.
C
C     F     FUNCTION OF PHF AND ESTIMATED P1 THAT MUST CONVERGE TO
C           ZERO TO OBTAIN THE AVERAGE MOLECULAR WEIGHT OF HF VAPOR
C     DFDP  DERIVATIVE OF F WITH RESPECT TO P1
C
C     IMPLICIT REAL*8(A-H,K-Z)
C
C     LOGICAL C1C3C6
C
C     COMMON /POLYMR/ C1, C3, C6,WMBHF
C
C     MW = WMBHF
C
C     IF (.NOT.C1C3C6) GO TO 10
C
C     C1 = 1.D0
C     C3 = 0.D0
C     C6 = 0.D0
C
C 10 CONTINUE
C

```

```

      IF (PHF.LT.1.D-5) RETURN
C
      PLIMIT = PHF*1.D-6
      TR = TF + 459.67D0
      K3 = DEXP(23884.0D0/TR - 51.2393D0)
      K6 = DEXP(40319.6D0/TR - 87.7927D0)
      P1 = PHF
C
20  CONTINUE
C
      F = PHF - P1 - K3*P1**3 - K6*P1**6
      IF (DABS(F).LT.PLIMIT) GO TO 30
      DFDP = -1.D0 - 3.D0*K3*P1**2 - 6.D0*K6*P1**5
      P1 = P1 - F/DFDP
C
      GO TO 20
C
30  CONTINUE
C
      P1MW1 = WMBHF*P1
      P3MW3 = 3.D0*WMBHF*K3*P1**3
      P6MW6 = 6.D0*WMBHF*K6*P1**6
      PMWSUM = P1MW1 + P3MW3 + P6MW6
      MW = PMWSUM/PHF
C
      IF (.NOT.C1C3C6) GO TO 40
C
      C1 = P1MW1/PMWSUM
      C3 = P3MW3/PMWSUM
      C6 = P6MW6/PMWSUM
C
40  CONTINUE
C
      RETURN
      END

```

## B.11 HHFH2O

```

      SUBROUTINE HHFH2O (TF, WHFL, WHFV, HL, HV)
C
C  THIS SUBROUTINE CALCULATES THE ENTHALPIES OF LIQUID AND VAPOR
C  MIXTURES OF HF AND H2O GIVEN THE TEMPERATURE AND THE WEIGHT MASS
C  FRACTION OF HF IN EACH PHASE. THE FOLLOWING VARIABLES ARE USED.
C
C      TF      TEMPERATURE, DEG F
C      WHFL    WEIGHT FRACTION HF IN LIQUID, LB HF/LB HF-H2O LIQ MIX
C      WHFV    WEIGHT FRACTION HF IN VAPOR, LB HF/LB HF-H2O VAP MIX
C      HL      ENTHALPY OF HF-H2O LIQUID MIXTURE, BTU/LB LIQ MIX
C      HV      ENTHALPY OF HF-H2O VAPOR MIXTURE, BTU/LB VAP MIX
C      C3POLY  MASS HF TRIMER TO MASS OF HF, LB TRIMER/LB HF VAPOR
C      C6POLY  MASS HF HEXAMER TO MASS OF HF, LB HEXAMER/LB HF VAPOR
C      WHFLSQ  WHFL**2
C

```

C A1,A2,A3,A4,A5 CONSTANTS IN EQUATIONS FOR LIQUID ENTHALPY  
 C B1,B2,B3,B4,B5 LINEAR CONSTANTS IN EQUATIONS FOR LIQUID  
 C ENTHALPY  
 C C2,C3,C4,C5 QUADRATIC CONSTANTS IN EQUATIONS FOR LIQUID  
 C ENTHALPY  
 C  
 C H20,H60,H80,H90,H100 LIQUID ENTHALPY AT 20, 60, 80, 90, AND  
 C 100 WT %, RESPECTIVELY, BTU/LB HF-H2O  
 C MIXTURE  
 C  
 C M20,M60,M80,M90 SLOPE OF H-WHFL CURVE AT 20, 60, 80, AND  
 C 90 WT %

C IMPLICIT REAL\*8 (A-H,J-Z)

C COMMON /POLYMR/ DUM1,C3POLY,C6POLY,DUM2

C THE FOLLOWING SEQUENCE OF EQUATIONS THROUGH "50 CONTINUE" EVALUATE  
 C THE ENTHALPY OF HF-H2O LIQUID MIXTURES. THE EQUATIONS ARE BASED ON  
 C A PLOT OF ENTHALPY VS CONCENTRATION AS A FUNCTION OF TEMPERATURE  
 C WHICH WAS SENT TO W. REID WILLIAMS BY BRIAN C. ROGERS OF ALLIED  
 C CHEMICAL, SOLVAY, NY, IN A LETTER DATED JULY 26, 1983. THE EQUATIONS  
 C WERE DEVELOPED BY W. R. WILLIAMS.

C WHFLSQ = WHFL\*WHFL

C A1 = -32.25200 + 0.9978300\*TF  
 C B1 = -357.7500 - 0.96900\*TF + 0.001300\*TF\*\*2

C IF (WHFL.GT.0.200) GO TO 10

C THE FOLLOWING EQUATION IS APPLICABLE FOR WHFL BETWEEN 0.0 AND 0.2.

C HL = A1 + B1\*WHFL

C GO TO 50

C 10 CONTINUE

C H20 = A1 + B1\*0.200  
 C H60 = -179.6800 + 0.6356900\*TF + 5.84290-4\*TF\*\*2  
 C M20 = B1  
 C C2 = (H20 - H60 + 0.400\*M20) / (-0.1600)  
 C B2 = M20 - 0.400\*C2  
 C A2 = H20 - 0.200\*B2 - 0.0400\*C2

C IF (WHFL.GT.0.600) GO TO 20

C THE FOLLOWING EQUATION IS APPLICABLE FOR WHFL BETWEEN 0.2 AND 0.6.

C HL = A2 + B2\*WHFL + C2\*WHFLSQ

C GO TO 50

C

20 CONTINUE

C

H80 = -159.26D0 + 0.7985D0\*TF  
 M60 = B2 + 1.2D0\*C2  
 C3 = (H60 - H80 + 0.2D0\*M60) / (-0.04D0)  
 B3 = M60 - 1.2D0\*C3  
 A3 = H60 - 0.6D0\*B3 - 0.36D0\*C3

C

IF (WHFL.GT.0.8D0) GO TO 30

C

C THE FOLLOWING EQUATION IS APPLICABLE FOR WHFL BETWEEN 0.6 AND 0.8.

C

HL = A3 + B3\*WHFL + C3\*WHFLSQ

C

GO TO 50

C

30 CONTINUE

C

H90 = -111.54D0 + 0.67057\*TF  
 M80 = B3 + 1.6D0\*C3  
 C4 = (H80 - H90 + 0.1D0\*M80) / (-0.01D0)  
 B4 = M80 - 1.6D0\*C4  
 A4 = H80 - 0.8D0\*B4 - 0.64D0\*C4

C

IF (WHFL.GT.0.9D0) GO TO 40

C

C THE FOLLOWING EQUATION IS APPLICABLE FOR WHFL BETWEEN 0.8 AND 0.9.

C

HL = A4 + B4\*WHFL + C4\*WHFLSQ

C

GO TO 50

C

40 CONTINUE

C

H100 = -23.3142D0 + 0.870283D0\*TF  
 M90 = B4 + 1.8D0\*C4  
 C5 = (H90 - H100 + 0.1D0\*M90) / (-0.01D0)  
 B5 = M90 - 1.8D0\*C5  
 A5 = H90 - 0.9D0\*B5 - 0.81D0\*C5

C

C THE FOLLOWING EQUATION IS APPLICABLE FOR WHFL BETWEEN 0.9 AND 1.0

C

HL = A5 + B5\*WHFL + C5\*WHFLSQ

C

50 CONTINUE

C

C THE FOLLOWING EQUATION FOR THE ENTHALPY OF A VAPOR MIXTURE OF HF AND  
 C H2O WAS DERIVED BY W. R. WILLIAMS FROM THE ABOVE CITED PLOT AND FROM  
 C INFORMATION PRESENTED IN JOHN M. BECKERDITE, DAVID R. POWELL, AND  
 C EMORY T. ADAMS, JR., "SELF-ASSOCIATION OF GASES. 2. THE ASSOCIATION  
 C OF HYDROGEN FLUORIDE," J. CHEM. ENG. DATA 1983, 28, 287-293.

C

HV = (1051.0D0 + 0.472D0\*TF) - (376.0D0 + 0.136D0\*TF  
 \* + 790.642D0\*C3POLY + 667.358D0\*C6POLY)\*WHFV



C  
 C RETURN  
 C  
 C END

## B.12 HUF6

      SUBROUTINE HUF6 (TF, PSIA, MW, HSOL, HLIQ, HVAP)  
 C  
 C THIS SUBROUTINE CALCULATES THE ENTHALPIES OF UF6 SOLID, LIQUID, AND  
 C VAPOR. THE FOLLOWING VARIABLES ARE USED.  
 C  
 C     TF        TEMPERATURE, DEG F  
 C     TR        ABSOLUTE TEMPERATURE, DEG R  
 C     TRSQ      (DEG R)\*\*2  
 C     PSIA      PRESSURE, PSIA  
 C     VPSIA     VAPOR PRESSURE CORRESPONDING TO TF, PSIA  
 C     MW        MOLECULAR WEIGHT, LB MASS/LB MOLE  
 C     HSOL      ENTHALPY OF THE SOLID, BTU/LB MASS  
 C     HLIQ      ENTHALPY OF THE LIQUID, BTU/LB MASS  
 C     HVAP      ENTHALPY OF THE VAPOR, BTU/LB MASS  
 C     DENLIQ    DENSITY OF THE LIQUID, LB MASS/FT\*\*3  
 C     ZPSIA     VAPOR COMPRESSIBILITY FACTOR AT TF AND PSIA  
 C     Z1ATM     VAPOR COMPRESSIBILITY FACTOR AT TF AND 14.696 PSIA  
 C  
 C THE FOLLOWING SUBROUTINES ARE CALLED.  
 C  
 C     DENUF6  
 C     VPRUF6  
 C     ZUF6  
 C  
 C THE ENTHALPY CORRELATIONS ARE BASED OF INFORMATION FOUND IN R.  
 C DEWITT, "URANIUM HEXAFLUORIDE: A SURVEY OF THE PHYSICO-CHEMICAL  
 C PROPERTIES," GAT-280, GOODYEAR ATOMIC CORP., PORTSMOUTH, OHIO, JAN.  
 C 29, 1960, PAGES 65 - 67. THE CORRELATIONS REPORTED IN GAT-280 FOR THE  
 C ENTHALPIES OF THE SOLID AND LIQUID ARE FOR SATURATED CONDITIONS, AND  
 C THE ENTHALPY OF THE VAPOR IS BASED ON A PRESSURE OF 1 ATM. THE LIQUID  
 C ENTHALPY CORRELATION WAS MODIFIED FOR SUPERSATURATED CONDITIONS (PSIA  
 C GRAETER THAN VPSIA) ASSUMING AN INCOMPRESSIBLE LIQUID. THE VAPOR  
 C ENTHALPY CORRELATION WAS MODIFIED USING THE MAGNUSON EQUATION OF  
 C STATE (SEE GAT-280, PAGES 97 - 101) AND THE DEPARTURE FUNCTION  
 C CORRELATIONS GIVEN IN R. C. REID, J. M. PRAUSNITZ, AND T. K.  
 C SHERWOOD, THE PROPERTIES OF GASES AND LIQUIDS, 3RD ED., MCGRAW-HILL  
 C BOOK COMPANY, 1977, PAGE 93, SO THAT BOTH SATURATED AND UNSATURATED  
 C VAPOR ENTHALPIES CAN BE CALCULATED.  
 C  
 C     IMPLICIT REAL\*8 (A-H,J-Z)  
 C  
 C     TR        = TF + 459.67D0  
 C  
 C     TRSQ     = TR\*\*2  
 C  
 C THE ENTHALPY OF THE SOLID IS GIVEN BY THE FOLLOWING CORRELATION WHICH

```

C IS ACCURATE WITHIN 0.01% FROM 17 DEG F TO THE TRIPLE POINT (147.3
C DEG F).
C
C      HSOL = ( 50.4460D0 - 5.70531D-2*TR + 1.27509D-4*TRSQ
*          - ( 9.64563D3/TR ) ) * ( 3.52D2/MW )
C
C CALCULATE THE DENSITY OF THE LIQUID AND THE VAPOR PRESSURE.
C
C      CALL DENUF6 (TF, PSIA, MW, 0.0D0, DENLIQ, 0.0D0)
C
C      CALL VPRUF6 (TF, VPSIA)
C
C THE ENTHALPY OF THE LIQUID IS GIVEN BY THE FOLLOWING CORRELATION
C WHICH IS REPORTED TO HAVE AN ACCURACY WITHIN 0.01% [OVER THE ASSUMED
C RANGE OF 147.3 TO 206.3 DEG F] FOR THE SATURATED LIQUID.
C
C      HLIQ = ( 30.6133D0 + 5.10057D-2*TR + 5.13165D-5*TRSQ
*            - ( 6.13934D3/TR )
*            + ( 1.82628D-1 * ( PSIA - VPSIA ) / DENLIQ ) )
*            * ( 3.52D2/MW )
C
C CALCULATE THE VAPOR COMPRESSIBILITY AT 14.696 PSIA AND AT "PSIA."
C
C      CALL ZUF6 (TF, 14.696D0, Z1ATM, 0.0D0, 0.0D0)
C
C      CALL ZUF6 (TF, PSIA, ZPSIA, 0.0D0, 0.0D0)
C
C THE ENTHALPY OF THE VAPOR IS GIVEN BY THE FOLLOWING CORRELATION.
C
C      HVAP = ( 43.2614D0 + 9.21307D-2*TR + 6.26265D-6*TRSQ
*            + ( 2.95171D3/TR )
*            + 3.0939D-3 * TR * (ZPSIA - Z1ATM) ) * ( 3.52D2/MW )
C
C      RETURN
C
C      END

```

### B.13 HUMID

```

      SUBROUTINE HUMID (IC, RH, RATIO)
C
C THIS SUBROUTINE CALCULATES THE RATIO OF MOLES OF WATER VAPOR IN HUMID
C AIR TO THE TOTAL MOLES OF AIR PLUS WATER VAPOR.
C
C THE FOLLOWING VARIABLES ARE USED.
C
C INPUT VARIABLES
C
C      IC          NODE NUMBER OF VECTOR HAVING TEMPERATURE AND
C                  PRESSURE REQUIRED FOR CALCULATING RATIO
C      RH          RELATIVE HUMIDITY CORRESPONDING TO TEMPERATURE
C                  AND PRESSURE OF NODE IC
C

```

```

C   OUTPUT VARIABLE
C
C   RATIO           RATIO OF MOLES OF WATER VAPOR TO TOTAL MOLES OF
C                   MOIST AIR
C
C   COMMON BLOCK VARIABLES
C
C   TC      (30)    NODE TEMPERATURE, DEG F
C   PC      (30)    NODE PRESSURE, PSIA
C
C   INTERNAL VARIABLES
C
C   WHFL           WEIGHT FRACTION OF HF IN HF-H2O CONDENSATE
C   PH20           VAPOR PRESSURE OF H2O, PSIA
C
C   THE FOLLOWING SUBROUTINE IS REQUIRED.
C
C               PHFH20
C
C   THE SUBROUTINE HFPOLY IS CALLED BY PHFH20, BUT IT IS NOT CALLED IN
C   CALCULATING PH20 FOR THIS SUBROUTINE.
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   COMMON /COMPTP/ TC(30), PC(30), DUM1(30)
C
C   WHFL   = 0.D0
C
C   CALL PHFH20 (TC(IC), WHFL, 0.D0, 0.D0, PH20, 0.D0)
C
C   RATIO  = RH*PH20/PC(IC)
C
C   RETURN
C
C   END

```

#### B.14 INTMEB

```

C   SUBROUTINE INTMEB
C
C   THIS SUBROUTINE DETERMINES THE FINAL STATE (PRESSURE, TEMPERATURE,
C   MASS FRACTIONS IN EACH PHASE) OF UF6 IN A CONTROL VOLUME GIVEN THE
C   INITIAL STATES OF INLET AND OUTLET STREAMS AND OF THE MASS IN THE
C   VOLUME AT THE BEGINNING OF A TIME STEP DURING WHICH MASS AND ENERGY
C   ARE ASSUMED TO FLOW AT CONSTANT RATES.
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   COMMON BLOCKS TRANSFER DATA BETWEEN INTMEB AND THE DRIVER.
C
C   COMMON /ICOMON/ ISEN, IPIG, IBRCH, IGEXIT
C   COMMON /CONCYL/ PCYL, TCYL, XVCYL, XLCYL, MW
C   COMMON /CONIN / PIN, TIN, XVIN, XLIN

```

```

COMMON /CONVOL/ PVOL,TVOL,XVOL,XLVOL
COMMON /PARAM / VOL,DELT,Q
COMMON /MASS / MOUT,MIN,MTOT
COMMON /TRIPLE/ TTRIPL,PTRIPL

C
  DIMENSION HARRAY(3,3),HVECTR(3)
C
C THE ARRAY FOR ENTHALPIES OF MATERIAL AT TIME T IS FILLED
C
  CALL HUF6(TVOL,PVOL,MW,HARRAY(1,3),HARRAY(1,2),HARRAY(1,1))
  CALL HUF6(TIN,PIN,MW,HARRAY(2,3),HARRAY(2,2),HARRAY(2,1))
  CALL HUF6(TVOL,PVOL,MW,HARRAY(3,3),HARRAY(3,2),HARRAY(3,1))
C
  HTOT =
* MTOT*(HARRAY(3,1)*XVOL + HARRAY(3,2)*(1.00-XVOL)*XLVOL
*           + HARRAY(3,3)*(1.00-XVOL)*(1.00-XLVOL))
*+(MIN*(HARRAY(2,1)*XVIN + HARRAY(2,2)*(1.00-XVIN)*XLIN
*           + HARRAY(2,3)*(1.00-XVIN)*(1.00-XLIN))
*-MOUT*(HARRAY(1,1)*XVCYL + HARRAY(1,2)*(1.00-XVCYL)*XLCYL
*           + HARRAY(1,3)*(1.00-XVCYL)*(1.00-XLCYL))
*+ Q)*DELT
C
  MTOT = MTOT + DELT*(MIN-MOUT)
C
C FIRST ASSUME A FINAL CONDITION AT THE TRIPLE POINT
C
  CALL HUF6 (TTRIPL,PTRIPL,MW,HVECTR(3),HVECTR(2),HVECTR(1))
C
  CALL DENUF6(TTRIPL,PTRIPL,MW,DENSOL,DENLIQ,DENVAP)
C
  MVAP = DENVAP*( VOL*DENLIQ*DENSOL*(HVECTR(2)-HVECTR(3))
*           +MTOT*(DENSOL*HVECTR(3)-DENLIQ*HVECTR(2))
*           +HTOT*(DENLIQ-DENSOL))
* /(( DENLIQ*DENSOL*(HVECTR(2)-HVECTR(3))
*     +DENVAP*DENLIQ*(HVECTR(1)-HVECTR(2))
*     -DENVAP*DENSOL*(HVECTR(1)-HVECTR(3)))
C
  MLIQ = HTOT/(HVECTR(2)-HVECTR(3))
*        -MTOT*HVECTR(3)/(HVECTR(2)-HVECTR(3))
*        -MVAP*(HVECTR(1)-HVECTR(3))/(HVECTR(2)-HVECTR(3))
C
  MSOL = MTOT-MVAP-MLIQ
C
  ITER8R = 0
C
  OLDSOL = MSOL
  OLDT = TTRIPL
C
  IF (MLIQ.LT.0.00) GO TO 50
  IF (MSOL.LT.0.00) GO TO 20
C
  TVOL = TTRIPL
  PVOL = PTRIPL
  XVOL = MVAP/MTOT

```

```

C      IF (MLIQ.EQ.0.D0.AND.MSOL.EQ.0.D0) GO TO 10
C      XLVOL = MLIQ/(MLIQ+MSOL)
C      RETURN
C
C 10 CONTINUE
C      XLVOL = 1.D0
C      RETURN
C
C FOLLOWING CODE SEGMENTS ARE CALLED WHEN FINAL CONDITIONS
C DO NOT MATCH THE TRIPLE POINT.
C
C 20 CONTINUE
C
C FINAL TEMPERATURE IS ABOVE TRIPLE POINT. NO SOLID IS PRESENT.
C
C      XLVOL = 1.D0
C
C 30 CONTINUE
C
C      CALL HUF6 (TVOL,PVOL,MW,HVECTR(3),HVECTR(2),HVECTR(1))
C
C      CALL DENUF6(TVOL,PVOL,MW,DENSOL,DENLIQ,DENVAP)
C
C      MVAP = DENVAP*( VOL*DENLIQ*DENSOL*(HVECTR(2)-HVECTR(3))
*          +MTOT*(DENSOL*HVECTR(3)-DENLIQ*HVECTR(2))
*          +HTOT*(DENLIQ-DENSOL))
*      /(( DENLIQ*DENSOL*(HVECTR(2)-HVECTR(3))
*          +DENVAP*DENLIQ*(HVECTR(1)-HVECTR(2))
*          -DENVAP*DENSOL*(HVECTR(1)-HVECTR(3)))
C
C      MLIQ = HTOT/(HVECTR(2)-HVECTR(3))
*          -MTOT*HVECTR(3)/(HVECTR(2)-HVECTR(3))
*          -MVAP*(HVECTR(1)-HVECTR(3))/(HVECTR(2)-HVECTR(3))
C
C      MSOL = MTOT-MVAP-MLIQ
C
C      XVOL = MVAP/MTOT
C
C      IF (DABS(MSOL).LT.1.D-6) RETURN
C
C      IF (MSOL.GT.0.D0) GO TO 40
C
C      OLDSOL = MSOL
C      OLDT = TVOL
C      TVOL = HITVOL
C      MSOL = HIMSOL
C
C 40 CONTINUE
C

```

```

NEWT  = TVOL - MSOL*(TVOL-OLDT)/(MSOL-OLDSOL)
C
IF (NEWT.GT.250.D0.OR.NEWT.LT.TTRIPL) STOP02
C
ITER8R = 1 + ITER8R
C
IF (ITER8R.GT.20) STOP03
C
HIMSOL = MSOL
HITVOL = TVOL
TVOL   = NEWT
C
CALL VPRUF6(TVOL,PVOL)
C
GO TO 30
C
50 CONTINUE
C
FINAL TEMPERATURE IS BELOW TRIPLE POINT. NO LIQUID IS PRESENT.
C
XLVOL  = 0.D0
TVOL   = TTRIPL - 10.D0
C
CALL VPRUF6(TVOL,PVOL)
C
60 CONTINUE
C
CALL HUF6 (TVOL,PVOL,MW,HVECTR(3),HVECTR(2),HVECTR(1))
C
CALL DENUF6(TVOL,PVOL,MW,DENSOL,DENLIQ,DENVAP)
C
MVAP  = DENVAP*( VOL*DENLIQ*DENSOL*(HVECTR(2)-HVECTR(3))
*      +MTOT*(DENSOL*HVECTR(3)-DENLIQ*HVECTR(2))
*      +HTOT*(DENLIQ-DENSOL))
*      /( DENLIQ*DENSOL*(HVECTR(2)-HVECTR(3))
*      +DENVAP*DENLIQ*(HVECTR(1)-HVECTR(2))
*      -DENVAP*DENSOL*(HVECTR(1)-HVECTR(3)))
C
MLIQ  = HTOT/(HVECTR(2)-HVECTR(3))
*      -MTOT*HVECTR(3)/(HVECTR(2)-HVECTR(3))
*      -MVAP*(HVECTR(1)-HVECTR(3))/(HVECTR(2)-HVECTR(3))
C
MSOL  = MTOT-MVAP-MLIQ
C
XVOL  = MVAP/MTOT
C
IF (DABS(MLIQ).LT.1.D-6) RETURN
C
IF (MLIQ.GT.0.D0) GO TO 80
C
OLDLIQ = MLIQ
OLDT   = TVOL
C
IF (ITER8R.GT.0.D0) GO TO 70

```

```

C      TVOL  = TVOL - 10.00
C
C      CALL VPRUF6(TVOL,PVOL)
C
C      GO TO 60
C
C 70 CONTINUE
C
C      OLDT  = TVOL
C      OLDLIQ = MLIQ
C      TVOL  = LOTVOL
C      MLIQ  = LOMLIQ
C
C 80 CONTINUE
C
C      ITER8R = 1 + ITER8R
C
C      IF (ITER8R.GT.20) STOP04
C
C      NEWT  = TVOL + MLIQ*(OLDT-TVOL)/(MLIQ-OLDLIQ)
C
C      IF (NEWT.GT.TTRIPL.OR.NEWT.LT.0.00) STOP05
C
C      LOMLIQ = MLIQ
C      LOTVOL = TVOL
C      TVOL  = NEWT
C
C      CALL VPRUF6(TVOL,PVOL)
C
C      GO TO 60
C
C      RETURN
C
C      END

```

## B.15 LEVEL

SUBROUTINE LEVEL (DENVAP, VLFACE)

```

C
C THIS SUBROUTINE CALCULATES THE LEVEL OF THE PHASE INTERFACE WITH
C RESPECT TO THE BOTTOM OF A CONTAINMENT VOLUME AND W.R.T. A BREACH
C OR PIPE SYSTEM ENTRANCE. THE CODE THEN DETERMINES THE MASS FRACTIONS
C OF VAPOR, LIQUID, AND SOLID WHICH LEAVE THE CONTAINMENT AND THE
C PRESSURE OF THE RELEASE, IF DIFFERENT FROM THE SATURATION PRESSURE.
C
C THE TOTAL MASS IN CONTAINMENT IS INPUT ALONG WITH THE TOTAL VOLUME,
C SATURATION PRESSURE AND TEMPERATURE, AND THE MASS FRACTIONS OF EACH
C PHASE PRESENT. ALSO INPUT ARE THE CONTAINMENT PARAMETERS OF LENGTH
C AND DIAMETER, THE BREACH PARAMETERS OF HOLE DIAMETER AND DISTANCE OF
C THE HOLE CENTER FROM THE CONTAINMENT CENTER. THE CONTAINMENT IS
C MODELED AS A CYLINDER WITH THE HOLE IN ONE END AND THE CYLINDER
C ORIENTATION (UPRIGHT OR ON ITS SIDE) IS ALSO INPUT.

```

```

C
C INPUT VARIABLES, VALUES PROVIDED BY CALLING PROGRAM.
C
C     DENVAP  DENSITY OF VAPOR, LB MASS/FT**3
C     VLFACE  HEIGHT ABOVE CYLINDER BOTTOM OF VAPOR-LIQUID
C             INTERFACE, IN
C     XVOL    MASS FRACTION OF VAPOR IN CYLINDER
C     MTOT    TOTAL MASS IN CYLINDER, LB MASS
C     VOL     TOTAL VOLUME ENCLOSED IN CYLINDER, FT**3
C     DIACYL  DIAMETER OF CYLINDER, IN
C     LCYL   LENGTH OF CYLINDER, IN
C     RHOLE  LENGTH OF RAY FROM CENTER OF CYLINDER
C             TO CENTER OF HOLE, IN
C     DHOLE  DIAMETER OF HOLE, IN
C
C INTERNAL VARIABLES USED BY THE LEVEL SUBROUTINE
C
C     ALPHA   ANGLE BETWEEN VERTICAL UPWARD RAY AND RAY FROM
C             CENTER OF CYLINDER TO CENTER OF HOLE, DEGREES
C     WVOL    VOLUME OF VAPOR IN CYLINDER, FT**3
C     VOL2,   TOTAL VOLUME AND VAPOR VOLUME IN CYLINDER,
C     WVOL2  RESPECTIVELY, IN**3
C     RADIAN  ANGLE AS DEFINED FOR ALPHA, RADIAN
C     ISPLIT  =0, VAPOR-LIQUID INTERFACE IS ABOVE (BELOW) HOLE
C             =1, VAPOR-LIQUID INTERFACE COINCIDES WITH HOLE
C     IVERT   =0, CYLINDER LIES ON SIDE
C             =1, CYLINDER STANDS ON END, HOLE ON BOTTOM
C     ITER8R  INDEX USED TO CONTROL NUMBER OF ITERATIONS
C     A1,A2,A3 OLD, CURRENT, AND NEW RESULTS FOR VLFACE
C     G1,G2,G3 OLD, CURRENT, AND NEW GUESSES FOR VLFACE
C     OLDVLF  STORAGE LOCATION FOR PREVIOUS VALUE OF VLFACE.
C     HINTER  DEPTH OF LIQUID ABOVE BOTTOM OF HOLE, IN
C     YVCYL  VAPOR VOLUME FRACTION
C             OF MATERIAL ENTERING RELEASE PATHWAY.
C     DENLS  DENSITY OF THE MASS FRACTION WHICH IS NOT VAPOR,
C             LB MASS/FT**3
C
C OUTPUT VARIABLES, VALUES RETURNED TO CALLING PROGRAM.
C
C     XVCYL  VAPOR MASS FRACTION
C             OF MATERIAL ENTERING RELEASE PATHWAY.
C     PCYL   PRESSURE OF MATERIAL
C             ENTERING RELEASE PATHWAY, PSIA
C
C     IMPLICIT REAL*8 (A-H,J-Z)
C
C COMMON BLOCKS TRANSFER MOST OF THE INPUT AND OUTPUT VALUES.
C
C     COMMON /CONCYL/ PCYL,TCYL,XVCYL,XLCYL,MW
C     COMMON /CONVOL/ PVOL,TVOL,XVOL,XLVOL
C     COMMON /PARAM / VOL,DELT,Q
C     COMMON /MASS / MSFLRT,MIN,MTOT
C     COMMON /CYLIND/ DIACYL,LCYL,RHOLE,DHOLE,ALPHA,IVERT
C

```



```

C  CALCULATE THE VOLUME OF VAPOR IN THE CYLINDER.
C
C      WVOL  = XVOL*MTOT/DENVAP
C
C  VOL AND WVOL ARE IN CUBIC FEET. CONVERT TO CUBIC INCHES.
C
C      VOL2  = VOL*1728.D0
C
C      WVOL2 = WVOL*1728.D0
C
C  ALPHA IS IN DEGREES. USE EQUIVALENT ANGLE IN RADIANS.
C
C      RADIAN = ALPHA*3.14159D0/180.D0
C
C  AN INTEGER INDEX IS SET TO ZERO FOR A VAPOR-LIQUID INTERFACE ABOVE
C  THE TOP OF THE HOLE OR BELOW THE BOTTOM OF THE HOLE. IF THE VAPOR-
C  LIQUID INTERFACE IS FOUND TO COINCIDE WITH THE HOLE, THE INDEX WILL
C  BE RESET TO 1.
C
C      ISPLIT = 0
C
C  IF THE HOLE IS AT THE BOTTOM OF A CYLINDER STANDING ON END, THE
C  VAPOR-LIQUID INTERFACE CAN BE CALCULATED DIRECTLY. THE PROGRAM WILL
C  SKIP DOWN TO THAT SECTION.
C
C      IF (IVERT.EQ.1) GO TO 70
C
C  CALCULATE VAPOR-LIQUID INTERFACE. START WITH THE VALUE OF VLFACE
C  PASSED FROM THE CALLING PROGRAM. THEN EVALUATE VLFACE USING THE
C  PREVIOUS VALUE AS A GUESS.
C
C      ITERR8R = 0
C
C      A1      = 0.D0
C
C      G1      = 0.D0
C
C      A2      = 0.D0
C
C      G2      = 0.D0
C
C      A3      = 0.D0
C
C      G3      = 0.D0
C
C 10 CONTINUE
C
C      OLDVLF = VLFACE
C
C      VLFACE = DIACYL/2.D0*(1.D0 + DCOS(3.14159D0*LCYL/VOL2
C      *      *(WVOL2/LCYL + (VLFACE - DIACYL/2.D0)
C      *      *DSQRT(VLFACE*DIACYL - VLFACE**2))))
C
C  IF VLFACE CONVERGES STOP THE ITERATION.

```

```

C      IF (DABS(VLFACE-OLDVLF).LT.1.D-6) GO TO 60
C      ITER8R = ITER8R + 1
C      IF VLFACE DOES NOT CONVERGE STOP EXECUTION.
C      IF (ITER8R.GT.100) STOP06
C      IF (VLFACE.GT.OLDVLF.AND.G1.GT.A1) GO TO 20
C      G1      = OLDVLF
C      A1      = VLFACE
C      GO TO 10
C      20 CONTINUE
C      A REGULA FALSI SCHEME DETERMINES FURTHER GUESSES FOR VLFACE.
C      G2      = OLDVLF
C      A2      = VLFACE
C      30 CONTINUE
C      G3      = (G2*(A1-A2)-A2*(G1-G2))
*          /((A1-A2)-(G1-G2))
C      A3      = DIACYL/2.D0*(1.D0 + DCOS(3.14159D0*LCYL/VOL2
*          *(VOL2/LCYL + (G3 - DIACYL/2.D0)
*          *DSQRT(G3*DIACYL - G3**2))))
C      IF A3 CONVERGES STOP THE ITERATION.
C      IF (DABS(A3-G3).LT.1.D-6) GO TO 50
C      ITER8R = ITER8R + 1
C      IF A3 DOES NOT CONVERGE STOP EXECUTION.
C      IF (ITER8R.GT.100) STOP07
C      THIS MODIFIED REGULA FALSI SELECTS WHICH OF THE TWO PREVIOUS GUESSES
C      TO REPLACE WITH THE NEW GUESS.  BY THIS MEANS THE REGULA FALSI IS
C      ALWAYS USED FOR INTERPOLATION, SPEEDING CONVERGENCE.
C      IF (G3.LT.A3) GO TO 40
C      A2      = A3
C      G2      = G3
C

```

```

      GO TO 30
C
C 40 CONTINUE
C
      A1      = A3
C
      G1      = G3
C
      GO TO 30
C
C 50 CONTINUE
C
C HEIGHT OF THE VAPOR-LIQUID INTERFACE IS DETERMINED. THE LAST PAIR OF
C GUESS AND RESULT IS STORED AS OLDVLF AND VLFACE, RESPECTIVELY.
C
      VLFACE = A3
C
      OLDVLF = G3
C
C 60 CONTINUE
C
C NOW CALCULATE THE DEPTH OF LIQUID ABOVE THE BOTTOM OF THE HOLE.
C
      HINTER = VLFACE - (DIACYL/2.D0 + RHOLE*DCOS(RADIAN)
*
*                - DHOLE/2.D0)
C
C HINTER NEGATIVE MEANS VAPOR-LIQUID INTERFACE IS BELOW BOTTOM OF HOLE;
C A VAPOR RELEASE OCCURS. SINCE THE CALLING PROGRAM HAS ALREADY
C INITIALIZED A VAPOR RELEASE, LEVEL RETURNS WITHOUT FURTHER
C CALCULATION.
C
      IF (HINTER.LE.0.D0) GO TO 100
C
C THE LIQUID LEVEL IS ABOVE THE BOTTOM OF THE HOLE. IF IT IS ABOVE THE
C TOP OF THE HOLE, THE RELEASE WILL CONTAIN NO VAPOR. CALCULATE THE
C INTERFACE LEVEL FOR A PRESSURE CORRECTION.
C
      VLFACE = HINTER - DHOLE/2.D0
C
      IF (HINTER.GE.DHOLE) GO TO 80
C
C THE LIQUID LEVEL COINCIDES WITH THE HOLE LEVEL. CALCULATE THE VAPOR
C VOLUME FRACTION AND SET ISPLIT TO 1.
C
      YVCYL = (ACOS(SNGL(2.D0*HINTER/DHOLE-1.D0))
*
*      -4.D0/DHOLE**2*(HINTER-DHOLE/2.D0)
*
*      *DSQRT(DHOLE*HINTER-HINTER**2))/3.14159D0
C
      ISPLIT = 1
C
C 70 CONTINUE
C
C CALCULATE DEPTH OF LIQUID IN VERTICAL CYLINDER.
C

```

```

      VLFACE = LCYL*VVOL/VOL
C
C      80 CONTINUE
C
C      SET XVCYL TO ZERO AND CALCULATE THE DENSITY OF THE NON-VAPOR MASS
C      FRACTION.
C
C      XVCYL = 0.D0
C
C      DENLS = MTOT*(1.D0-XVOL)/(VOL-VVOL)
C
C      IF (ISPLIT.NE.1) GO TO 90
C
C      IF THE LIQUID LEVEL COINCIDES WITH THE LEVEL OF THE HOLE THE VAPOR
C      MASS FRACTION OF THE RELEASE IS RECALCULATED. VLFACE IS SET TO ZERO
C      SO THAT THE PRESSURE OF THE RELEASE WILL EQUAL THE SATURATION
C      PRESSURE.
C
C      XVCYL = YVCYL*DENVAP/DENLS
C      *      / (1.D0 - YVCYL + YVCYL*DENVAP/DENLS)
C
C      VLFACE = 0.D0
C
C      90 CONTINUE
C
C      CALCULATE RELEASE PRESSURE. NO CORRECTION IF VLFACE IS ZERO.
C
C      PCYL = PVOL + VLFACE*DENLS/1728.D0
C
C      100 CONTINUE
C
C      VLFACE = OLDFLF
C
C      THIS SUBROUTINE CANNOT PROVIDE REASONABLE RESULTS IF THE UF6 GOES
C      SOLID BEFORE THE INTERFACE DROPS BELOW THE BOTTOM OF THE HOLE. CHECK
C      FOR THIS RESULT AND STOP IF A PROBLEM IS ENCOUNTERED.
C
C      IF (XLCYL.EQ.0.D0.AND.XVCYL.NE.1.D0) STOP11
C
C      RETURN
C
C      END

```

## B.16 MIXFLW

```

      SUBROUTINE MIXFLW (IC, INLET, INODES)
C
C      *****
C      *
C      * WARNING ! THIS SUBROUTINE USES THE NULL VECTOR (NODE 30) FOR
C      * INTERMEDIATE STORAGE. NODE 30 VALUES ARE RESET TO THOSE VALUES
C      * ASSIGNED BY THE SUBROUTINE SETRAY.
C      *
C      *

```

```

C *****
C
C THIS SUBROUTINE COMBINES UP TO 4 INLET STREAMS AND DETERMINES THE
C OUTLET PHASE COMPOSITION AND TEMPERATURE AT A GIVEN FINAL PRESSURE.
C IF REACTIVE COMPONENTS ARE IN THE STREAMS, THEY ARE ALLOWED TO
C REACT TO THE EXTENT OF THE LIMITING REACTANT. ALL INLET STREAMS MUST
C BE BLOWER NODES.
C
C THE FOLLOWING VARIABLES ARE USED IN THIS SUBROUTINE.
C
C INPUT VARIABLES
C
C IC          NODE NUMBER REPRESENTING COMBINED STREAM
C INLET       NUMBER OF STREAMS TO BE MIXED (MAXIMUM OF 4)
C INODES      MAXIMUM NUMBER OF NODES ALLOWED BY THE SET OF
C             SUBROUTINES OF WHICH THIS SUBROUTINE IS A PART,
C             CORRESPONDS TO THE NULL VECTOR NODE NUMBER
C
C COMMON BLOCK VARIABLES
C
C MASS (30,9) COMPONENT MASS FLOW RATE, LB/(DELTA)
C TC (30)   NODE TEMPERATURE, DEG F
C PC (30)   NODE PRESSURE, PSIA
C ACFM (30) VOLUMETRIC FLOW RATE THROUGH STREAM NODE,
C           FT**3/MIN
C H (30)   NODE ENTHALPY RATE, BTU/(DELTA)
C IIN (30,4) NODE INPUT STREAM NUMBER
C IOUT (30,4) NODE OUTPUT STREAM NUMBER
C AMINLN   MINIMUM NATURAL LOG ACCEPTED BY THE COMPUTER
C DELT     TIME INTERVAL USED IN TRANSIENT SIMULATION, SEC
C
C INTERNAL VARIABLE
C
C IOUTMP    TEMPORARY STORAGE VARIABLE
C
C THE FOLLOWING SUBROUTINE IS CALLED BY MIXFLW.
C
C COMPRT
C
C THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED.
C
C DENTHL
C DENUF6
C HFPLY
C HHFH20
C HUF6
C PHASE
C PHFH20
C VPRUF6
C ZUF6
C
C IMPLICIT REAL*8 (A-H,J-Z)
C
C COMMON /LBMASS/ MASS(30,9), DUM1

```

```

COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
COMMON /VOLUME/ ACFM(30), DUM3(61)
COMMON /ENTHAL/ H(30), DUM4(120)
COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
COMMON /CONTRL/ AMINLN, DUM5, DELT, DUM6, IDUM1, DUM7
C
C SPECIFY INITIAL ESTIMATES OF MIXED STREAM TEMPERATURE AND VOLUME
C FLOW RATE.
C
C   IF (TC(IC).EQ.0.D0) TC(IC) = TC(IIN(IC,1))
C
C   IF (ACFM(IC).GT.0.D0) GO TO 20
C
C   ACFM(IC) = 0.D0
C
C   DO 10 I10=1,INLET
C
C       ACFM(IC) = ACFM(IC) + ACFM(IIN(IC,I10))
C
C 10 CONTINUE
C
C 20 CONTINUE
C
C   ACFM(IC) = ACFM(IC)*DELT/6.D1
C
C SET NODE IC COMPONENT MASS AND ENTHALPY RATES TO ZERO AND TEMPORARILY
C SET THE OUTLET NODE OF NODE IC TO THE NULL VECTOR.
C
C   DO 30 I30=1,9
C
C       MASS(IC,I30) = 0.D0
C
C 30 CONTINUE
C
C   H(IC) = 0.D0
C
C   IOUTMP = IOUT(IC,1)
C
C   IOUT(IC,1) = 30
C
C COMBINE STREAMS TO OBTAIN COMPONENT MASS AND ENTHALPY RATES, THEN
C RESET OUTLET STREAM NODE FOR NODE IC.
C
C   CALL COMPRT (IC, INLET, INODES)
C
C   IOUT(IC,1) = IOUTMP
C
C SET "NULL VECTOR" VALUES TO BEGIN ITERATION TO OBTAIN MIXED STREAM
C PHASE COMPOSITION AND TEMPERATURE AS WELL AS VOLUME FLOW RATE WHICH
C CORRESPOND TO THE OUTLET PRESSURE.
C
C   ACFM(30) = ACFM(IC)*PC(IC)/PC(IOUT(IC,1))
C
C   H(30) = H(IC)

```

```

C
C   TC(30) = TC(IC)
C
C   DO 40 I40=1,9
C
C       MASS(30,I40) = MASS(IC,I40)
C
C   40 CONTINUE
C
C   50 CONTINUE
C
C       CALL COMPRT (30, 1, INODES)
C
C       IF (DABS(PC(30) - PC(IOUT(IC,1)))<.LT.1.D-4) GO TO 60
C
C       ACFM(30) = ACFM(30)*PC(30)/PC(IOUT(IC,1))
C
C       GO TO 50
C
C   60 CONTINUE
C
C   TRANSFER TEMPORARY VALUES STORED IN THE NULL VECTOR TO NODE VECTOR
C   IC, THEN RESET NULL VECTOR VALUES.
C
C       DO 70 I70=1,9
C
C           MASS(IC,I70) = MASS(30,I70)
C           MASS(30,I70) = 0.D0
C
C   70 CONTINUE
C
C       PC(IC) = PC(30)
C       PC(30) = 0.D0
C
C       TC(IC) = TC(30)
C       TC(30) = 0.D0
C
C       H(30) = 0.D0
C
C       ACFM(IC) = 6.D1*ACFM(30)/DELT
C       ACFM(30) = 0.D0
C
C       RETURN
C
C       END

```

## B.17 PHASE

```

C       SUBROUTINE PHASE (TF, IC)
C
C   THIS SUBROUTINE CALCULATES THE PHASE COMPOSITION OF THE HF-H2O SYSTEM
C   IN A COMPARTMENT. THE FOLLOWING VARIABLES ARE USED.
C
C

```

C TF TEMPERATURE, DEG F  
 C TR ABSOLUTE TEMPERATURE, DEG R  
 C IC NUMBER OF NODE BEING EVALUATED  
 C MASS MASS OF COMPONENT IN NODE, LB  
 C MSSH2O MASS OF WATER IN NODE, LB  
 C MSSHF MASS OF HF IN NODE, LB  
 C MSSTOT COMBINED MASS OF H2O AND HF IN NODE, LB  
 C MSSVAP MASS OF HF AND H2O VAPOR IN NODE, LB  
 C WMOL COMPONENT MOLECULAR WEIGHT, LB/LB MOLE  
 C MW ESTIMATED MOLECULAR WEIGHT OF HF VAPOR, LB/LB MOLE  
 C VOL VOLUME OF NODE, FT\*\*3  
 C WHFL WEIGHT FRACTION OF HF IN THE HF-H2O LIQUID CONDENSATE,  
 C LB HF LIQ/LB HF-H2O LIQ MIX  
 C WHFV WEIGHT FRACTION OF HF IN THE HF-H2O VAPOR MIXTURE,  
 C LB HF VAP/LB HF-H2O VAP MIX  
 C WHFTOT WEIGHT FRACTION HF IN THE HF-H2O SYSTEM, LB HF/LB HF+H2O  
 C AZEOTR WEIGHT FRACTION OF HF IN AN HF-H2O MIXTURE OF AZEOTROPIC  
 C COMPOSITION, LB HF/LB HF-H2O MIX  
 C WHF WEIGHT FRACTION OF HF IN THE LIQUID REQUIRED TO YIELD  
 C PHF BASED ON THE CONCENTRATION OF HF ASSUMED TO BE  
 C VAPOR ONLY, LB HF LIQUID/LB HF-H2O LIQ MIX  
 C PHF PARTIAL VAPOR PRESSURE OF HF, PSIA  
 C PH2O PARTIAL VAPOR PRESSURE OF H2O, PSIA  
 C PSUM VAPOR PRESSURE OF THE HF-H2O SYSTEM, PSIA  
 C YHF MOLE FRACTION OF HF IN THE HF-H2O VAPOR SYSTEM, MOLES HF  
 C VAPOR/MOLES HF-H2O VAPOR MIXTURE  
 C NVAP MOLES OF HF-H2O VAPOR MIXTURE, MOLES/LB PLUME  
 C PCALC PARTIAL PRESSURE OF HF-H2O VAPOR MIXTURE RESULTING FROM  
 C NVAP, VOLUME, AND TR, PSIA  
 C PDIF PCALC - PSUM  
 C PCONV PRESSURE CONVERSION FACTOR FROM TORR TO PSIA  
 C AMINLN MINIMUM NATURAL LOG ACCEPTED BY COMPUTER  
 C LNPHF LN(PHF/PCONV)  
 C  
 C A, B COEFFICIENTS FOR  $\text{LN}(\text{PHF}) = A/\text{TR} + B$   
 C  
 C LNPHF1, LNPHF2 LN(PHF) AT I AND I + 1  
 C  
 C IJ INDEX CONTROLLING PHASE ITERATION SCHEME  
 C ICOUNT COUNTER FOR PHASE ITERATION SCHEME

C THE FOLLOWING SUBROUTINES ARE CALLED.

C HFPLY  
 C PHFH2O

C IMPLICIT REAL\*8 (A-H,J-Z)

C DIMENSION WHFL(3), PDIF(3)  
 C DIMENSION A(20), B(20)

C COMMON /LBMASS/ MASS(30,9), DUM1  
 C COMMON /VOLUME/ VOL(30), DUM2(61)  
 C COMMON /MOLWT/ WMOL(9)



```

COMMON /CONTRL/ AMINLN, DUM3, DUM4(2), IDUM1, DUM5
C
DATA A /-10689D0,-10536D0,-10647D0,-10675D0,-10460D0,-10362D0,
* -9779.5D0,-8917.7D0,-8188.2D0,-7770.0D0,-7575.0D0,-7411.4D0,
* -7315.7D0,-7163.4D0,-6984.3D0,-6459.7D0,-6269.7D0,-5891.7D0,
* -5849.8D0,-5641.0D0/
C
DATA B /17.680D0,18.069D0,18.793D0,19.409D0,19.595D0,19.951D0,
* 19.429D0,18.948D0,18.256D0,17.975D0,18.054D0,18.178D0,
* 18.365D0,18.457D0,18.492D0,17.857D0,17.812D0,17.391D0,
* 17.555D0,17.364D0/
C
TR      = TF + 459.67D0
PCONV   = 14.696D0/7.6D2
C
MSSHF   = MASS(IC,4) + MASS(IC,5)
MSSH2O  = MASS(IC,2) + MASS(IC,3)
MSSTOT  = MSSHF + MSSH2O
C
WHFTOT  = MSSHF/MSSTOT
C
C THE FOLLOWING SECTION EVALUATES THE WEIGHT FRACTION OF HF IN THE
C LIQUID, WHF, REQUIRED TO YIELD PHF BASED ON THE ASSUMPTION THAT ALL
C HF IS IN THE VAPOR PHASE. IF THE REQUIRED WHF IS GREATER THAN ONE,
C CONDENSATION WILL OCCUR. IF WHF IS LESS THAN OR EQUAL TO ONE, PSUM
C CORRESPONDING TO WHF IS CALCULATED AND COMPARED TO PHF + PH2O EVALU-
C ATED ASSUMING ALL HF AND H2O IS IN THE VAPOR PHASE. IF PSUM IS LESS
C THAN PHF + PH2O, CONDENSATION WILL OCCUR.
C
10 CONTINUE
C
PHF      = MSSHF*TR*10.73D0/VOL(IC)/WMOL(5)
C
CALL HFPLY (TF, PHF, MW, .TRUE.)
C
IF (DABS(MW-WMOL(5)).LT.1.D-4) GO TO 20
C
WMOL(5) = (MW + WMOL(5))/2.D0
C
GO TO 10
C
20 CONTINUE
C
WMOL(5) = MW
C
PH2O     = MSSH2O*TR*10.73D0/VOL(IC)/WMOL(3)
C
LNPHF    = AMINLN
C
IF (PHF.GT.0.D0) LNPHF = DLOG(PHF/PCONV)
C
C THE FOLLOWING EQUATION APPLIES FOR WHF BETWEEN 0.00 AND 0.05.
C
WHF      = PHF*0.05D0/PCONV/DEXP(A(1)/TR + B(1))

```

```

C
C   IF (WHF.LT.0.05D0) GO TO 40
C
C   THE FOLLOWING SET OF ITERATIVE EQUATIONS IS APPLICABLE BETWEEN 0.05
C   AND 1.00. IF WHF IS FOUND TO BE GREATER THAN 1 ON THE INTERATION 19,
C   CONDENSATION OCCURS.
C
C   DO 30 I30 = 1,19
C
C       LNPHF1 = A(I30)/TR + B(I30)
C       LNPHF2 = A(I30+1)/TR + B(I30+1)
C
C       WHF    = 0.05D0*((LNPHF - LNPHF1)/(LNPHF2 - LNPHF1)
*           + DFLOAT(I30))
C
C       IF (WHF.GE.(0.05D0*DFLOAT(I30)).AND.WHF.LE.
*           (0.05D0*DFLOAT(I30+1))) GO TO 40
C
C   30 CONTINUE
C
C       IF (WHF.GT.1.00) GO TO 50
C
C   40 CONTINUE
C
C       CALL PHFH20 (TF, WHF, 0.00, 0.00, 0.00, PSUM)
C
C       IF (PSUM.LT.(PHF+PH20)) GO TO 50
C
C       MASS(IC,5) = MSSHF
C       MASS(IC,4) = 0.00
C       MASS(IC,3) = MSSH20
C       MASS(IC,2) = 0.00
C
C       RETURN
C
C   50 CONTINUE
C
C   IF CONDENSATION OCCURS, THE FOLLOWING SECTION EVALUATES THE
C   EQUILIBRIUM VAPOR PHASE COMPOSITION AT TF.
C
C       IF (MSSHF.EQ.0.00.OR.MSSH20.EQ.0.00) GO TO 60
C
C       AZEOTR = 0.3826D0
C
C       IF (DABS(AZEOTR-WHFTOT).GE.1.D-6) GO TO 70
C
C   THE FOLLOWING SECTION EVALUATES THE VAPOR CONCENTRATION AT THE
C   AZETROPE OR FOR A PURE COMPONENT.
C
C   60 CONTINUE
C
C       CALL PHFH20 (TF,WHFTOT,YHF,PHF,PH20,PSUM)
C
C       IF (MSSHF.GT.0.00) CALL HFPOLY (TF,PHF,WMOL(5),.TRUE.)

```

```

C
  MASS(IC,5) = PHF*VOL(IC)*WMOL(5)/10.73D0/TR
  MASS(IC,4) = MSSHF-MASS(IC,5)
  MASS(IC,3) = PH20*VOL(IC)*WMOL(3)/10.73D0/TR
  MASS(IC,2) = MSSH20-MASS(IC,3)
C
  RETURN
C
70 CONTINUE
C
  ICOUNT = 0
C
  WHFL(1) = AZEOTR + DSIGN(1.D-6,(WHFTOT-AZEOTR))
  WHFL(2) = WHFTOT
C
  IJ      = 1
C
  GO TO 90
C
80 CONTINUE
C
  IJ      = 2
C
90 CONTINUE
C
  CALL PHFH20 (TF,WHFL(IJ),YHF,PHF,PH20,PSUM)
C
  CALL HFPLY (TF,PHF,WMOL(5),.TRUE.)
C
  WHFV    = YHF*WMOL(5)/(YHF*WMOL(5) + (1.D0 - YHF)*WMOL(3))
C
  MSSVAP = (MSSH20*WHFL(IJ) - MSSHF*(1.D0 - WHFL(IJ)))
1         / (WHFL(IJ) - WHFV)
C
  NVAP    = MSSVAP*WHFV/WMOL(5) + MSSVAP*(1.D0 - WHFV)/WMOL(3)
C
  PCALC   = NVAP*10.73D0*TR/VOL(IC)
C
  PDIF(IJ) = PCALC - PSUM
C
  IF (IJ - 2) 80,100,110
C
100 CONTINUE
C
  ICOUNT = ICOUNT + 1
C
  IJ      = 3
C
  M       = (PDIF(2) - PDIF(1))/(WHFL(2) - WHFL(1))
C
  WHFL(3) = WHFL(2) - PDIF(2)/M
C
  IF ((PDIF(1)-PDIF(2)).GE.PSUM) WHFL(3) = (WHFL(1) + WHFL(2))/2.D0
C

```

```

      GO TO 90
C
110 CONTINUE
C
      IF (DABS(PDIF(3)).LT.(PSUM*1.D-3)) GO TO 140
C
      IF (ICOUNT.EQ.100) STOP12
C
      IF (PDIF(3)) 120,140,130
C
120 CONTINUE
C
      WHFL(2) = WHFL(3)
      PDIF(2) = PDIF(3)
C
      GO TO 100
C
130 CONTINUE
C
      WHFL(1) = WHFL(3)
      PDIF(1) = PDIF(3)
C
      GO TO 100
C
140 CONTINUE
C
      MASS(IC,5) = MSSVAP*WHFV
      MASS(IC,4) = MSSHF-MASS(IC,5)
      MASS(IC,3) = MSSVAP*(1.D0 - WHFV)
      MASS(IC,2) = MSSH2O-MASS(IC,3)
C
      RETURN
C
      END

```

## B.18 PHFH2O

```

      SUBROUTINE PHFH2O (TF, WHFL, YHF, PHF, PH2O, PSUM)
C
C THIS ROUTINE CALCULATES THE MOLE FRACTION OF HF IN THE VAPOR PHASE OF
C THE HF-H2O SYSTEM AS WELL AS THE PARTIAL VAPOR PRESSURES OF HF AND
C H2O AND THEIR SUM GIVEN THE TEMPERATURE IN DEG F AND THE WEIGHT
C FRACTION OF HF IN THE LIQUID PHASE. THE FOLLOWING VARIABLES ARE USED.
C
C      TF      TEMPERATURE, DEG F
C      TR      TEMPERATURE, DEG R
C      WHFL    WEIGHT FRACTION OF HF IN THE LIQUID HF-H2O MIXTURE,
C             LB HF LIQ/LB HF-H2O LIQ MIX
C      YHF     MOLE FRACTION OF HF IN THE VAPOR HF-H2O MIXTURE,
C             MOLES HF VAPOR/MOLES HF-H2O VAPOR
C      PHF     PARTIAL VAPOR PRESSURE OF HF, PSIA
C      PH2O    PARTIAL VAPOR PRESSURE OF H2O, PSIA
C      PSUM    VAPOR PRESSURE OF THE HF-H2O VAPOR MIXTURE, PSIA

```

```

C      PCONV  CONVERSION FACTOR FROM TORR TO PSIA, PSIA/TORR
C
C      A, B    COEFFICIENTS FOR LN(PHF) = A/TR + B
C
C      LNPHF1, LNPHF2  LN(PHF) EVALUATED AT I1 AND I2
C      I1, I2  INDICES FOR EVALUATING PHF (I2 = I1 + 1)
C
C      LNPHF   LN(PHF)
C      AMINLN  MINIMUM NATURAL LOG ACCEPTED BY COMPUTER
C      MWAZ    MOLECULAR WEIGHT OF HF VAPOR AT THE AZEOTROPE,
C             LB/LB MOLE
C      AZEOTR  AZEOTROPIC WEIGHT FRACTION OF HF IN THE HF-H2O SYSTEM
C      PHFAZ   PARTIAL VAPOR OF HF AT THE AZEOTROPIC COMPOSITION
C      PH2OAZ  PARTIAL VAPOR OF H2O AT THE AZEOTROPIC COMPOSITION
C      PAZEOT  PHFAZ + PH2OAZ
C
C      IMPLICIT REAL*8 (A-H,J-Z)
C
C      DIMENSION A(20), B(20)
C
C      COMMON /CONTRL/ AMINLN
C
C      DATA A /-10689D0,-10536D0,-10647D0,-10675D0,-10460D0,-10362D0,
*      -9779.5D0,-8917.7D0,-8188.2D0,-7770.0D0,-7575.0D0,-7411.4D0,
*      -7315.7D0,-7163.4D0,-6984.3D0,-6459.7D0,-6269.7D0,-5891.7D0,
*      -5849.8D0,-5641.0D0/
C
C      DATA B /17.680D0,18.069D0,18.793D0,19.409D0,19.595D0,19.951D0,
*      19.429D0,18.948D0,18.256D0,17.975D0,18.054D0,18.178D0,
*      18.365D0,18.457D0,18.492D0,17.857D0,17.812D0,17.391D0,
*      17.555D0,17.364D0/
C
C      TR      = TF + 459.67D0
C
C      PCONV   = 14.696D0/7.6D2
C
C      THE FOLLOWING SEQUENCE OF EQUATIONS THROUGH "30 CONTINUE" EVALUATES
C      THE PARTIAL VAPOR PRESSURE OF HF. THESE EQUATIONS ARE BASED ON A PLOT
C      OF PARTIAL VAPOR PRESSURE OF HF VS TEMPERATURE AS A FUNCTION OF
C      WEIGHT FRACTION OF HF IN THE LIQUID PHASE. THIS PLOT WAS PROVIDED TO
C      W. REID WILLIAMS BY BRIAN C. ROGERS OF ALLIED CHEMICAL, SOLVAY, NY,
C      IN A LETTER DATED JULY 26, 1983. THE EQUATIONS WERE DERIVED BY W. R.
C      WILLIAMS.
C
C      PHF     = 0.0D0
C
C      IF (WHFL.LE.(DEXP(AMINLN+6.D0))) GO TO 30
C
C      I1      = IDINT(WHFL/0.05D0)
C
C      IF (I1.EQ.20) I1 = 19
C
C      I2      = I1 + 1
C

```

```

      IF (I1.EQ.0) GO TO 10
C
      LNPHF1 = A(I1)/TR + B(I1)
C
10 CONTINUE
C
      LNPHF2 = A(I2)/TR + B(I2)
C
      IF (I1.EQ.0) GO TO 20
C
C THE FOLLOWING EQUATION APPLIES FOR WHFL BETWEEN 0.05 AND 1.00.
C
      LNPHF = LNPHF1 + (LNPHF2 - LNPHF1)*(WHFL/0.05 - DFLOAT(I1))
C
      PHF = PCONV*DEXP(LNPHF)
C
      GO TO 30
C
20 CONTINUE
C
C THE FOLLOWING EQUATION APPLIES FOR WHFL BETWEEN 0.00 AND 0.05.
C
      PHF = (WHFL/0.05D0)*PCONV*DEXP(LNPHF2)
C
30 CONTINUE
C
C THE FOLLOWING SEQUENCE OF EQUATIONS THROUGH "60 CONTINUE" EVALUATES
C A PSEUDO PARTIAL VAPOR PRESSURE FOR H2O. THE EQUATIONS ARE BASED ON
C THE VAPOR PRESSURE OF WATER GIVEN IN R. C. REID, J. M. PRAUSNITZ, AND
C T. K. SHERWOOD, THE PROPERTIES OF GASES AND LIQUIDS, 3RD ED., MCGRAW-
C HILL BOOK COMPANY, 1977, PP. 629 AND 632, AN ESTIMATED VALUE OF THE
C PARTIAL VAPOR PRESSURE OF H2O AT THE AZEOTROPE, AND THE REQUIREMENT
C THAT PH2O = 0 AT WHFL = 1. THE EQUATIONS USED BELOW WERE DERIVED BY
C W. R. WILLIAMS.
C
C THE FOLLOWING EQUATION GIVES THE VAPOR PRESSURE OF H2O.
C
      PH2O = PCONV*DEXP(18.3034D0 - 6869.59D0/(TF + 376.64D0))
C
      IF (WHFL.EQ.0.D0) GO TO 50
C
C THE FOLLOWING SEQUENCE OF EQUATIONS ESTIMATES THE PARTIAL VAPOR
C PRESSURE OF H2O AT THE AZEOTROPE.
C
      LNPHF1 = A(7)/TR + B(7)
C
      LNPHF2 = A(8)/TR + B(8)
C
      AZEOTR = 0.3826D0
C
      LNPHF = LNPHF1 + (LNPHF2 - LNPHF1)*(AZEOTR - 0.35D0)/0.05D0
C
      PHFAZ = PCONV*DEXP(LNPHF)
C

```

```

C IN THE FOLLOWING CALL TO HFPOLY, THE LOGICAL VARIABLE C1C3C6 IS
C SPECIFIED AS .FALSE. SINCE PREVIOUS ESTIMATES OF C1, C3, AND C6
C SHOULD NOT BE CHANGED.
C
C   CALL HFPOLY (TF, PHFAZ, MNAZ, .FALSE.)
C
C   YHF   = (AZEOTR/MNAZ)/(AZEOTR/MNAZ + (1.00 - AZEOTR)/18.01600)
C
C   PH2OAZ = (1.00 - YHF)*PHFAZ/YHF
C
C   IF (WHFL.GT.0.382600) GO TO 40
C
C THE FOLLOWING EQUATIONS APPLY FOR WHFL BETWEEN 0.0 AND THE AZEOTROPE.
C
C   PAZEOT = PHFAZ + PH2OAZ
C
C   PSUM   = PH2O + (PAZEOT - PH2O)*WHFL/AZEOTR
C
C   PH2O   = PSUM - PHF
C
C   GO TO 60
C
C 40 CONTINUE
C
C THE FOLLOWING EQUATION APPLIES FOR WHFL BETWEEN THE AZEOTROPE AND 1.
C
C   PH2O   = PH2OAZ*((1.00 - WHFL)/(1.00 - AZEOTR))**3
C
C 50 CONTINUE
C
C   PSUM   = PHF + PH2O
C
C 60 CONTINUE
C
C   YHF   = PHF/PSUM
C
C   RETURN
C
C   END

```

## B.19 PIPSYS

SUBROUTINE PIPSYS(G)

```

C
C THE PIPSYS SUBROUTINE RECALCULATES THE MASS VELOCITY AS IT MOVES DOWN
C THE LENGTH OF THE PIPE AND FIXTURE SYSTEM. THE INITIAL MASS VELOCITY
C SUPPLIED TO PIPSYS CORRESPONDS TO THE ENTRANCE EFFECT PRESSURE DROP.
C THE TRUE MASS VELOCITY MUST BE LESS THAN OR EQUAL TO THIS FIGURE. SO
C A NEW GUESS OF MASS VELOCITY IS CALCULATED.
C
C *****
C *
C * WARNING: THE VALUE OF MASS VELOCITY, G, IS CONSTANT ONLY *

```

```

C      *      IF THE PIPING SYSTEM DIAMETER IS CONSTANT.  HOWEVER,      *
C      *      MASS FLOW RATE IS CONSTANT.  THESE VALUES ARE RELATED      *
C      *      THROUGH PIPE DIAMETERS.  THE VALUE GFAT IS CALCULATED      *
C      *      WHEN A MASS VELOCITY POTENTIALLY DIFFERENT FROM THE      *
C      *      INITIAL G CAN BE EXPECTED FOR A PARTICULAR DOWNSTREAM      *
C      *      FEATURE.                                                    *
C      *                                                                 *
C      *****
C
C      IMPLICIT REAL*8 (A-H,J-Z)
C
C      COMMON /ICOMON/ ISEN, IPIG, IBRCH, IGEXIT
C      COMMON /CONCYL/ PCYL,TCYL,XVCYL,XLCYL,MW
C      COMMON /CONENT/ PENT,TENT,XVENT,XLENT,UNTBAR
C      COMMON /GMTRY / PIGRAY
C      COMMON /CNSTNT/ ALPHA,BETA,DELTA,GAMMA,EPSLN
C      COMMON /TRIPLE/ TTRIPL,PTRIPL
C
C      DIMENSION PIGRAY(99,3),CONRAY(99,6)
C
C      TWELTH = 1.00/12.00
C
C      REYNMX = 1.1504
C
C      THE IGEXIT SWITCH CONTROLS THE CALCULATION OF THE EXIT.  AT A VALUE
C      OF IGEXIT=2 THE EXIT IS KNOWN TO BE CONTROLLED BY PRESSURE DROP AND
C      THE FURTHER CALCULATION OF GMAX VALUES SHOULD BE SUPPRESSED.
C
C      IGEXIT = 1
C
C      TO BEGIN THE PIPE SYSTEM CALCULATION, A GUESS FOR G ONE-HALF THE
C      VALUE ENTERED AS PIPSYS WAS CALLED (WHICH MIGHT BE A CHOKE FLOW
C      VALUE) IS USED IN CALCULATING THE ENTRY PRESSURE DROP.  A NEW GMAX FOR
C      CHOKE FLOW IS THEN DETERMINED AND IF THIS VALUE IS LESS THAN THE
C      ASSUMED G, THE ASSUMED G IS REDUCED BEFORE ENTRY CONDITIONS ARE
C      RECALCULATED.
C
C      CONRAY(IPIG,1) = PIGRAY(IPIG,3)
C
C      SET UPPER AND LOWER BOUNDS ON G AND MAKE FIRST GUESS.
C
C      CONRAY(IPIG,5) = 1.D10
C
C      IF (IBRCH.LT.3) CONRAY(IPIG,5) = G
C
C      CONRAY(IPIG,6) = 0.00
C
C      IF (IBRCH.LT.3) G      = G/2.00
C
C      10 CONTINUE
C
C      ON RETURNING TO THIS POINT IN THE SUBROUTINE (I.E., 10 CONTINUE), THE
C      VALUE OF G HAS BEEN ADJUSTED AND THE ENTIRE PIPE SYSTEM CALCULATION
C      IS REPEATED STARTING WITH THE ENTRANCE EFFECT.

```



```

C
C   IF ( (CONRAY(IPIG,5)-CONRAY(IPIG,6)) / (CONRAY(IPIG,5)+
*     CONRAY(IPIG,6)) .LT.EPSLN) GO TO 200
C
C 20 CONTINUE
C
C   PENT = PCYL-PIGRAY(1,2)*G**2/DELTA*UNTBAR
C
C   CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,PENT,ISEN,XVENT,XLENT,TENT)
C
C   CALL DENUF6(TENT,PENT,MW,RHOS,RHOL,RHOV)
C
C   OLDVBR = UNTBAR
C
C   UNTBAR = XVENT/RHOV+(1.D0-XVENT)*XLENT/RHOL
*     +(1.D0-XVENT)*(1.D0-XLENT)/RHOS
C
C A NEW SET OF ENTRANCE CONDITIONS BASED ON THE NEW VALUE OF MASS
C VELOCITY HAS BEEN COMPUTED.
C
C   IF (DABS(UNTBAR-OLDVBR).GT.(EPSLN)) GO TO 20
C
C   P2 = PENT-1.D-3
C
C EVALUATE GMAX BASED ON ISENTROPIC EXPANSION.
C
C   ISNGMX = 0
C
C   CALL FLASH (TENT, PENT, MW, XVENT, XLENT, P2, ISNGMX,
*     XV2, XL2, T2)
C
C   CALL DENUF6(T2,P2,MW,RHOS,RHOL,RHOV)
C
C   V2BAR = XV2/RHOV+(1.D0-XV2)*XL2/RHOL
*     +(1.D0-XV2)*(1.D0-XL2)/RHOS
C
C   GMAX = DSQRT(ALPHA*(PENT-P2)/(V2BAR-UNTBAR))
C
C   IF (GMAX.LE.G) GO TO 180
C
C LOAD THE FIRST ROW OF CONRAY.
C
C   CONRAY(1,1) = PENT
C   CONRAY(1,2) = TENT
C   CONRAY(1,3) = XVENT
C   CONRAY(1,4) = XLENT
C   CONRAY(1,5) = UNTBAR
C   CONRAY(1,6) = GMAX
C
C   IFEAT = 2
C
C 30 CONTINUE
C
C   IF (IFEAT.EQ.IPIG) GO TO 150

```

```

C
C   GO TO (40,100,130), IDINT(PIGRAY(IFEAT,1))
C
C 40 CONTINUE
C
C THE PIPE SOLVER STARTS HERE BY LIMITING THE TOTAL NUMBER OF STEPS TO
C THE PRESSURE DIFFERENCE BETWEEN THE BEGINNING OF THE PIPE AND THE
C SURROUNDINGS. IN LATER PASSES THE TOTAL PRESSURE DROP CONSIDERED
C WILL BE UPDATED. EACH STEP INCLUDES A CALCULATION OF THE PIPE LENGTH
C CORRESPONDING TO AN INCREMENTAL PRESSURE DROP OF ABOUT ONE PSI.
C
C   DELTAP = CONRAY((IFEAT-1),1)-CONRAY(IPIG,1)
C
C THE TRIPLE POINT PRESSURE MUST NOT BE INCLUDED IN DELTAP IF FLASHING
C FLOW IS OCCURRING.
C
C   IF (CONRAY((IFEAT-1),1).GT.PTR IPL .AND.
*   CONRAY(IPIG,1).LT.PTR IPL .AND.
*   CONRAY((IFEAT-1),3).NE.1.D0)
*   DELTAP = CONRAY((IFEAT-1),1)-PTR IPL
C
C   IF (DELTAP.LE.0.D0) GO TO 180
C
C   ICON   = 1
C
C 50 CONTINUE
C
C   IDELP  = IDINT(DELTAP)
C
C   IF (IDELP.EQ.0) IDELP = 1
C
C   DELP   = DELTAP/DFLOAT(IDELP)
C   P1     = CONRAY((IFEAT-1),1)
C   T1     = CONRAY((IFEAT-1),2)
C   XV1    = CONRAY((IFEAT-1),3)
C   XL1    = CONRAY((IFEAT-1),4)
C   V1BAR  = CONRAY((IFEAT-1),5)
C   DLSUM  = 0.D0
C
C ADJUST THE MASS VELOCITY BASED ON THE ENTRANCE DIAMETER TO THE
C CURRENT DIAMETER.
C
C   GFEAT = G*(PIGRAY(1,3)**2)/(PIGRAY(IFEAT,3)**2)
C
C   DO 80 I80 = 1, IDELP
C
C   P2     = P1-DELP
C
C 60 CONTINUE
C
C   PAVG   = (P2+P1)/2.D0
C
C   CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,P2,ISEN,XV2,XL2,T2)
C

```

```

C      CALL DENUF6(T2,P2,MW,RHOS,RHOL,RHOV)
C      V2BAR = XV2/RHOV + (1.D0-XV2)*XL2/RHOL
*      + (1.D0-XV2)*(1.D0-XL2)/RHOS
C      CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,PAVG,ISEN,XVAVG,XLAVG,TAVG)
C      CALL DENUF6(TAVG,PAVG,MW,RHOS,RHOL,RHOV)
C      VBRAVG = XVAVG/RHOV + (1.D0-XVAVG)*XLAVG/RHOL
*      + (1.D0-XVAVG)*(1.D0-XLAVG)/RHOS
C      CALL VISUF6(TAVG,PAVG,MW,VISL,VISV)
C      VIS = (VISV*XVAVG/RHOV + VISL*(1.D0-XVAVG)*XLAVG/RHOL)/VBRAVG
C      REYN = 3600.D0*PIGRAY(IFEAT,3)*GFEAT/VIS
C      BFACTR = 1.D25
C      IF (REYN.GT.1.D3) BFACTR = (37580.D0/REYN)**16
C      AFACTR = 0.D0
C      IF (REYN.GT.1.D3) AFACTR = (2.457D0*
*      DLOG(1.D0/((7.D0/REYN)**0.9D0 + (0.27D0*EPSD))))**16
C      THE EQUATION FOR FRICTION FACTOR IS OF A TYPE WHICH LEADS TO AN ERROR
C      MESSAGE IF REYN IS TOO LARGE. LIMITING REYN WILL NOT AFFECT THIS
C      CALCULATION AT THIS POINT. THIS PROBLEM IS SIMPLY A MACHINE
C      LIMITATION.
C      IF (REYN.GT.REYNMX) REYN = REYNMX
C      FFACTR = 2.D0*((8.D0/REYN)**12
*      + (1.D0/(AFACTR+BFACTR)**1.5D0))**TWELTH
C      DELTAL = (4633.1D0*(P1-P2) + GFEAT**2*(V1BAR-V2BAR))/
*      (2.D0*FFACTR*GFEAT**2*(VBRAVG)/PIGRAY(IFEAT,3)
*      + 32.174D0*DSIN(THETA)/(VBRAVG))
C      IF (DELTAL.LE.0.D0 .AND. IGEXIT.EQ.2) WRITE (5,500) IFEAT
C      IF (DELTAL.LE.0.D0) GO TO 180
C      DLSUM = DLSUM + DELTAL
C      EVALUATE GMAX BASED ON ISENTROPIC EXPANSION.
C      P3 = P2-1.D-3
C      ISNGMX = 0
C      CALL FLASH (T2, P2, MW, XV2, XL2, P3, ISNGMX,

```

```

*      XV3, XL3, T3)
C
  CALL DENUF6(T3,P3,MW,RHOS,RHOL,RHOV)
C
  V3BAR = XV3/RHOV+(1.D0-XV3)*XL3/RHOL
*      +(1.D0-XV3)*(1.D0-XL3)/RHOS
C
  GMAX  = DSQRT(ALPHA*(P2-P3)/(V3BAR-V2BAR))
C
  IF (GMAX.LE.GFEAT .AND. DLSUM.LT.(PIGRAY(IFEAT,2)-0.01D0) .AND.
*    IGEXIT.EQ.2) WRITE (5,510) IFEAT
C
  IF (GMAX.LE.GFEAT .AND. DLSUM.LT.(PIGRAY(IFEAT,2)-0.01))
*    GO TO 180
C
  IF (DABS(DLSUM-PIGRAY(IFEAT,2)).LT.1.D-2) GO TO 90
C
  IF (DLSUM.LT.PIGRAY(IFEAT,2) .AND. ICON.EQ.1) GO TO 70
C
  IF (ICON.EQ.100) STOP13
C
  IF (ICON.EQ.1) PUPPER = P1
  IF (ICON.EQ.1) PLOWER = P2
C
  IF (DLSUM.GT.PIGRAY(IFEAT,2) .AND. ICON.GT.1) PLOWER = P2
  IF (DLSUM.LT.PIGRAY(IFEAT,2) .AND. ICON.GT.1) PUPPER = P2
C
  P2 = (PUPPER + PLOWER)/2.D0
C
  ICON = ICON + 1
C
  DLSUM = DLSUM - DELTAL
C
  GO TO 60
C
70 CONTINUE
C
  P1      = P2
  T1      = T2
  XV1     = XV2
  XL1     = XL2
  V1BAR   = V2BAR
C
80 CONTINUE
C
  GO TO 180
C
90 CONTINUE
C
C PRESSURE DROP EVALUATED FOR TOTAL LENGTH OF CURRENT FEATURE. CHOKE
C FLOW DOES NOT OCCUR IN THE CURRENT FEATURE.
C
  CONRAY(IFEAT,1) = P2
  CONRAY(IFEAT,2) = T2

```

```

CONRAY(IFEAT,3) = XV2
CONRAY(IFEAT,4) = XL2
CONRAY(IFEAT,5) = V2BAR
CONRAY(IFEAT,6) = GMAX*PIGRAY(IFEAT,3)**2/PIGRAY(IFEAT,1)**2
C
  IFEAT = IFEAT + 1
C
C FINISHED WITH PIPE ELEMENT.
C
  GO TO 30
C
100 CONTINUE
C
C EXPANSIONS AND FITTINGS FOR WHICH PRESSURE DROP MUST BE CALCULATED
C ARE HANDLED BY THIS SECTION OF PROGRAMMING.
C
C ADJUST THE MASS VELOCITY BASED ON THE ENTRANCE DIAMETER TO THE
C CURRENT DIAMETER.
C
  GFEAT = G*(PIGRAY(1,3)**2)/(PIGRAY(IFEAT,3)**2)
C
  CONRAY(IFEAT,1) = CONRAY((IFEAT-1),1)
*      - PIGRAY(IFEAT,2) * GFEAT**2/DELTA
*      * CONRAY((IFEAT-1),5)
C
  CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,CONRAY(IFEAT,1),ISEN,
*      CONRAY(IFEAT,3),CONRAY(IFEAT,4),CONRAY(IFEAT,2))
C
  CALL DENUF6 (CONRAY(IFEAT,2),CONRAY(IFEAT,1),MW,RHOS,RHOL,RHOV)
C
  CONRAY(IFEAT,5) =          CONRAY(IFEAT,3)/RHOV
*      + (1.D0-CONRAY(IFEAT,3))*CONRAY(IFEAT,4)/RHOL
*+ (1.D0-CONRAY(IFEAT,3))*(1.D0-CONRAY(IFEAT,4))/RHOS
C
C FOR A SUDDEN EXPANSION, A GMAX VALUE NEED NOT BE CALCULATED. GMAX
C FOR THE PREVIOUS ELEMENT IS PLACED IN THE CONDITIONS ARRAY.
C
  IF (PIGRAY((IFEAT+1),3).GT.PIGRAY(IFEAT,3) .AND.
*      (IFEAT+1).LT.IPIG) GO TO 120
C
110 CONTINUE
C
  P2      = CONRAY(IFEAT,1)-1.D-3
C
C EVALUATE GMAX BASED ON ISENTROPIC EXPANSION.
C
  ISNGMX = 0
C
  CALL FLASH (CONRAY(IFEAT,2), CONRAY(IFEAT,1), MW,
*      CONRAY(IFEAT,3), CONRAY(IFEAT,4), P2, ISNGMX, XV2, XL2, T2)
C
  CALL DENUF6(T2,P2,MW,RHOS,RHOL,RHOV)
C
  V2BAR = XV2/RHOV+(1.D0-XV2)*XL2/RHOL

```

```

      *      + (1.D0-XV2)*(1.D0-XL2)/RHDS
C
      GMAX  = DSQRT(ALPHA*(CONRAY(IFEAT,1)-P2)/
      *      (V2BAR-CONRAY(IFEAT,5)))
C
C IF GMAX IS SMALLER THAN G, THE CALCULATION MUST BE RESTARTED AT A
C NEW, LOWER VALUE OF G.
C
      IF (GMAX.LE.GFEAT) GO TO 180
C
120 CONTINUE
C
      CONRAY(IFEAT,6) = GMAX*PIGRAY(IFEAT,3)**2/PIGRAY(1,3)**2
C
      IF (PIGRAY((IFEAT+1),3).GT.PIGRAY(IFEAT,3) .AND.
      *   (IFEAT+1).LT.IPIG) CONRAY(IFEAT,6) = CONRAY((IFEAT-1),6)
C
      IFEAT  = IFEAT+1
C
      GO TO 30
C
130 CONTINUE
C
C CONTRACTIONS IN THE PIPE SYSTEM ARE HANDLED BY THIS SECTION OF THE
C PROGRAM. SINCE THE PRESSURE DROP IS A FUNCTION OF DOWNSTREAM
C CONDITIONS, AN ITERATION IS REQUIRED. INITIALLY THE SPECIFIC VOLUME
C UPSTREAM IS ASSUMED TO HOLD DOWNSTREAM. THEN A NEW GUESS IS COMPUTED.
C
      ICON  = 1
C
      CONRAY(IFEAT,5) = CONRAY((IFEAT-1),5)
C
C ADJUST THE MASS VELOCITY BASED ON THE ENTRANCE DIAMETER TO
C THE CURRENT DIAMETER.
C
      GFEAT = G*(PIGRAY(1,3)**2)/(PIGRAY(IFEAT,3)**2)
C
140 CONTINUE
C
      CONRAY(IFEAT,1) = CONRAY((IFEAT-1),1)
      *      - PIGRAY(IFEAT,2)*(GFEAT**2)/DELTA
      *      * CONRAY(IFEAT,5)
C
      CALL FLASH (TCYL,PCYL,MW,XVCYL,XLCYL,CONRAY(IFEAT,1),ISEN,
      *      CONRAY(IFEAT,3),CONRAY(IFEAT,4),CONRAY(IFEAT,2))
C
      CALL DENUF6 (CONRAY(IFEAT,2),CONRAY(IFEAT,1),MW,RHOS,RHOL,RHOV)
C
      OLDCON = CONRAY(IFEAT,5)
C
      CONRAY(IFEAT,5) =
      *      CONRAY(IFEAT,3)/RHOV
      *      + (1.D0-CONRAY(IFEAT,3))*CONRAY(IFEAT,4)/RHOL
      *      + (1.D0-CONRAY(IFEAT,3))*(1.D0-CONRAY(IFEAT,4))/RHOS
C

```

```

      ICON  = ICON + 1
C
      IF (ICON.GT.100) STOP14
C
      IF (DABS(CONRAY(IFEAT,5)-OLDCON).GT.EPSLN) GO TO 140
C
      GO TO 110
C
150 CONTINUE
C
C EVALUATION OF PRESSURE DROP ALONG THE PIPING SYSTEM FOR THE CURRENT
C VALUE OF G IS COMPLETE EXCEPT FOR THE EXHAUST PRESSURE DROP.
C
      DELTAP = PIGRAY(IPIG,2)*GFEAT**2*CONRAY((IPIG-1),5)/DELTA
C
C DETERMINE WHETHER THE CURRENT VALUE OF G IS AN UPPER OR LOWER LIMIT.
C
      IF (CONRAY((IPIG-1),1) - DELTAP - PIGRAY(IPIG,3)) 170, 190, 160
C
160 CONTINUE
C
C RESET LOWER BOUND ON G AND INCREASE MASS VELOCITY.
C
      CONRAY(IPIG,6) = G
C
      G      = (G + CONRAY(IPIG,5))/2.00
C
      IF (CONRAY(IPIG,5).EQ.1.0D0) G = CONRAY(IPIG,6)/0.98D0
C
      GO TO 10
C
C RESET UPPER BOUND AND REDUCE MASS VELOCITY.
C
170 CONTINUE
C
      IGEXIT = 2
C
180 CONTINUE
C
      CONRAY(IPIG,5) = G
C
      G      = (G+ CONRAY(IPIG,6))/2.00
C
      IF (CONRAY(IPIG,6).EQ.0.0D0 .AND. IBRCH.EQ.3)
*      G = CONRAY(IPIG,5)*0.98D0
C
      GO TO 10
C
190 CONTINUE
C
      IGEXIT = 2
C
200 CONTINUE
C

```

```

      RETURN
C
500 FORMAT (' ',/, ' WARNING ! CHOKE FLOW PREDICTED IN FEATURE',
*          I3,/, ' AFTER PRESSURE-DROP-CONTROLLED FLOW ESTABLISHED',
*          ' FOR PIPING SYSTEM (DELTA.LE.0).')
C
510 FORMAT (' ',/, ' WARNING ! CHOKE FLOW PREDICTED IN FEATURE',
*          I3,/, ' AFTER PRESSURE-DROP-CONTROLLED FLOW ESTABLISHED',
*          ' FOR PIPING SYSTEM (ISENTROPIC FLASH).')
C
      END

```

## B.20 REMOVE

```

      SUBROUTINE REMOVE (IC, IREMOV)
C
C THIS SUBROUTINE DETERMINES THE MASSES OF CONDENSED PHASES REMOVED BY
C DEPOSITION FROM A ROOM.
C
C THE FOLLOWING VARIABLES ARE USED.
C
C INPUT VARIABLES
C
C IC          NODE NUMBER OF COMPARTMENT FROM WHICH CONDENSATE
C             IS BEING REMOVED BY FALL OUT
C IREMOV      NODE NUMBER OF REMOVAL STREAM
C
C COMMON BLOCK VARIABLES
C
C MASS      (30,9) COMPONENT MASS REMOVAL RATE, LB/(DELTA), OR
C             COMPONENT MASS IN COMPARTMENT, LB
C VOL       (30)   NODE VOLUME, FT**3
C DPAREA   (30)   DEPOSITION AREA, FT**2
C DEPVEL   (30)   DEPOSITION VELOCITY, FT/SEC
C AMINLN   (30)   MINIMUM NATURAL LOG ACCEPTED BY COMPUTER
C DELT     (30)   TIME INTERVAL FOR TRANSIENT SIMULATION, SEC
C TC       (30)   NODE TEMPERATURE, DEG F
C PC       (30)   NODE PRESSURE, PSIA
C H        (30)   ENTHALPY RATE, BTU/(DELTA)
C
C INTERNAL VARIABLE
C
C RMFRAC    REMOVAL FRACTION (VOLUME BASIS)
C
C THE FOLLOWING SUBROUTINE IS CALLED.
C
C          DENTHL
C
C OTHER SUBROUTINES REQUIRED ARE:
C
C          DENUF6
C          HHFH20
C          HUF6

```



```

C          VPRUF6
C          ZUF6
C
C          IMPLICIT REAL*8 (A-H,J-Z)
C
C          COMMON /LBMASS/ MASS(30,9), DUM1
C          COMMON /VOLUME/ VOL(30), DUM2(30), DPAREA(30), DEPVEL
C          COMMON /CONTRL/ AMINLN, DUM3, DELT, DUM4, IDUM1, DUM5
C          COMMON /COMPTP/ TC(30), PC(30), DUM6(30)
C          COMMON /ENTHAL/ H(30), DUM7(120)
C
C          CALCULATE THE REMOVAL FRACTION WHICH IS BASED ON THE VOLUME FROM
C          WHICH CONDENSATES CAN BE REMOVED DURING THE TIME INTERVAL USED
C          FOR THE TRANSIENT ANALYSIS DIVIDED BY THE TOTAL VOLUME OF THE
C          COMPARTMENT. THE FIRST VOLUME IS THE PRODUCT OF THE DEPOSITION
C          VELOCITY, THE DEPOSITION AREA, AND THE TIME INTERVAL.
C
C          RMFRAC = DEPVEL*DPAREA(IC)*DELT/VOL(IC)
C
C          APPLY THE REMOVAL FRACTION, RMFRAC, TO CONDENSED PHASES CONTAINED
C          IN NODE IC.
C
C          MASS(IREMOV,1) = 0.D0
C          MASS(IREMOV,2) = MASS(IC,2)*RMFRAC
C          MASS(IREMOV,3) = 0.D0
C          MASS(IREMOV,4) = MASS(IC,4)*RMFRAC
C          MASS(IREMOV,5) = 0.D0
C          MASS(IREMOV,6) = MASS(IC,6)*RMFRAC
C          MASS(IREMOV,7) = MASS(IC,7)*RMFRAC
C          MASS(IREMOV,8) = 0.D0
C          MASS(IREMOV,9) = MASS(IC,9)*RMFRAC
C
C          SET THE TEMPERATURE AND PRESSURE OF THE REMOVAL STREAM TO THAT OF THE
C          SOURCE NODE, THEN CALCULATE THE ENTHALPY RATE OF THE REMOVAL STREAM.
C
C          TC(IREMOV) = TC(IC)
C          PC(IREMOV) = PC(IC)
C
C          CALL DENTHL (TC(IREMOV), PC(IREMOV), IREMOV, H(IREMOV))
C
C          RETURN
C
C          END

```

## B.21 RESIST

```

C          SUBROUTINE RESIST (IC)
C
C          THIS SUBROUTINE EVALUATES THE RESISTENCE TERM FOR THE RELATIONSHIP
C          DELP = KRCOEF*MASS-FLOW-RATE**2/DENSITY. THE MASS FLOW RATE FOR THE
C          TIME STEP DELT MUST HAVE ALREADY BEEN CALCULATED BEFORE THIS
C          SUBROUTINE IS CALLED UNLESS A RESISTANCE COEFFICIENT FOR THE STREAM
C          HAS BEEN ENTERED.

```

```

C
C THE FOLLOWING VARIABLES ARE USED IN THIS SUBROUTINE:
C
C INPUT VARIABLE
C
C IC          STREAM NODE FOR WHICH RESISTANCE TERM IS TO BE
C             EVALUATED
C
C COMMON BLOCK VARIABLES
C
C MASS      (30,9) COMPONENT NODE MASS OR MASS FLOW RATE, LB
C             (COMPARTMENT) OR LB/(DELT) (STREAM)
C TC        (30)  NODE TEMPERATURE, DEG F
C PC        (30)  NODE PRESSURE, PSIA
C VOL       (30)  COMPARTMENT NODE VOLUME, FT**3
C KRCOEF   (30)  RESISTANCE COEFFICIENT (INPUT), --, OR
C             RESISTANCE TERM (OUTPUT), PSI-SEC**2/LB-FT**3
C
C             NOTE: AS A RESISTANCE TERM, KRCOEF IS A COMBINATION
C             OF THE RESISTANCE TERM, THE CROSS-SECTIONAL
C             AREA OF FLOW, AND CONVERSION FACTORS.
C
C IIN       (30,4) NODE INPUT STREAM NUMBER
C IOUT      (30,4) NODE OUTPUT STREAM NUMBER
C AMINLN    MINIMUM NATURAL LOG ACCEPTED BY THE COMPUTER
C DELT      TIME INTERVAL USED IN TRANSIENT SIMULATION, SEC
C
C EQUIVALENCED VARIABLE
C
C FLAREA   (30)  CROSS-SECTIONAL AREA FOR FLOW, FT**2
C
C INTERNAL VARIABLES
C
C DELP     ABSOLUTE PRESSURE DIFFERENCE ACROSS NODE, PSI
C MASS1    TOTAL MASS IN INLET NODE, LB
C MASS2    TOTAL MASS FLOW RATE IN STREAM NODE, LB/(DELT)
C DENS     DENSITY OF MATERIAL FLOWING INTO THE STREAM
C          NODE, LB/FT**3
C
C IMPLICIT REAL*8 (A-H,J-Z)
C
C DIMENSION FLAREA(30)
C
C COMMON /LBMASS/ MASS(30,9), DUM1
C COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
C COMMON /VOLUME/ VOL(30), KRCOEF(30), DUM3(31)
C COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C COMMON /CONTRL/ AMINLN, DUM4, DELT, DUM5, IDUM1, DUM6
C
C EQUIVALENCE (VOL(1), FLAREA(1))
C
C IF (KRCOEF(IC).LE.0.D0) GO TO 10
C
C IF A POSITIVE RESISTANCE COEFFICIENT HAS BEEN ENTERED, FOR EXAMPLE, A

```

```

C VALUE OF 1.5 CORRESPONDING TO A SUDDEN CONTRACTION FOLLOWED BY A
C SUDDEN EXPANSION, THE RESISTANCE TERM IS EVALUATED USING THE FOLLOW-
C ING EQUATION.
C
C      KRCOEF(IC) = KRCOEF(IC)/FLAREA(IC)/FLAREA(IC)/9266.1D0
C
C      RETURN
C
C 10 CONTINUE
C
C THE REMAINDER OF THIS SUBROUTINE EVALUATES A COEFFICIENT WHICH
C INCORPORATES THE RESISTANCE COEFFICIENT, FLOW AREA, AND CONVERSION
C FACTORS INDIRECTLY BY USING INITIAL STEADY STATE CONDITIONS OF MASS
C FLOW RATE AND PRESSURE DROP.
C
C      DELP = PC(IIN(IC,1)) - PC(IOUT(IC,1))
C
C      MASS1 = 0.D0
C      MASS2 = 0.D0
C
C      DO 20 I20=1,9
C
C          MASS1 = MASS1 + MASS(IIN(IC,1),I20)
C          MASS2 = MASS2 + MASS(IC,I20)
C
C 20 CONTINUE
C
C      DENS = MASS1/VOL(IIN(IC,1))
C
C      KRCOEF(IC) = DELP*DENS*DELT*DELT/MASS2/MASS2
C
C      RETURN
C
C      END

```

## B.22 ROOM

```

      SUBROUTINE ROOM (IC, RATIO)
C
C THIS SUBROUTINE EVALUATES THE INITIAL MASSES AND ENTHALPIES IN NODES
C WHICH REPRESENT ROOMS.
C
C THE FOLLOWING VARIABLES ARE USED.
C
C INPUT VARIABLES
C
C      IC          NUMBER OF NODE BEING INITIALIZED
C      RATIO       RATIO OF THE MOLES OF WATER VAPOR TO THE TOTAL
C                  NUMBER OF MOLES OF MOIST AIR
C
C COMMON BLOCK VARIABLES
C
C      MASS      (30,9) NODE COMPONENT MASS, LB

```

```

C      TC      (30)   NODE TEMPERATURE, DEG F
C      PC      (30)   NODE PRESSURE, PSIA
C      WMOL    (9)    COMPONENT MOLECULAR WEIGHT, LB/LB MOLE
C      H       (30)   NODE ENTHALPY, BTU
C      VOL     (30)   NODE VOLUME, FT**3

```

```

C      INTERNAL VARIABLES

```

```

C      NTOT          TOTAL MOLES OF MOIST AIR IN NODE
C      NH2O          MOLES OF WATER VAPOR IN NODE
C      NAIR          MOLES OF DRY AIR IN NODE

```

```

C      THE FOLLOWING SUBROUTINE IS CALLED.

```

```

C          DENTHL

```

```

C      THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED.

```

```

C          DENUF6
C          HHFH20
C          HUF6
C          VPRUF6
C          ZUF6

```

```

C      IMPLICIT REAL*8 (A-H,J-Z)

```

```

C      COMMON /LBMASS/ MASS(30,9), DUM1
C      COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
C      COMMON /MOLWT/ WMOL(9)
C      COMMON /ENTHAL/ H(30), DUM3(120)
C      COMMON /VOLUME/ VOL(30), DUM4(61)

```

```

C      NTOT = PC(IC)*VOL(IC)/10.73D0/(TC(IC) + 459.67D0)

```

```

C      NH2O = RATIO*NTOT
C      NAIR = NTOT - NH2O

```

```

C      MASS(IC,3) = NH2O*WMOL(3)
C      MASS(IC,1) = NAIR*WMOL(1)

```

```

C      CALL DENTHL(TC(IC), PC(IC), IC, H(IC))

```

```

C      RETURN

```

```

C      END

```

## B.23 SETRAY

```

C      SUBROUTINE SETRAY (INODES, INOUT)

```

```

C      THIS SUBROUTINE IS USED TO INITIALIZE VALUES IN THE VARIOUS ARRAYS
C      NEEDED FOR TRANSIENT COMPARTMENT ANALYSIS.

```

```

C

```

C THE FOLLOWING VARIABLES ARE USED.

C

C OUTPUT VARIABLES

C

C INODES NUMBER OF NODES AVAILABLE IN THE TRANSIENT  
 C COMPARTMENT MODEL (NOTE: NODE 30 IS THE NULL  
 C VECTOR)  
 C INOUT NUMBER OF INPUT AND NUMBER OF OUTPUT STREAMS  
 C ALLOWED IN THE TRANSIENT COMPARTMENT MODEL

C

C COMMON BLOCK VARIABLES

C

C MASS (30,9) NODE COMPONENT MASS, LB, OR NODE COMPONENT FLOW  
 C RATE, LB/(DELT)  
 C RH FRACTIONAL RELATIVE HUMIDITY, --  
 C TC (30) NODE TEMPERATURE, DEG F  
 C PC (30) NODE PRESSURE, PSIA  
 C TSURF (30) NODE HEAT TRANSFER SURFACE TEMPERATURE, DEG F  
 C WMOL (9) COMPONENT MOLECULAR WEIGHTS, LB/LB MOLE  
 C VOL (30) NODE VOLUME, FT\*\*3  
 C KRCDEF (30) RESISTANCE COEFFICIENT, --, OR RESISTENCE TERM,  
 C PSI-SEC\*\*2/LB-FT\*\*2  
 C DPAREA (30) DEPOSITION AREA, FT\*\*2  
 C DEPVEL DEPOSITION VELOCITY, FT/SEC  
 C H (30) NODE ENTHALPY, BTU, OR NODE ENTHALPY RATE,  
 C BTU/(DELT)  
 C QRATE (30) HEAT TRANSFER RATE, BTU/(DELT)  
 C QCOOL (30) COOLING RATE, BTU/(DELT)  
 C HTCDEF (30) HEAT TRANSFER COEFFICIENT, BTU/SEC-FT\*\*2-DEG F  
 C HTAREA (30) HEAT TRANSFER AREA, FT\*\*2  
 C IIN (30,4) NODE INLET STREAMS  
 C IOUT (30,4) NODE OUTLET STREAMS  
 C AMINLN NATURAL LOG OF THE MINIMUM NUMBER ACCEPTED BY  
 C THE COMPUTER  
 C TIME CUMULATIVE TIME OF THE TRANSIENT SIMULATION, SEC  
 C DELT TIME INCREMENT FOR THE TRANSIENT SIMULATION, SEC  
 C MAXTIM MAXIMUM CUMULATIVE TIME OF THE SIMULATION, SEC  
 C IFLAG CONTROL VARIABLE FOR PRINTING OUTPUT  
 C TRELS TOTAL RELEASE TIME, SEC  
 C C1 WEIGHT FRACTION OF MONOMER TO HF VAPOR  
 C C3 WEIGHT FRACTION OF TRIMER TO HF VAPOR  
 C C6 WEIGHT FRACTION OF HEXAMER TO HF VAPOR  
 C WMBHF EFFECTIVE MOLECULAR WEIGHT OF HF VAPOR,  
 C LB/LB MOLE  
 C ITYPE TYPE OF RELEASE  
 C SOURCE TOTAL MASS OF RELEASED MATERIAL, LB  
 C ISEN CONTROL VARIABLE IDENTIFYING BASIS FOR UF6  
 C LIQUID FLASH OR VAPOR EXPANSION

C

C EQUIVALENCED VARIABLES

C

C ACFM (30) BLOWER FLOW RATE, FT\*\*3/MIN  
 C FLAREA (30) FLOW AREA FOR PRESSURE DROP CONTROLLED FLOW,  
 C FT\*\*2

C

```

C      IMPLICIT REAL*8 (A-H,J-Z)
C
C      DIMENSION ACFM(30), FLAREA(30)
C
C      COMMON /LBMASS/ MASS(30,9), RH
C      COMMON /COMPTP/ TC(30), PC(30), TSURF(30)
C      COMMON /MOLWT/ WMOL(9)
C      COMMON /VOLUME/ VOL(30), KRCOEF(30), DPAREA(30), DEPVEL
C      COMMON /ENTHAL/ H(30), QRATE(30), QCOOL(30), HTCDEF(30),
*      HTAREA(30)
C      COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C      COMMON /CONTRL/ AMINLN, TIME, DELT, MAXTIM, IFLAG, TRELS
C      COMMON /POLYMR/ C1, C3, C6, WMBHF
C      COMMON /MISCEL/ ITYPE, SOURCE, ISEN
C
C      EQUIVALENCE (VOL(1), ACFM(1), FLAREA(1))
C
C      AMINLN = -88.D0
C
C      INODES = 30
C      INOUT  = 4
C
C      MOLECULAR WEIGHTS.
C
C      WMOL(1) = 28.966D0
C      WMOL(2) = 18.016D0
C      WMOL(3) = WMOL(2)
C      WMOL(4) = 20.008D0
C      WMOL(5) = WMOL(4)
C      WMOL(6) = 352.025D0
C      WMOL(7) = WMOL(6)
C      WMOL(8) = WMOL(6)
C      WMOL(9) = 308.025D0
C
C      WMBHF  = WMOL(4)
C
C      DO 30 I30=1,INODES
C
C          DO 10 I10=1,9
C
C              MASS(I30,I10) = 0.D0
C
C      10      CONTINUE
C
C          VOL(I30) = 0.D0
C          H(I30)   =0.D0
C          QRATE(I30) = 0.D0
C          QCOOL(I30) = 0.D0
C          HTCDEF(I30) = 0.D0
C          VOL(I30) = 0.D0
C          KRCOEF(I30) = 0.D0
C          DPAREA(I30) = 0.D0
C

```

```

      DO 20 I20=1,INOUT
C
      IIN(I30,I20) = INODES
      IOUT(I30,I20) = INODES
C
C 20    CONTINUE
C
C 30 CONTINUE
C
      DEPVEL = 0.03300
C
      RETURN
C
      END

```

## B.24 SSBLOW

```

      SUBROUTINE SSBLOW (IC, RATIO)
C
C THIS SUBROUTINE EVALUATES THE STEADY-STATE COMPONENT MASS FLOW RATES
C RESULTING FROM THE FLOW OF MOIST AIR THROUGH A CONSTANT VOLUME BLOWER
C GIVEN THE RATIO OF WATER VAPOR TO AIR AND WATER. FOR STEADY STATE
C CONDITIONS, THE TEMPERATURE AND PRESSURE OF NODE IC SHOULD BE THAT OF
C THE NODE SERVING AS THE INLET TO NODE IC.
C
C THE FOLLOWING VARIABLES ARE USED:
C
C INPUT VARIABLES
C
C IC          STREAM NODE NUMBER
C RATIO       RATIO OF MOLES OF WATER VAPOR TO TOTAL MOLES OF
C             MOIST AIR
C
C COMMON BLOCK VARIABLES
C
C MASS      (30,9) COMPONENT NODE MASS OR MASS FLOW RATE, LB
C             (COMPARTMENT) OR LB/(DELT) (STREAM)
C TC        (30)  NODE TEMPERATURE, DEG F
C PC        (30)  NODE PRESSURE, PSIA
C WMOL      (9)   COMPONENT MOLECULAR WEIGHTS, LB/LB MOLE
C ACFM      (30)  VOLUMETRIC FLOW RATE THROUGH STREAM NODE,
C             FT**3/MIN
C H         (30)  ENTHALPY RATE, BTU/(DELT)
C IIN       (30,4) NODE INPUT STREAM NUMBER
C IOUT      (30,4) NODE OUTPUT STREAM NUMBER
C AM:NLN    MINIMUM NATURAL LOG ACCEPTED BY THE COMPUTER
C TIME      TIME AT WHICH FLOW RATE IS BEING EVALUATED, SEC
C DELT      TIME INTERVAL USED IN TRANSIENT SIMULATION, SEC
C
C INTERNAL VARIABLES
C
C TR        ABSOLUTE TEMPERATURE, DEG R
C NTOT      TOTAL MOLE FLOW RATE, MOLE/(DELT)

```

```

C
C THE FOLLOWING SUBROUTINE IS CALLED BY DENTHL:
C
C           DENTHL
C
C OTHER SUBROUTINES REQUIRED (BECAUSE OF DENTHL) ARE:
C
C           HHFH20
C           HUF6
C           DENUF6
C           VPRUF6
C           ZUF6
C
C           IMPLICIT REAL*8 (A-H,J-Z)
C
C           COMMON /LBMASS/ MASS(30,9), DUM1
C           COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
C           COMMON /MOLWT/ WMOL(9)
C           COMMON /VOLUME/ ACFM(30), DUM3(61)
C           COMMON /ENTHAL/ H(30), DUM4(120)
C           COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C           COMMON /CONTRL/ AMINLN, TIME, DELT, DUM5, IDUM, DUM6
C
C           TC(IC) = TC(IIN(IC,1))
C           PC(IC) = PC(IIN(IC,1))
C
C           TR      = TC(IC) + 459.67D0
C
C           NTOT    = PC(IC)*ACFM(IC)*DELT/10.73D0/TR/6.D1
C
C           MASS(IC,3) = RATIO*NTOT*WMOL(3)
C           MASS(IC,1) = (1.D0 - RATIO)*NTOT*WMOL(1)
C
C           CALL DENTHL (TC(IC), PC(IC), IC, H(IC))
C
C           RETURN
C
C           END

```

## B.25 STERM

```

C           SUBROUTINE STERM (IC, ICMAN, SOLIDS)
C
C THIS SUBROUTINE EVALUATES A STEADY STATE RELEASE RATE BASED ON THE
C INITIAL PRESSURE OF THE MAIN COMPARTMENT AND, FOR UF6 RELEASES,
C WHETHER THE RELEASE IS ISENTROPIC OR ISENTHALPIC.
C
C THE FOLLOWING VARIABLES ARE USED.
C
C INPUT VARIABLES
C
C           IC           NODE NUMBER FOR SOURCE
C           ICMAN        NODE NUMBER OF COMPARTMENT IN WHICH SOURCE IS

```



```

C          LOCATED
C
C  OUTPUT VARIABLE
C
C    SOLIDS          MASS FLOW RATE OF UF6 SOLIDS BEING DEPOSITED ON
C                   FLOOR, LB/(DELT)
C
C  COMMON BLOCK VARIABLES
C
C    MASS    (30,9)  COMPONENT MASS FLOW RATE, LB/(DELT)
C    TC      (30)    NODE TEMPERATURE, DEG F
C    PC      (30)    NODE PRESSURE, PSIA
C    WMOL    (9)     COMPONENT MOLECULAR WEIGHT
C    H       (30)    NODE ENTHALPY RATE, BTU/(DELT)
C    AMINLN  MINIMUM NATURAL LOG ACCEPTED BY THE COMPUTER
C    DELT    INTERVAL OF TIME USED FOR TRANSIENT SIMULATION,
C             SEC
C    TRELS   TOTAL TIME OF RELEASE, SEC
C    ITYPE   RELEASE TYPE IDENTIFIER
C
C             4     HF LIQUID
C             5     HF VAPOR
C             7     UF6 LIQUID, SOLIDS DUMPED TO FLOOR
C            -7     UF6 LIQUID, SOLIDS AIRBORNE
C             8     UF6 VAPOR
C
C    SOURCE   TOTAL MASS OF SOURCE, LB
C    ISEN     BASIS FOR FLASH OF UF6 LIQUID
C
C             0     ISENTROPIC FLASH
C             1     ISENTHALPIC FLASH
C
C  INTERNAL VARIABLES
C
C    WHFL     WEIGHT FRACTION OF HF IN HF-H2O CONDENSATE
C    PHF      VAPOR PRESSURE OF HF, PSIA
C    XVINIT   INITIAL UF6 VAPOR MASS FRACTION
C    XLINIT   INITIAL UF6 LIQUID MASS FRACTION IN THE UF6
C             CONDENSED FRACTION
C    XVFIN    FINAL UF6 VAPOR MASS FRACTION
C    XLFIN    FINAL UF6 LIQUID MASS FRACTION IN THE UF6
C             CONDENSED FRACTION
C    TFIN     FINAL TEMPERATURE OF FLASHED UF6 CORRESPONDING
C             TO THE PRESSURE OF THE MAIN COMPARTMENT, DEG F
C    PUF6     VAPOR PRESSURE OF UF6, PSIA
C
C  THE FOLLOWING SUBROUTINES ARE CALLED BY THIS SUBROUTINE.
C
C          DENTHL
C          FLASH
C          HFPOLY
C          PHFH20
C          VPRUF6
C

```

```

C THE FOLLOWING SUBROUTINES ARE ALSO REQUIRED TO EXECUTE THIS
C SUBROUTINE.
C
C           DENUF6
C           EQTUF6
C           HHFH20
C           HUF6
C           SUF6
C           ZUF6
C
C           IMPLICIT REAL*8 (A-H,J-Z)
C
C           COMMON /LBMASS/ MASS(30,9), DUM1
C           COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
C           COMMON /MOLWT/ WMOL(9)
C           COMMON /ENTHAL/ H(30), DUM3(120)
C           COMMON /CONTRL/ AMINLN, DUM4, DELT, DUM5, IDUM, TRELS
C           COMMON /MISCEL/ ITYPE, SOURCE, ISEN
C
C           SOLIDS = 0.D0
C
C           MASS(IC,IABS(ITYPE)) = SOURCE*DELT/TRELS
C
C           SOURCE TERM FOR HF LIQUID.
C
C           IF (ITYPE.EQ.4) GO TO 40
C
C           SOURCE TERM FOR HF VAPOR. IF THE ENTERED SOURCE PRESSURE IS LESS
C           THAN ZERO OR GREATER THAN THE VAPOR PRESSURE CORRESPONDING TO THE
C           SOURCE TEMPERTURE, THE SOURCE PRESSURE IS SET EQUAL TO THE VAPOR
C           PRESSURE.
C
C           IF (ITYPE.NE.5) GO TO 10
C
C           WHFL = 1.D0
C
C           CALL PHFH20 (TC(IC), WHFL, 0.D0, PHF, 0.D0, 0.D0)
C
C           IF (PHF.LT.PC(IC).OR.PC(IC).LT.0.D0) PC(IC) = PHF
C
C           CALL HFPLY (TC(IC), PC(IC), WMOL(5), .TRUE.)
C
C           GO TO 40
C
C           10 CONTINUE
C
C           SOURCE TERM FOR UF6 LIQUID. UF6 LIQUID IS FLASHED TO THE INITIAL
C           PRESSURE OF THE COMPARTMENT. IF ITYPE = 7, ONLY THE VAPOR FRACTION IS
C           UTILIZED AS A SOURCE TERM FOR THE COMPARTMENT, WHILE THE SOLIDS
C           FRACTION IS ACCUMULATED ON THE FLOOR. IF ITYPE = -7, BOTH SOLID AND
C           VAPOR ARE INCORPORATED INTO THE SOURCE TERM.
C
C           IF (IABS(ITYPE).NE.7) GO TO 20
C

```

```

      CALL VPRUF6 (TC(IC), PC(IC))
C
      XVINIT = 0.D0
      XLINIT = 1.D0
C
      CALL FLASH (TC(IC), PC(IC), WMOL(7), XVINIT, XLINIT, PC(ICMAIN),
*      ISEN, XVFIN, XLFIN, TFIN)
C
      MASS(IC,8) = MASS(IC,7)*XVFIN
C
      SOLIDS = MASS(IC,7) - MASS(IC,8)
C
      IF (ITYPE.EQ.-7) MASS(IC,6) = SOLIDS
      IF (ITYPE.EQ.-7) SOLIDS = 0.D0
C
      MASS(IC,7) = 0.D0
C
      TC(IC) = TFIN
C
      PC(IC) = PC(ICMAIN)
C
      GO TO 40
C
20 CONTINUE
C
C SOURCE TERM FOR UF6 VAPOR. IF THE ENTERED SOURCE PRESSURE IS LESS
C THAN OR EQUAL TO ZERO OR GREATER THAN THE VAPOR PRESSURE
C CORRESPONDING TO THE SOURCE TEMPERATURE, THE SOURCE PRESSURE IS SET
C EQUAL TO THE VAPOR PRESSURE.
C
      IF (ITYPE.NE.8) GO TO 30
C
      CALL VPRUF6 (TC(IC), PUF6)
C
      IF (PUF6.LT.PC(IC).OR.PC(IC).LE.0.D0) PC(IC) = PUF6
C
      GO TO 40
C
30 CONTINUE
C
      WRITE (5,500) ITYPE
C
      STOP15
C
40 CONTINUE
C
      CALL DENTHL (TC(IC), PC(IC), IC, H(IC))
C
      RETURN
C
500 FORMAT (//,5X,'ITYPE =',3I,' NOT RECOGNIZED.',//)
C
      END

```

**B.26 SUF6**

SUBROUTINE SUF6 (TF, PSIA, MW, SSOL, SLIQ, SVAP)

C THIS SUBROUTINE CALCULATES THE ENTROPIES OF UF6 SOLID, LIQUID, AND  
C VAPOR. THE FOLLOWING VARIABLES ARE USED.

C  
C TF TEMPERATURE, DEG F  
C TR ABSOLUTE TEMPERATURE, DEG R  
C LNTR LN(TR)  
C TRSQ TR\*\*2  
C PSIA PRESSURE, PSIA  
C MW MOLECULAR WEIGHT, LB MASS/LB MOLE  
C SSOL ENTROPY OF THE SOLID, BTU/LB MASS-DEG F  
C SLIQ ENTROPY OF THE LIQUID, BTU/LB MASS-DEG F  
C SVAP ENTROPY OF THE VAPOR, BTU/LB MASS-DEG F  
C ZPSIA VAPOR COMPRESSIBILITY FACTOR AT TF AND PSIA  
C Z1ATM VAPOR COMPRESSIBILITY FACTOR AT TF AND 14.696 PSIA

C THE FOLLOWING SUBROUTINE IS CALLED.

C ZUF6

C THE ENTROPY CORRELATIONS ARE BASED ON INFORMATION IN R. DEWITT,  
C "URANIUM HEXAFLUORIDE: A SURVEY OF THE PHYSICO-CHEMICAL PROPERTIES,"  
C GAT-280, GOODYEAR ATOMIC CORP., PORTSMOUTH, OHIO, JAN. 29, 1960,  
C PAGES 67 - 70. THE ENTROPY OF THE VAPOR GIVEN BY THE CORRELATION IN  
C GAT-280 IS FOR A PRESSURE OF 1 ATM. THE VAPOR CORRELATION GIVEN BELOW  
C HAS BEEN MODIFIED USING THE MAGNUSON EQUATION OF STATE (SEE GAT-280,  
C PAGES 97 - 101) AND THE DEPARTURE FUNCTION CORRELATIONS GIVEN IN  
C R. C. REID, J. M. PRAUSNITZ, AND T. K. SHERWOOD, THE PROPERTIES OF  
C GASES AND LIQUIDS, 3RD ED., MCGRAW-HILL BOOK COMPANY, 1977, PAGE 93,  
C SO THAT BOTH SATURATED AND UNSATURATED VAPOR ENTROPIES CAN BE  
C CALCULATED.

C IMPLICIT REAL\*8 (A-H,J-Z)

C TR = TF + 459.67D0  
C LNTR = DLOG(TR)  
C TRSQ = TR\*\*2

C THE ENTROPY OF THE SOLID IS GIVEN BY THE FOLLOWING CORRELATION WHICH  
C IS ACCURATE WITHIN 0.01% BETWEEN 32 DEG F AND THE TRIPLE POINT (147.3  
C DEG F).

C SSOL = ( 3.93535D-1 - 5.70531D-2\*LNTR + 2.55019D-4\*TR  
C \* - ( 4.82282D3/TRSQ ) ) \* ( 3.52D2/MW )

C THE ENTROPY OF THE LIQUID IS GIVEN BY THE FOLLOWING CORRELATION WHICH  
C IS REPORTED TO HAVE AN ACCURACY OF 0.01% [OVER AN ASSUMED RANGE OF  
C 147.3 TO 206.3 DEG F].

C SLIQ = ( -1.72963D-1 + 5.10057D-2\*LNTR + 1.02633D-4\*TR  
C \* - ( 3.06967D3/TRSQ ) ) \* ( 3.52D2/MW )

```

C
C CALCULATE THE VAPOR COMPRESSIBILITY FACTOR AT 14.696 PSIA AND AT
C "PSIA."
C
C     CALL ZUF6 (TF, 14.696D0, Z1ATM, 0.0D0, 0.0D0)
C     CALL ZUF6 (TF, PSIA, ZPSIA, 0.0D0, 0.0D0)
C
C THE ENTROPY OF THE VAPOR IS GIVEN BY THE FOLLOWING CORRELATION.
C
C     SVAP = ( -3.32704D-1 + 9.21307D-2*LNTR + 1.25237D-5*TR
*           + ( 1.47586D3/TRSQ ) + 3.0939D-3 * (ZPSIA - Z1ATM)
*           + 1.0313D-3 * DLOG( (1.0D0 - Z1ATM) / (1.0D0 - ZPSIA) ) )
*           * ( 3.52D2/MW )
C
C     RETURN
C
C     END

```

### B.27 THCUF6

```

C
C SUBROUTINE THCUF6 (TF, PSIA, MW, THCSOL, THCLIQ, THCVAP)
C
C THIS SUBROUTINE CALCULATES THE THERMAL CONDUCTIVITY OF UF6 SOLID,
C LIQUID, AND VAPOR. THE FOLLOWING VARIABLES ARE USED.
C
C     TF      TEMPERATURE, DEG F
C     TR      ABSOLUTE TEMPERATURE, DEG R
C     PSIA    PRESSURE, PSIA
C     MW      MOLECULAR WEIGHT, LB MASS/LB MOLE
C     THCSOL  THERMAL CONDUCTIVITY OF THE SOLID, BTU/HR-FT-DEG F
C     THCLIQ  THERMAL CONDUCTIVITY OF THE LIQUID, BTU/HR-FT-DEG F
C     THCVAP  THERMAL CONDUCTIVITY OF THE VAPOR, BTU/HR-FT-DEG F
C     CPLIQ   HEAT CAPACITY OF THE LIQUID, BTU/LB MASS-DEG F
C     DENLIQ  DENSITY OF THE LIQUID, LB MASS/FT**3
C
C THE FOLLOWING SUBROUTINES ARE CALLED.
C
C     CPUF6
C     DENUF6
C
C     IMPLICIT REAL*8 (A-H,J-Z)
C
C     TR      = TF + 459.67D0
C
C THE THERMAL CONDUCTIVITY OF THE SOLID IS BASED ON DATA OBTAINED FROM
C E. J. BARBER (PERSONAL COMMUNICATION, JULY 13, 1983). ASSUMING A
C LINEAR RELATIONSHIP BETWEEN THERMAL CONDUCTIVITY AND TEMPERATURE,
C THE THERMAL CONDUCTIVITY OF THE SOLID IS GIVEN BY
C
C     THCSOL = 2.586D-1 + 6.084D-4*TF
C
C CALCULATE THE HEAT CAPACITY AND THE DENSITY OF THE LIQUID.
C

```

```

C      CALL CPUF6 (TF, PSIA, MW, 0.000, CPLIQ, 0.000, 0.000, 0.000)
C
C      CALL DENUF6 (TF, PSIA, MW, 0.000, DENLIQ, 0.000)
C
C THE THERMAL CONDUCTIVITY OF THE LIQUID IS BASED ON A SINGLE VALUE
C REPORTED IN R. DEWITT, "URANIUM HEXAFLUORIDE: A SURVEY OF THE
C PHYSICO-CHEMICAL PROPERTIES," GAT-280, GOODYEAR ATOMIC CORP.,
C PORTSMOUTH, OHIO, JAN. 29, 1960, PAGE 46. ASSUMING A GENERAL FORM OF
C VARIOUS PREDICTIVE CORRELATIONS FOR THERMAL CONDUCTIVITY OF A LIQUID,
C WHICH IS  $K = B * CP * (DEN^{**1.33}) / TR$ , THE COEFFICIENT B WAS
C DETERMINED. THUS, AN APPROXIMATE CORRELATION FOR LIQUID THERMAL
C CONDUCTIVITY IS GIVEN BY
C
C      THCLIQ = 3.247D-1 * CPLIQ * ( DENLIQ**(4.00/3.00) ) / TR
C
C THE THERMAL CONDUCTIVITY OF THE VAPOR IS BASED ON GAT-280, PAGES 44 -
C 46, AND IS GIVEN BY
C
C      THCVAP = 3.268D-3 * ( 1.000 + 2.52D-3*TF )
C
C      RETURN
C
C      END

```

## B.28 TRBLOW

```

C      SUBROUTINE TRBLOW (IC)
C
C THIS SUBROUTINE EVALUATES THE TRANSIENT MASS FLOW RATES FOR A
C CONSTANT VOLUME BLOWER REPRESENTED BY NODE IC WHICH DRAWS FROM A
C COMPARTMENT REPRESENTED BY NODE IIN(IC,1).
C
C THE FOLLOWING VARIABLES ARE USED:
C
C      INPUT VARIABLE
C
C      IC          STREAM NODE NUMBER
C
C      COMMON BLOCK VARIABLES
C
C      MASS      (30,9)  COMPONENT NODE MASS OR MASS FLOW RATE, LB
C                      (COMPARTMENT) OR LB/(DELT) (STREAM)
C      TC        (30)    NODE TEMPERATURE, DEG F
C      PC        (30)    NODE PRESSURE, PSIA
C      WMOL      (9)     COMPONENT MOLECULAR WEIGHTS, LB/LB MOLE
C      ACFM      (30)    VOLUMETRIC FLOW RATE THROUGH BLOWER, FT**3/MIN
C      H         (30)    ENTHALPY OR ENTHALPY RATE, BTU OR BTU/(DELT)
C      AMINLN    MINIMUM NATURAL LOG ACCEPTED BY THE COMPUTER
C      DELT      TIME INTERVAL USED IN TRANSIENT SIMULATION, SEC
C      IIN       (30,4)  NODE INPUT STREAM NUMBER
C      IOUT      (30,4)  NODE OUTPUT STREAM NUMBER
C
C      EQUIVALENCED VARIABLE

```

```

C
C      VOL      (30)    COMPARTMENT NODE VOLUME, FT**3
C
C      INTERNAL VARIABLE
C
C      FRAC      RATIO OF BLOWER VOLUME FLOW RATE-TIME INTERVAL
C                  PRODUCT TO INLET NODE VOLUME
C
C      IMPLICIT REAL*8 (A-H,J-Z)
C
C      DIMENSION VOL(30)
C
C      COMMON /LBMASS/ MASS(30,9), DUM1
C      COMMON /COMPTP/ TC(30), PC(30), DUM2(30)
C      COMMON /MOLWT/ WMOL(9)
C      COMMON /VOLUME/ ACFM(30), DUM3(61)
C      COMMON /ENTHAL/ H(30), DUM4(120)
C      COMMON /CONTRL/ AMINLN, DUM5, DELT, DUM6, IDUM1, DUM7
C      COMMON /ISTRMS/ IIN(30,4), IOUT(30,4)
C
C      EQUIVALENCE (VOL(1),ACFM(1))
C
C      FRAC      = ACFM(IC)*DELT/6.01/VOL(IIN(IC,1))
C
C      DO 10 I10=1,9
C
C          MASS(IC,I10) = FRAC*MASS(IIN(IC,1),I10)
C
C 10 CONTINUE
C
C      H(IC)    = FRAC*H(IIN(IC,1))
C      TC(IC)   = TC(IIN(IC,1))
C      PC(IC)   = PC(IIN(IC,1))
C
C      RETURN
C
C      END

```

## B.29 VISUF6

```

      SUBROUTINE VISUF6 (TF, PSIA, MW, VISLIQ, VISVAP)
C
C      THIS SUBROUTINE CALCULATES THE VISCOSITIES OF UF6 LIQUID AND VAPOR.
C      THE FOLLOWING VARIABLES ARE USED.
C
C      TF      TEMPERATURE, DEG F
C      TR      ABSOLUTE TEMPERATURE, DEG R
C      PSIA    PRESSURE, PSIA
C      MW      MOLECULAR WEIGHT, LB/LB MOLE
C      VISLIQ  LIQUID VISCOSITY, LB MASS/FT-HR
C      VISVAP  VAPOR VISCOSITY, LB MASS/FT-HR
C
C      THE FOLLOWING SUBROUTINE IS CALLED.

```

```

C
C   VPRUF6
C
C   THE VISCOSITY CORRELATIONS ARE BASED ON INFORMATION FROM R. DEWITT,
C   "URANIUM HEXAFLUORID: A SURVEY OF THE PHYSICO-CHEMICAL PROPERTIES,"
C   GAT-280, GOODYEAR ATOMIC CORP., PORTSMOUTH, OHIO, JAN. 29, 1960,
C   PAGES 38 - 44. THE VAPOR VISCOSITY CORRELATION WAS FITTED TO DATA
C   REPORTED IN GAT-280 BY W. R. WILLIAMS.
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   TR      = TF + 459.67D0
C
C   THE VISCOSITY OF THE LIQUID IS GIVEN BY THE FOLLOWING CORRELATION
C   WHICH IS BASED ON DATA RANGING FROM 158 TO 410 DEG F. THE SUM OF THE
C   TERMS IN THE EXPONENTIAL IS CORRECT BASED ON THE DATA OF BLATT
C   REPORTED BY DEWITT IN TABLE 25.
C
C   VISLIQ = 0.404D0 * DEXP( (9.97D2 + 4.1D-2*PSIA)/TR )
C
C   THE VISCOSITY OF THE VAPOR BASED ON DATA RANGING FROM 104 TO 392
C   DEG F IS GIVEN WITHIN 0.6% BY THE FOLLOWING CORRELATION.
C
C   VISVAP =          1.192D-4 * TR**0.9305D0
C
C   RETURN
C
C   END

```

### B.30 VPRUF6

```

C
C   SUBROUTINE VPRUF6 (TF, PSIA)
C
C   THIS SUBROUTINE CALCULATES THE VAPOR PRESSURE OF UF6. THE FOLLOWING
C   VARIABLES ARE USED.
C
C       TF      TEMPERATURE, DEG F
C       PSIA    PRESSURE, PSIA
C       P1      PRESSURE, PSIA
C       P2      PRESSURE, PSIA
C
C   THE VAPOR PRESSURE CORRELATIONS USED ARE BASED ON R. DEWITT, "URANIUM
C   HEXAFLUORIDE: A SURVEY OF THE PHYSICO-CHEMICAL PROPERTIES," GAT-280,
C   GOODYEAR ATOMIC CORP., PORTSMOUTH, OHIO, JAN. 29, 1960, PAGE 81.
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   IF (TF.GE.147.306561D0) GO TO 10
C
C   THE VAPOR PRESSURE OF UF6 OVER THE SOLID FROM 32 DEG F TO THE TRIPLE
C   POINT AT 147.3 DEG F IS GIVEN BY
C
C   PSIA      = DEXP ( 10.4443D0 + 9.64233D-3*TF - ( 3.90741D3 /

```



```

      *      ( TF + 298.149D0 ) ) )
C
      RETURN
C
10 CONTINUE
C
C DEWITT RECOMMENDS 2 CORRELATIONS FOR THE VAPOR PRESSURE OF UF6 OVER
C THE LIQUID. THE FIRST, WHICH IS GIVEN BELOW BY P1, GIVES GOOD AGREE-
C MENT (0.03%) FROM THE TRIPLE POINT TO 240.8 DEG F. THE SECOND, WHICH
C IS GIVEN BELOW BY P2, AGREES WITHIN 0.3% ON AVERAGE BETWEEN THE
C 240.8 DEG F AND THE CRITICAL POINT. P2 EXCEEDS THE TABULATED VALUES
C OF VAPOR PRESSURE FROM 240.8 DEG F TO ABOUT 276 DEG F. BY USING A
C WEIGHTED AVERAGE OF P1 AND P2 OVER THIS RANGE, A BETTER AGREEMENT
C WITH TABULATED VALUES IS OBTAINED, AS WELL AS A CONTINUOUS FUNCTION
C FOR VAPOR PRESSURE.
C
      P1      = DEXP ( 12.1600D0 - ( 4.66807D3 / ( TF + 367.533D0 ) ) )
      P2      = DEXP ( 13.7627D0 - ( 6.97611D3 / ( TF + 511.866D0 ) ) )
C
      IF (TF. GE. 2.40D2) GO TO 20
C
C THE VAPOR PRESSURE OF UF6 OVER THE LIQUID FROM THE TRIPLE POINT TO
C 240 DEG F IS GIVEN BY
C
      PSIA    = P1
C
      RETURN
C
20 CONTINUE
C
      IF (TF.GE.2.76D2) GO TO 30
C
C THE VAPOR PRESSURE OF UF6 OVER THE LIQUID FROM 240 TO 276 DEG F IS
C GIVEN BY
C
      PSIA    = ( (2.76D2 - TF)*P1 + (TF - 2.40D2)*P2 ) / 3.6D1
C
      RETURN
C
30 CONTINUE
C
C THE VAPOR PRESSURE OF UF6 OVER THE LIQUID FROM 276 DEG F TO THE
C CRITICAL POINT IS GIVEN BY
C
      PSIA    = P2
C
      RETURN
C
      END

```

**B.31 ZUF6**

```

SUBROUTINE ZUF6 (TF, PSIA, Z, ZP, ZT)
C
C THIS SUBROUTINE CALCULATES THE COMPRESSIBILITY FACTOR OF UF6 AS WELL
C AS THE QUANTITIES ZP AND ZT. THE FOLLOWING VARIABLES ARE USED.
C
C   TF      TEMPERATURE, DEG F
C   TR      ABSOLUTE TEMPERATURE, DEG R
C   TCUBE   (DEG R)**3
C   PSIA    PRESSURE, PSIA
C   Z       COMPRESSIBILITY FACTOR
C
C   ZP = Z - P (DZ/DP), EVALUATED FOR CONSTANT T
C   ZT = Z + T (DZ/DT), EVALUATED FOR CONSTANT P
C
C THE COMPRESSIBILITY FACTOR IS BASED ON THE EQUATION OF STATE FOR UF6
C PROPOSED BY D. W. MAGNUSON CITED BY R. DEWITT, "URANIUM HEXAFLUORIDE:
C A SURVEY OF THE PHYSICO-CHEMICAL PROPERTIES," GAT-280, GOODYEAR
C ATOMIC CORP., PORTSMOUTH, OHIO, JAN. 29, 1960, PAGES 24 AND 97 - 101.
C
C   IMPLICIT REAL*8 (A-H,J-Z)
C
C   TR      = TF + 459.67D0
C   TCUBE   = TR**3
C
C   Z       = TCUBE / ( TCUBE + 4.8923D5*PSIA )
C
C   ZP      = ( 2.0D0 - Z ) * Z
C   ZT      = ( 4.0D0 - 3.0D0*Z ) * Z
C
C   RETURN
C
C   END

```

## **Appendix C**

### **EXAMPLE PROBLEM OUTPUT**

Output for Examples 1 (Cases 1 through 4), 2 (Cases 1 and 3), 3 (Cases 1 through 3), 4 (Cases 1 through 4), and 5 are included in this appendix. Output for Examples 1, 2, and 3 were produced by CYLIND. Output for Example 4, Cases 1 and 3, as well as Example 5, were produced by FODRFT and for Example 4, Cases 2 and 4, by INDRFT. Example problems are described in Chapter 5. Output for Examples 2 (Case 2) and 6 from CYLIND and BATCH, respectively, are included in Chapter 5 as are selected plots produced by COMPLT and CYLPLT.

TITLE: EX. 1, CASE 1. 10-TON CYL, SHEARED VALVE AT 6 O'CLOCK, UF6 AT 200 F

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****				***** CONDITION OF UF6 EXHAUSTED *****									
	SOLID	LIQUID	MASS (LB)	TEMP (DEG F)	PRES (PSIA)	RELEASE PHASE	PATHWAY	INLET	FLOW RATE BASIS	SOLID	LIQUID	RELEASE RATE (LB/SEC)	TEMP (DEG F)	PRES (PSIA)
0.	0.0	21003.4	26.6	21030.0	200.000	51.152	LIQUID	LIQUID	CHOKE	2.944	0.000	3.390	6.334	14.700
60.	0.0	20619.2	30.7	20650.0	199.949	51.114	LIQUID	LIQUID	CHOKE	2.943	0.000	3.387	6.330	14.700
120.	0.0	20235.3	34.9	20270.2	199.896	51.075	LIQUID	LIQUID	CHOKE	2.942	0.000	3.384	6.326	14.700
180.	0.0	19851.6	39.0	19890.6	199.843	51.036	LIQUID	LIQUID	CHOKE	2.941	0.000	3.381	6.322	14.700
240.	0.0	19468.1	43.2	19511.3	199.789	50.996	LIQUID	LIQUID	CHOKE	2.940	0.000	3.379	6.318	14.700
300.	0.0	19084.8	47.3	19132.2	199.734	50.955	LIQUID	LIQUID	CHOKE	2.939	0.000	3.376	6.314	14.700
360.	0.0	18701.9	51.4	18753.3	199.678	50.914	LIQUID	LIQUID	CHOKE	2.938	0.000	3.373	6.310	14.700
420.	0.0	18319.1	55.6	18374.7	199.621	50.871	LIQUID	LIQUID	CHOKE	2.937	0.000	3.370	6.306	14.700
480.	0.0	17936.6	59.7	17996.3	199.562	50.828	LIQUID	LIQUID	CHOKE	2.935	0.000	3.367	6.302	14.700
540.	0.0	17554.4	63.8	17618.2	199.503	50.785	LIQUID	LIQUID	CHOKE	2.934	0.000	3.363	6.298	14.700
600.	0.0	17172.5	67.8	17240.3	199.442	50.740	LIQUID	LIQUID	CHOKE	2.933	0.000	3.360	6.293	14.700
660.	0.0	16790.8	71.9	16862.7	199.381	50.695	LIQUID	LIQUID	CHOKE	2.932	0.000	3.357	6.289	14.700
720.	0.0	16409.4	76.0	16485.4	199.318	50.648	LIQUID	LIQUID	CHOKE	2.931	0.000	3.354	6.284	14.700
780.	0.0	16028.3	80.0	16108.3	199.254	50.601	LIQUID	LIQUID	CHOKE	2.929	0.000	3.350	6.280	14.700
840.	0.0	15647.5	84.1	15731.6	199.188	50.553	LIQUID	LIQUID	CHOKE	2.928	0.000	3.347	6.275	14.700
900.	0.0	15267.0	88.1	15355.1	199.121	50.503	LIQUID	LIQUID	CHOKE	2.927	0.000	3.343	6.270	14.700
960.	0.0	14886.7	92.1	14978.9	199.052	50.453	LIQUID	LIQUID	CHOKE	2.925	0.000	3.340	6.265	14.700
1020.	0.0	14506.8	96.1	14603.0	198.982	50.402	LIQUID	LIQUID	CHOKE	2.924	0.000	3.336	6.260	14.700
1080.	0.0	14127.2	100.1	14227.4	198.910	50.349	LIQUID	LIQUID	CHOKE	2.922	0.000	3.332	6.255	14.700
1140.	0.0	13748.0	104.1	13852.1	198.837	50.295	LIQUID	LIQUID	CHOKE	2.921	0.000	3.328	6.249	14.700
1200.	0.0	13369.0	108.1	13477.1	198.761	50.240	LIQUID	LIQUID	CHOKE	2.920	0.000	3.325	6.244	14.700
1260.	0.0	12990.5	112.0	13102.5	198.684	50.184	LIQUID	LIQUID	CHOKE	2.918	0.000	3.320	6.238	14.700
1320.	0.0	12612.2	116.0	12728.2	198.605	50.126	LIQUID	LIQUID	CHOKE	2.916	0.000	3.316	6.233	14.700
1380.	0.0	12234.3	119.9	12354.2	198.524	50.066	LIQUID	LIQUID	CHOKE	2.915	0.000	3.312	6.227	14.700
1440.	0.0	11856.8	123.8	11980.6	198.440	50.006	LIQUID	LIQUID	CHOKE	2.913	0.000	3.308	6.221	14.700
1500.	0.0	11479.7	127.7	11607.3	198.354	49.943	LIQUID	LIQUID	CHOKE	2.911	0.000	3.303	6.215	14.700
1560.	0.0	11102.9	131.6	11234.5	198.266	49.879	LIQUID	LIQUID	CHOKE	2.910	0.000	3.299	6.208	14.700
1620.	0.0	10726.5	135.4	10862.0	198.175	49.812	LIQUID	LIQUID	CHOKE	2.908	0.000	3.294	6.202	14.700
1680.	0.0	10350.6	139.3	10489.9	198.081	49.744	LIQUID	LIQUID	CHOKE	2.906	0.000	3.289	6.195	14.700
1740.	0.0	9975.1	143.1	10118.2	197.984	49.674	LIQUID	LIQUID	CHOKE	2.904	0.000	3.284	6.188	14.700
1800.	0.0	9600.0	146.9	9746.9	197.884	49.601	LIQUID	LIQUID	CHOKE	2.902	0.000	3.279	6.181	14.700
1860.	0.0	9225.4	150.7	9376.0	197.780	49.526	LIQUID	LIQUID	CHOKE	2.900	0.000	3.274	6.173	14.700
1920.	0.0	8851.2	154.4	9005.6	197.673	49.449	LIQUID	LIQUID	CHOKE	2.898	0.000	3.268	6.166	14.700
1980.	0.0	8477.5	158.1	8635.7	197.562	49.369	LIQUID	LIQUID	CHOKE	2.896	0.000	3.262	6.158	14.700
2040.	0.0	8104.4	161.8	8266.2	197.447	49.286	LIQUID	LIQUID	CHOKE	2.893	0.000	3.256	6.150	14.700
2100.	0.0	7731.7	165.5	7897.2	197.327	49.199	LIQUID	LIQUID	CHOKE	2.891	0.000	3.250	6.141	14.700
2160.	0.0	7359.6	169.2	7528.8	197.202	49.109	LIQUID	LIQUID	CHOKE	2.888	0.000	3.244	6.132	14.700
2220.	0.0	6988.1	172.8	7160.9	197.071	49.015	LIQUID	LIQUID	CHOKE	2.886	0.000	3.237	6.123	14.700
2280.	0.0	6617.1	176.4	6793.5	196.935	48.918	LIQUID	LIQUID	CHOKE	2.883	0.000	3.230	6.113	14.700
2340.	0.0	6246.8	179.9	6426.7	196.792	48.815	LIQUID	LIQUID	CHOKE	2.880	0.000	3.223	6.103	14.700
2400.	0.0	5877.1	183.5	6060.6	196.642	48.708	LIQUID	LIQUID	CHOKE	2.877	0.000	3.215	6.092	14.700
2460.	0.0	5508.1	186.9	5695.0	196.484	48.595	LIQUID	LIQUID	CHOKE	2.874	0.000	3.207	6.081	14.700
2520.	0.0	5139.8	190.4	5330.2	196.317	48.476	LIQUID	LIQUID	CHOKE	2.871	0.000	3.198	6.069	14.700

## Ex. 1, Case 1 (continued)

2580.	0.0	4772.3	193.8	4966.1	196.140	48.350	LIQUID	49.015	CHOKE	2.867	0.000	3.189	6.056	14.700	133.780
2640.	0.0	4405.6	197.1	4602.7	195.951	48.217	LIQUID	48.756	CHOKE	2.863	0.000	3.180	6.043	14.700	133.780
2700.	0.0	4039.7	200.4	4240.1	195.750	48.074	LIQUID	48.567	CHOKE	2.856	0.000	3.167	6.023	14.700	133.780
2760.	0.0	3675.1	203.6	3878.7	195.555	47.922	LIQUID	48.327	CHOKE	2.844	0.000	3.147	5.991	14.700	133.780
2820.	0.0	3312.6	206.7	3519.3	195.303	47.759	LIQUID	48.073	CHOKE	2.831	0.000	3.126	5.957	14.700	133.780
2880.	0.0	2952.1	209.7	3161.9	195.051	47.582	LIQUID	47.805	CHOKE	2.817	0.000	3.104	5.921	14.700	133.780
2940.	0.0	2594.0	212.7	2806.6	194.777	47.390	LIQUID	47.518	CHOKE	2.803	0.000	3.080	5.883	14.700	133.780
3000.	0.0	2238.2	215.5	2453.6	194.476	47.179	LIQ-VAP	47.179	CHOKE	2.761	0.000	3.040	5.801	14.700	133.780
3060.	0.0	1887.7	217.9	2105.6	194.078	46.903	VAPOR	46.903	CHOKE	0.000	0.000	2.365	2.366	14.700	192.978
3120.	0.0	1781.4	182.2	1963.6	179.706	37.704	VAPOR	37.704	PDC	0.000	0.000	1.902	1.902	14.700	178.873
3180.	0.0	1695.4	154.0	1849.5	167.107	30.838	VAPOR	30.838	PDC	0.000	0.000	1.485	1.485	14.700	166.491
3240.	0.0	1627.7	132.7	1760.4	156.501	25.843	VAPOR	25.843	PDC	0.000	0.000	1.163	1.163	14.700	156.057
3300.	0.0	1574.1	116.5	1690.6	147.655	22.178	VAPOR	22.178	PDC	0.000	0.000	0.906	0.906	14.700	147.345
3360.	79.8	1440.1	116.3	1636.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3420.	162.9	1303.0	116.6	1582.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3480.	245.9	1165.8	117.0	1528.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3540.	328.9	1028.7	117.4	1474.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3600.	411.9	891.5	117.8	1421.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3660.	494.9	754.3	118.1	1367.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3720.	577.9	617.2	118.5	1313.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3780.	660.9	480.0	118.9	1259.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3840.	743.9	342.9	119.3	1206.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3900.	826.9	205.7	119.6	1152.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3960.	909.9	68.5	120.0	1098.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003

TITLE: EX. 1, CASE 2. 10-TON CYL, SHEARED VALVE AT 9 O'CLOCK, UF6 AT 200 F

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****			***** CONDITION OF UF6 EXHAUSTED *****			***** CONDITION OF UF6 EXHAUSTED *****			FLOM RATE BASIS	PRES (PSIA)	RELEASE PHASE	PRES (PSIA)	RELEASE RATE (LB/SEC)	TEMP (DEG F)	PRES		
	SOLID	LIQUID	MASS (LB)	VAPOR	TOTAL	TEMP (DEG F)	PRES (PSIA)	RELEASE PHASE	PRES (PSIA)								SOLID	LIQUID
0.	0.0	21003.4	26.6	21030.0	0	200.000	51.152	LIQUID	53.179	CHOKE	53.179	LIQUID	2.944	0.000	3.390	6.334	14.700	133.780
60.	0.0	20619.2	30.7	20649.9	199.949	51.114	51.075	LIQUID	53.039	CHOKE	53.039	LIQUID	2.943	0.000	3.387	6.331	14.700	133.780
120.	0.0	20235.2	34.9	20270.1	199.896	51.075	51.036	LIQUID	52.901	CHOKE	52.901	LIQUID	2.942	0.000	3.384	6.327	14.700	133.780
180.	0.0	19851.5	39.0	19890.5	199.843	51.036	50.996	LIQUID	52.766	CHOKE	52.766	LIQUID	2.941	0.000	3.382	6.323	14.700	133.780
240.	0.0	19468.0	43.2	19511.1	199.789	50.996	50.955	LIQUID	52.632	CHOKE	52.632	LIQUID	2.940	0.000	3.379	6.319	14.700	133.780
300.	0.0	19084.7	47.3	19132.0	199.734	50.955	50.914	LIQUID	52.501	CHOKE	52.501	LIQUID	2.939	0.000	3.376	6.315	14.700	133.780
360.	0.0	18701.7	51.4	18753.1	199.678	50.914	50.871	LIQUID	52.371	CHOKE	52.371	LIQUID	2.938	0.000	3.373	6.311	14.700	133.780
420.	0.0	18318.9	55.6	18374.5	199.620	50.871	50.828	LIQUID	52.241	CHOKE	52.241	LIQUID	2.937	0.000	3.370	6.307	14.700	133.780
480.	0.0	17936.4	59.7	17996.1	199.562	50.828	50.785	LIQUID	52.112	CHOKE	52.112	LIQUID	2.936	0.000	3.367	6.302	14.700	133.780
540.	0.0	17554.1	63.8	17617.9	199.503	50.785	50.740	LIQUID	51.984	CHOKE	51.984	LIQUID	2.934	0.000	3.364	6.298	14.700	133.780
600.	0.0	17172.2	67.8	17240.0	199.442	50.740	50.695	LIQUID	51.857	CHOKE	51.857	LIQUID	2.933	0.000	3.361	6.294	14.700	133.780
660.	0.0	16790.5	71.9	16862.4	199.381	50.695	50.648	LIQUID	51.729	CHOKE	51.729	LIQUID	2.932	0.000	3.357	6.289	14.700	133.780
720.	0.0	16409.0	76.0	16485.0	199.318	50.648	50.601	LIQUID	51.602	CHOKE	51.602	LIQUID	2.931	0.000	3.354	6.285	14.700	133.780
780.	0.0	16027.9	80.0	16107.9	199.253	50.601	50.553	LIQUID	51.474	CHOKE	51.474	LIQUID	2.930	0.000	3.351	6.280	14.700	133.780
840.	0.0	15647.0	84.1	15731.1	199.188	50.553	50.503	LIQUID	51.346	CHOKE	51.346	LIQUID	2.928	0.000	3.347	6.275	14.700	133.780
900.	0.0	15266.5	88.1	15354.6	199.121	50.503	50.453	LIQUID	51.218	CHOKE	51.218	LIQUID	2.927	0.000	3.344	6.271	14.700	133.780
960.	0.0	14886.2	92.1	14978.4	199.052	50.453	50.402	LIQUID	51.089	CHOKE	51.089	LIQUID	2.926	0.000	3.340	6.266	14.700	133.780
1020.	0.0	14506.3	96.1	14602.4	198.982	50.402	50.349	LIQUID	50.960	CHOKE	50.960	LIQUID	2.924	0.000	3.336	6.259	14.700	133.780
1080.	0.0	14126.7	100.1	14226.9	198.910	50.349	50.295	LIQUID	50.830	CHOKE	50.830	LIQUID	2.915	0.000	3.324	6.239	14.700	133.780
1140.	0.0	13748.4	104.1	13852.6	198.837	50.295	50.240	LIQUID	50.699	CHOKE	50.699	LIQUID	2.915	0.000	3.312	6.218	14.700	133.780
1200.	0.0	13371.4	108.1	13479.5	198.762	50.240	50.184	LIQUID	50.568	CHOKE	50.568	LIQUID	2.898	0.000	3.300	6.198	14.700	133.780
1260.	0.0	12995.6	112.0	13107.6	198.685	50.184	50.127	LIQUID	50.436	CHOKE	50.436	LIQUID	2.889	0.000	3.288	6.177	14.700	133.780
1320.	0.0	12621.1	115.9	12736.9	198.607	50.127	50.069	LIQUID	50.304	CHOKE	50.304	LIQUID	2.881	0.000	3.276	6.157	14.700	133.780
1380.	0.0	12247.8	119.8	12367.5	198.527	50.069	50.009	LIQUID	50.170	CHOKE	50.170	LIQUID	2.872	0.000	3.264	6.136	14.700	133.780
1440.	0.0	11875.7	123.6	11999.3	198.444	50.009	49.933	LIQ-VAP	50.009	CHOKE	50.009	LIQ-VAP	2.828	0.000	3.232	6.060	14.700	133.780
1500.	0.0	11508.4	127.4	11635.7	198.340	49.933	49.933	LIQ-VAP	49.933	CHOKE	49.933	LIQ-VAP	1.238	0.000	2.648	3.887	14.700	133.780
1560.	0.0	11174.7	127.8	11402.5	196.942	48.923	48.923	VAPOR	48.923	CHOKE	48.923	VAPOR	0.000	0.000	2.462	2.462	14.700	195.786
1620.	0.0	11130.3	124.5	11254.8	193.642	46.601	46.601	VAPOR	46.601	CHOKE	46.601	VAPOR	0.000	0.000	2.352	2.352	14.700	192.550
1680.	0.0	10992.5	121.2	11113.7	190.435	44.425	44.425	VAPOR	44.425	CHOKE	44.425	VAPOR	0.000	0.000	2.249	2.249	14.700	189.404
1740.	0.0	10860.7	118.0	10978.8	187.317	42.385	42.385	VAPOR	42.385	CHOKE	42.385	VAPOR	0.000	0.000	2.152	2.152	14.700	186.345
1800.	0.0	10734.8	114.9	10849.7	184.286	40.471	40.471	VAPOR	40.471	CHOKE	40.471	VAPOR	0.000	0.000	2.060	2.060	14.700	183.369
1860.	0.0	10614.3	111.8	10726.1	181.337	38.673	38.673	VAPOR	38.673	PDC	38.673	VAPOR	0.000	0.000	1.959	1.959	14.700	180.475
1920.	0.0	10499.7	108.8	10608.5	178.490	36.995	36.995	VAPOR	36.995	PDC	36.995	VAPOR	0.000	0.000	1.860	1.860	14.700	177.679
1980.	0.0	10391.0	105.9	10496.9	175.748	35.433	35.433	VAPOR	35.433	PDC	35.433	VAPOR	0.000	0.000	1.766	1.766	14.700	174.985
2040.	0.0	10287.8	103.2	10391.0	173.106	33.976	33.976	VAPOR	33.976	PDC	33.976	VAPOR	0.000	0.000	1.678	1.678	14.700	172.389
2100.	0.0	10189.7	100.5	10290.2	170.562	32.617	32.617	VAPOR	32.617	PDC	32.617	VAPOR	0.000	0.000	1.595	1.595	14.700	169.889
2160.	0.0	10096.6	97.9	10194.5	168.113	31.348	31.348	VAPOR	31.348	PDC	31.348	VAPOR	0.000	0.000	1.517	1.517	14.700	167.480
2220.	0.0	10008.0	95.5	10103.5	165.754	30.163	30.163	VAPOR	30.163	PDC	30.163	VAPOR	0.000	0.000	1.443	1.443	14.700	165.161
2280.	0.0	9923.8	93.1	10016.9	163.484	29.055	29.055	VAPOR	29.055	PDC	29.055	VAPOR	0.000	0.000	1.373	1.373	14.700	162.928
2340.	0.0	9843.7	90.9	9934.6	161.300	28.019	28.019	VAPOR	28.019	PDC	28.019	VAPOR	0.000	0.000	1.306	1.306	14.700	160.779
2400.	0.0	9767.5	88.7	9856.2	159.198	27.049	27.049	VAPOR	27.049	PDC	27.049	VAPOR	0.000	0.000	1.243	1.243	14.700	158.711
2460.	0.0	9695.0	86.7	9781.7	157.177	26.141	26.141	VAPOR	26.141	PDC	26.141	VAPOR	0.000	0.000	1.183	1.183	14.700	156.722
2520.	0.0	9626.0	84.7	9710.7	155.233	25.291	25.291	VAPOR	25.291	PDC	25.291	VAPOR	0.000	0.000	1.126	1.126	14.700	154.809

Ex. 1, Case 2 (continued)

2580.	0.0	9560.3	82.8	9643.2	153.366	24.494	VAPOR	24.494	PDC	0.000	0.000	0.000	1.071	14.700	152.970
2640.	0.0	9497.8	81.1	9578.9	151.572	23.747	VAPOR	23.747	PDC	0.000	0.000	0.000	1.019	14.700	151.204
2700.	0.0	9438.4	79.4	9517.8	149.850	23.047	VAPOR	23.047	PDC	0.000	0.000	0.000	0.969	14.700	149.508
2760.	0.0	9381.9	77.7	9459.6	148.197	22.390	VAPOR	22.390	PDC	0.000	0.000	0.000	0.922	14.700	147.880
2820.	37.3	9289.9	77.0	9404.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
2880.	120.3	9152.7	77.4	9350.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
2940.	203.4	9015.6	77.8	9296.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3000.	286.4	8878.4	78.2	9243.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3060.	369.4	8741.3	78.6	9189.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3120.	452.4	8604.1	79.3	9135.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3180.	535.4	8466.9	79.3	9081.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3240.	618.4	8329.8	79.7	9027.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3300.	701.4	8192.6	80.1	8974.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3360.	784.4	8055.5	80.4	8920.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3420.	867.4	7918.3	80.8	8866.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3480.	950.4	7781.1	81.2	8812.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3540.	1033.4	7644.0	81.6	8759.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3600.	1116.4	7506.8	81.9	8705.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3660.	1199.4	7369.7	82.3	8651.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3720.	1282.4	7232.5	82.7	8597.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3780.	1365.4	7095.4	83.1	8543.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3840.	1448.4	6958.2	83.5	8490.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3900.	1531.4	6821.0	83.8	8436.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
3960.	1614.4	6683.9	84.2	8382.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4020.	1697.4	6546.7	84.6	8328.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4080.	1780.4	6409.6	85.0	8275.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4140.	1863.4	6272.4	85.3	8221.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4200.	1946.4	6135.2	85.7	8167.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4260.	2029.4	5998.1	86.1	8113.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4320.	2112.4	5860.9	86.5	8059.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4380.	2195.4	5723.8	86.8	8006.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4440.	2278.5	5586.6	87.2	7952.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4500.	2361.5	5449.5	87.6	7898.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4560.	2444.5	5312.3	88.0	7844.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4620.	2527.5	5175.1	88.4	7791.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4680.	2610.5	5038.0	88.7	7737.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4740.	2693.5	4900.8	89.1	7683.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4800.	2776.5	4763.7	89.5	7629.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4860.	2859.5	4626.5	89.9	7575.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4920.	2942.5	4489.3	90.2	7522.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
4980.	3025.5	4352.2	90.6	7468.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5040.	3108.5	4215.0	91.0	7414.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5100.	3191.5	4077.9	91.4	7360.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5160.	3274.5	3940.7	91.8	7307.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5220.	3357.5	3803.5	92.1	7253.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5280.	3440.5	3666.4	92.5	7199.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5340.	3523.5	3529.2	92.9	7145.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5400.	3606.5	3392.1	93.3	7091.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003

## Ex. 1, Case 2 (continued)

5460.	3689.5	3254.9	93.6	7038.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5520.	3772.5	3117.8	94.0	6984.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5580.	3855.5	2980.6	94.4	6930.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5640.	3938.5	2843.4	94.8	6876.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5700.	4021.5	2706.3	95.1	6823.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5760.	4104.5	2569.1	95.5	6769.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5820.	4187.5	2432.0	95.9	6715.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5880.	4270.5	2294.8	96.3	6661.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
5940.	4353.5	2157.6	96.7	6607.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6000.	4436.6	2020.5	97.0	6554.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6060.	4519.6	1883.3	97.4	6500.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6120.	4602.6	1746.2	97.8	6446.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6180.	4685.6	1609.0	98.2	6392.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6240.	4768.6	1471.8	98.5	6339.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6300.	4851.6	1334.7	98.9	6285.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6360.	4934.6	1197.5	99.3	6231.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6420.	5017.6	1060.4	99.7	6177.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6480.	5100.6	923.2	100.0	6123.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6540.	5183.6	786.1	100.4	6070.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6600.	5266.6	648.9	100.8	6016.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6660.	5349.6	511.7	101.2	5962.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6720.	5432.6	374.6	101.6	5908.7	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6780.	5515.6	237.4	101.9	5855.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
6840.	5598.6	100.3	102.3	5801.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003





Ex. 1, Case 3 (continued)

2580.	358.3	16634.5	39.0	17031.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14.700	147.003
2640.	441.3	16497.3	39.4	16978.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
2700.	524.3	16360.2	39.8	16924.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
2760.	607.3	16223.0	40.1	16870.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
2820.	690.3	16085.8	40.5	16816.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
2880.	773.3	15948.7	40.9	16762.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
2940.	856.3	15811.5	41.3	16709.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3000.	939.3	15674.4	41.7	16655.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3060.	1022.3	15537.2	42.0	16601.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3120.	1105.3	15400.0	42.4	16547.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3180.	1188.3	15262.9	42.8	16494.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3240.	1271.3	15125.7	43.2	16440.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3300.	1354.3	14988.6	43.5	16386.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3360.	1437.3	14851.4	43.9	16332.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3420.	1520.3	14714.2	44.3	16278.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3480.	1603.3	14577.1	44.7	16225.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3540.	1686.3	14439.9	45.0	16171.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3600.	1769.3	14302.8	45.4	16117.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3660.	1852.3	14165.6	45.8	16063.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3720.	1935.3	14028.5	46.2	16010.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3780.	2018.4	13891.3	46.6	15956.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3840.	2101.4	13754.1	46.9	15902.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3900.	2184.4	13617.0	47.3	15848.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
3960.	2267.4	13479.8	47.7	15794.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4020.	2350.4	13342.7	48.1	15741.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4080.	2433.4	13205.5	48.4	15687.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4140.	2516.4	13068.3	48.8	15633.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4200.	2599.4	12931.2	49.2	15579.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4260.	2682.4	12794.0	49.6	15526.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4320.	2765.4	12656.9	49.9	15472.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4380.	2848.4	12519.7	50.3	15418.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4440.	2931.4	12382.5	50.7	15364.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4500.	3014.4	12245.4	51.1	15310.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4560.	3097.4	12108.2	51.5	15257.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4620.	3180.4	11971.1	51.8	15203.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4680.	3263.4	11833.9	52.2	15149.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4740.	3346.4	11696.8	52.6	15095.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4800.	3429.4	11559.6	53.0	15042.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4860.	3512.4	11422.4	53.3	14988.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4920.	3595.4	11285.3	53.7	14934.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
4980.	3678.4	11148.1	54.1	14880.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5040.	3761.4	11011.0	54.5	14826.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5100.	3844.4	10873.8	54.8	14773.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5160.	3927.4	10736.6	55.2	14719.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5220.	4010.4	10599.5	55.6	14665.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5280.	4093.5	10462.3	56.0	14611.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5340.	4176.5	10325.2	56.4	14558.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003
5400.	4259.5	10188.0	56.7	14504.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.896	0.896	14.700	147.003

Ex. 1, Case 3 (continued)

5460.	4342.5	10050.8	57.1	14450.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5520.	4425.5	9913.7	57.5	14396.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5580.	4508.5	9776.5	57.9	14342.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5640.	4591.5	9639.4	58.2	14289.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5700.	4674.5	9502.2	58.6	14235.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5760.	4757.5	9365.1	59.0	14181.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5820.	4840.5	9227.9	59.4	14127.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5880.	4923.5	9090.7	59.7	14074.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
5940.	5006.5	8953.6	60.1	14020.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6000.	5089.5	8816.4	60.5	13966.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6060.	5172.5	8679.3	60.9	13912.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6120.	5255.5	8542.1	61.3	13858.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6180.	5338.5	8404.9	61.6	13805.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6240.	5421.5	8267.8	62.0	13751.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6300.	5504.5	8130.6	62.4	13697.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6360.	5587.5	7993.5	62.8	13643.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6420.	5670.5	7856.3	63.1	13590.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6540.	5836.5	7582.0	63.9	13482.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6600.	5919.5	7444.8	64.3	13428.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6660.	6002.5	7307.7	64.7	13374.9	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6720.	6085.5	7170.5	65.0	13321.1	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6780.	6168.5	7033.4	65.4	13267.3	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6840.	6251.6	6896.2	65.8	13213.5	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6900.	6334.6	6759.0	66.2	13159.8	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
6960.	6417.6	6621.9	66.5	13106.0	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
7020.	6500.6	6484.7	66.9	13052.2	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
7080.	6583.6	6347.6	67.3	12998.4	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003
7140.	6666.6	6210.4	67.7	12944.6	147.307	22.042	VAPOR	22.042	PDC	0.000	0.000	0.000	0.896	14,700	147.003





Ex. 2, Case 1 (continued)

430.	0.0	11383.8	182.3	11566.2	188.045	42.855	LIQUID	45.101	CHOKE	16.157	0.000	16.731	32.887	14.700	133.780
440.	0.0	11052.0	185.3	11237.3	187.978	42.811	LIQUID	45.006	CHOKE	16.148	0.000	16.712	32.860	14.700	133.780
450.	0.0	10720.5	188.2	10908.7	187.908	42.766	LIQUID	44.908	CHOKE	16.140	0.000	16.693	32.833	14.700	133.780
460.	0.0	10389.3	191.0	10580.3	187.837	42.720	LIQUID	44.810	CHOKE	16.131	0.000	16.673	32.804	14.700	133.780
470.	0.0	10058.4	193.9	10252.3	187.763	42.672	LIQUID	44.710	CHOKE	16.122	0.000	16.653	32.775	14.700	133.780
480.	0.0	9727.8	196.8	9924.6	187.688	42.624	LIQUID	44.609	CHOKE	16.113	0.000	16.633	32.745	14.700	133.780
490.	0.0	9397.5	199.6	9597.1	187.610	42.574	LIQUID	44.505	CHOKE	16.103	0.000	16.611	32.714	14.700	133.780
500.	0.0	9067.5	202.5	9270.0	187.531	42.522	LIQUID	44.401	CHOKE	16.093	0.000	16.590	32.683	14.700	133.780
510.	0.0	8737.9	205.3	8943.1	187.448	42.469	LIQUID	44.294	CHOKE	16.083	0.000	16.567	32.650	14.700	133.780
520.	0.0	8408.6	208.1	8616.6	187.363	42.414	LIQUID	44.185	CHOKE	16.072	0.000	16.544	32.616	14.700	133.780
530.	0.0	8079.6	210.8	8290.5	187.275	42.358	LIQUID	44.074	CHOKE	16.062	0.000	16.520	32.581	14.700	133.780
540.	0.0	7751.1	213.5	7964.7	187.184	42.300	LIQUID	43.961	CHOKE	16.050	0.000	16.495	32.545	14.700	133.780
550.	0.0	7422.9	216.3	7639.2	187.090	42.239	LIQUID	43.846	CHOKE	16.039	0.000	16.469	32.508	14.700	133.780
560.	0.0	7095.1	219.1	7314.1	186.992	42.177	LIQUID	43.728	CHOKE	16.027	0.000	16.443	32.469	14.700	133.780
570.	0.0	6767.7	221.8	6989.4	186.891	42.112	LIQUID	43.607	CHOKE	16.014	0.000	16.415	32.429	14.700	133.780
580.	0.0	6440.7	224.4	6665.1	186.785	42.044	LIQUID	43.483	CHOKE	16.001	0.000	16.386	32.387	14.700	133.780
590.	0.0	6114.2	227.1	6341.3	186.675	41.974	LIQUID	43.355	CHOKE	15.987	0.000	16.357	32.344	14.700	133.780
600.	0.0	5788.1	229.7	6017.8	186.560	41.901	LIQUID	43.224	CHOKE	15.973	0.000	16.326	32.299	14.700	133.780
610.	0.0	5462.5	232.3	5694.8	186.440	41.824	LIQUID	43.089	CHOKE	15.958	0.000	16.293	32.251	14.700	133.780
620.	0.0	5137.5	234.9	5372.3	186.314	41.744	LIQUID	42.950	CHOKE	15.943	0.000	16.259	32.202	14.700	133.780
630.	0.0	4812.9	237.4	5050.3	186.182	41.660	LIQUID	42.806	CHOKE	15.926	0.000	16.223	32.150	14.700	133.780
640.	0.0	4488.9	239.9	4728.8	186.043	41.572	LIQUID	42.656	CHOKE	15.909	0.000	16.186	32.095	14.700	133.780
650.	0.0	4165.5	242.3	4407.9	185.895	41.479	LIQUID	42.501	CHOKE	15.891	0.000	16.146	32.037	14.700	133.780
660.	0.0	3842.7	244.7	4087.5	185.739	41.380	LIQUID	42.348	CHOKE	15.871	0.000	16.104	31.976	14.700	133.780
670.	0.0	3520.6	247.1	3767.7	185.573	41.275	LIQUID	42.169	CHOKE	15.851	0.000	16.060	31.911	14.700	133.780
680.	0.0	3199.2	249.4	3448.6	185.395	41.163	LIQUID	41.991	CHOKE	15.829	0.000	16.012	31.841	14.700	133.780
690.	0.0	2878.6	251.6	3130.2	185.204	41.043	LIQUID	41.803	CHOKE	15.805	0.000	15.961	31.766	14.700	133.780
700.	0.0	2558.8	253.8	2812.5	184.997	40.914	LIQUID	41.603	CHOKE	15.779	0.000	15.907	31.686	14.700	133.780
710.	0.0	2239.8	255.9	2495.7	184.772	40.773	LIQUID	41.391	CHOKE	15.751	0.000	15.847	31.598	14.700	133.780
720.	0.0	1921.8	257.9	2179.7	184.526	40.619	LIQUID	41.162	CHOKE	15.721	0.000	15.782	31.502	14.700	133.780
730.	0.0	1605.0	259.7	1864.7	184.252	40.450	LIQUID	40.913	CHOKE	15.687	0.000	15.710	31.397	14.700	133.780
740.	0.0	1289.3	261.4	1550.7	183.946	40.260	LIQUID	40.640	CHOKE	15.644	0.000	15.625	31.269	14.700	133.780
750.	0.0	975.0	263.0	1238.0	183.597	40.045	LIQUID	40.355	CHOKE	15.546	0.000	15.480	31.026	14.700	133.780
760.	0.0	663.5	264.3	927.8	183.193	39.797	LIQUID	39.989	CHOKE	15.436	0.000	15.315	30.751	14.700	133.780
770.	0.0	355.0	265.3	620.3	182.712	39.503	LIQ-VAP	39.503	CHOKE	15.151	0.000	15.023	30.174	14.700	133.780

TITLE: EX. 2, CASE 3. RELEASE FROM 8" BREACH IN SIDE OF 14-T CYL (AS HOLE IN END)

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	MASS (LB)	TEMP (DEG F)	RELEASE RATE (LB/SEC)	TEMP (DEG F)
0.	0.0	25900.0	0.000	14.700
60.	0.0	23879.7	0.000	14.700
120.	0.0	21776.8	0.000	14.700
180.	0.0	19748.2	0.000	14.700
240.	0.0	17725.8	0.000	14.700
300.	0.0	15710.1	0.000	14.700
360.	0.0	13702.0	0.000	14.700
420.	0.0	11702.4	0.000	14.700
480.	0.0	9712.6	0.000	14.700
540.	0.0	7734.2	0.000	14.700
600.	0.0	5769.8	0.000	14.700
660.	0.0	3823.1	0.000	14.700
720.	0.0	1901.4	0.000	14.700

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	SOLID	TOTAL
0.	49.4	25900.0	16.396	33.671
60.	68.6	23879.7	16.371	33.587
120.	87.6	21864.5	16.343	33.496
180.	106.5	19854.7	16.313	33.397
240.	125.1	17850.9	16.280	33.288
300.	143.5	15853.6	16.243	33.167
360.	161.6	13863.6	16.201	33.031
420.	179.3	11881.8	16.153	32.876
480.	196.6	9909.2	16.097	32.695
540.	213.3	7947.5	16.029	32.476
600.	229.2	5999.0	15.943	32.201
660.	243.7	4056.9	15.825	31.828
720.	255.8	2157.2	15.636	31.240

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	LIQUID VAPOR	TOTAL
0.	49.4	25900.0	17.275	33.671
60.	68.6	23879.7	17.216	33.587
120.	87.6	21864.5	17.153	33.496
180.	106.5	19854.7	17.084	33.397
240.	125.1	17850.9	17.008	33.288
300.	143.5	15853.6	16.924	33.167
360.	161.6	13863.6	16.830	33.031
420.	179.3	11881.8	16.723	32.876
480.	196.6	9909.2	16.598	32.695
540.	213.3	7947.5	16.448	32.476
600.	229.2	5999.0	16.259	32.201
660.	243.7	4056.9	16.004	31.828
720.	255.8	2157.2	15.604	31.240

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	LIQUID VAPOR	TOTAL
0.	49.4	25900.0	17.275	33.671
60.	68.6	23879.7	17.216	33.587
120.	87.6	21864.5	17.153	33.496
180.	106.5	19854.7	17.084	33.397
240.	125.1	17850.9	17.008	33.288
300.	143.5	15853.6	16.924	33.167
360.	161.6	13863.6	16.830	33.031
420.	179.3	11881.8	16.723	32.876
480.	196.6	9909.2	16.598	32.695
540.	213.3	7947.5	16.448	32.476
600.	229.2	5999.0	16.259	32.201
660.	243.7	4056.9	16.004	31.828
720.	255.8	2157.2	15.604	31.240

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	LIQUID VAPOR	TOTAL
0.	49.4	25900.0	17.275	33.671
60.	68.6	23879.7	17.216	33.587
120.	87.6	21864.5	17.153	33.496
180.	106.5	19854.7	17.084	33.397
240.	125.1	17850.9	17.008	33.288
300.	143.5	15853.6	16.924	33.167
360.	161.6	13863.6	16.830	33.031
420.	179.3	11881.8	16.723	32.876
480.	196.6	9909.2	16.598	32.695
540.	213.3	7947.5	16.448	32.476
600.	229.2	5999.0	16.259	32.201
660.	243.7	4056.9	16.004	31.828
720.	255.8	2157.2	15.604	31.240

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	LIQUID VAPOR	TOTAL
0.	49.4	25900.0	17.275	33.671
60.	68.6	23879.7	17.216	33.587
120.	87.6	21864.5	17.153	33.496
180.	106.5	19854.7	17.084	33.397
240.	125.1	17850.9	17.008	33.288
300.	143.5	15853.6	16.924	33.167
360.	161.6	13863.6	16.830	33.031
420.	179.3	11881.8	16.723	32.876
480.	196.6	9909.2	16.598	32.695
540.	213.3	7947.5	16.448	32.476
600.	229.2	5999.0	16.259	32.201
660.	243.7	4056.9	16.004	31.828
720.	255.8	2157.2	15.604	31.240

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	LIQUID VAPOR	TOTAL
0.	49.4	25900.0	17.275	33.671
60.	68.6	23879.7	17.216	33.587
120.	87.6	21864.5	17.153	33.496
180.	106.5	19854.7	17.084	33.397
240.	125.1	17850.9	17.008	33.288
300.	143.5	15853.6	16.924	33.167
360.	161.6	13863.6	16.830	33.031
420.	179.3	11881.8	16.723	32.876
480.	196.6	9909.2	16.598	32.695
540.	213.3	7947.5	16.448	32.476
600.	229.2	5999.0	16.259	32.201
660.	243.7	4056.9	16.004	31.828
720.	255.8	2157.2	15.604	31.240

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****		***** CONDITION OF UF6 EXHAUSTED *****	
	LIQUID VAPOR	TOTAL	LIQUID VAPOR	TOTAL
0.	49.4	25900.0	17.275	33.671
60.	68.6	23879.7	17.216	33.587
120.	87.6	21864.5	17.153	33.496
180.	106.5	19854.7	17.084	33.397
240.	125.1	17850.9	17.008	33.288
300.	143.5	15853.6	16.924	33.167
360.	161.6	13863.6	16.830	33.031
420.	179.3	11881.8	16.723	32.876
480.	196.6	9909.2	16.598	32.695
540.	213.3	7947.5	16.448	32.476
600.	229.2	5999.0	16.259	32.201
660.	243.7	4056.9	16.004	31.828
720.	255.8	2157.2	15.604	31.240

TITLE: EX. 3, CASE 1. 14-TON CYL W/ RUPTURED PIGTAIL (6 IN)

TIME (SEC)	***** CONDITION OF UF6 IN CONTAINMENT *****			***** CONDITION OF UF6 EXHAUSTED *****									
	SOLID	LIQUID	VAPOR	TEMP (DEG F)	PRES (PSIA)	PATHWAY	INLET	FLOW RATE BASIS	SOLID	LIQUID	VAPOR	TEMP (DEG F)	PRES (PSIA)
0.	0.0	25948.1	51.9	26000.0	200.000				0.000	0.000	2.126	14.700	198.784
30.	0.0	25883.8	52.4	25936.2	199.368				0.000	0.000	2.108	14.700	198.165
60.	0.0	25820.1	52.9	25873.0	198.740				0.000	0.000	2.090	14.700	197.549
90.	0.0	25757.0	53.3	25810.3	198.115				0.000	0.000	2.072	14.700	196.936
120.	0.0	25694.4	53.7	25748.1	197.493				0.000	0.000	2.055	14.700	196.326
150.	0.0	25632.3	54.2	25686.5	196.874				0.000	0.000	2.037	14.700	195.720
180.	0.0	25570.8	54.6	25625.4	196.259				0.000	0.000	2.020	14.700	195.117
210.	0.0	25509.8	54.9	25564.8	195.647				0.000	0.000	2.002	14.700	194.517
240.	0.0	25449.4	55.3	25504.7	195.039				0.000	0.000	1.983	14.700	193.920
270.	0.0	25389.6	55.6	25445.2	194.434				0.000	0.000	1.966	14.700	193.327
300.	0.0	25330.3	56.0	25386.2	193.833				0.000	0.000	1.951	14.700	192.737
330.	0.0	25271.4	56.3	25327.7	193.234				0.000	0.000	1.934	14.700	192.150
360.	0.0	25213.1	56.6	25269.7	192.639				0.000	0.000	1.918	14.700	191.566
390.	0.0	25155.2	56.9	25212.1	192.047				0.000	0.000	1.903	14.700	190.986
420.	0.0	25097.9	57.2	25155.0	191.458				0.000	0.000	1.887	14.700	190.408
450.	0.0	25041.0	57.5	25098.4	190.871				0.000	0.000	1.872	14.700	189.832
480.	0.0	24984.6	57.7	25042.3	190.288				0.000	0.000	1.856	14.700	189.260
510.	0.0	24928.6	58.0	24986.6	189.708				0.000	0.000	1.838	14.700	188.691
540.	0.0	24873.3	58.2	24931.5	189.133				0.000	0.000	1.823	14.700	188.126
570.	0.0	24818.4	58.4	24876.8	188.560				0.000	0.000	1.808	14.700	187.564
600.	0.0	24763.9	58.6	24822.6	187.990				0.000	0.000	1.791	14.700	187.005
630.	0.0	24710.0	58.8	24768.8	187.423				0.000	0.000	1.777	14.700	186.449
660.	0.0	24656.5	59.0	24715.5	186.860				0.000	0.000	1.762	14.700	185.896
690.	0.0	24603.5	59.2	24662.7	186.300				0.000	0.000	1.748	14.700	185.346
720.	0.0	24550.9	59.4	24610.2	185.742				0.000	0.000	1.735	14.700	184.799
750.	0.0	24498.6	59.5	24558.2	185.187				0.000	0.000	1.720	14.700	184.254
780.	0.0	24446.9	59.7	24506.6	184.636				0.000	0.000	1.703	14.700	183.713
810.	0.0	24395.7	59.8	24455.5	184.088				0.000	0.000	1.689	14.700	183.175
840.	0.0	24344.9	60.0	24404.8	183.543				0.000	0.000	1.676	14.700	182.640
870.	0.0	24294.5	60.1	24354.5	183.001				0.000	0.000	1.662	14.700	182.108



TITLE: EX. 3, CASE 2. 14-TON CYL W/ RUPTURED PIGTAIL (2 FT)

TIME (SEC)	***** CONDITION OF UFG6 IN CONTAINMENT *****			PATHWAY INLET	FLOW RATE	***** CONDITION OF UFG6 EXHAUSTED *****									
	***** MASS (LB) *****	***** TEMP (DEG F) *****	***** PRES (PSIA) *****			***** RELEASE PHASE *****	***** PRES (PSIA) *****	***** RELEASE RATE (LB/SEC) *****	***** TEMP (DEG F) *****	***** PRES (PSIA) *****					
	SOLID	LIQUID	VAPOR	TOTAL	TEMP (DEG F)	PRES (PSIA)	RELEASE PHASE	PATHWAY INLET	FLOW RATE	SOLID	LIQUID	VAPOR	TOTAL	TEMP (DEG F)	PRES (PSIA)
0.	0.0	25948.1	51.9	26000.0	200.000	51.152	VAPOR	51.152	PDC	0.000	0.000	1.914	1.914	14.700	198.784
30.	0.0	25890.2	52.4	25942.6	199.431	50.732	VAPOR	50.732	PDC	0.000	0.000	1.899	1.899	14.700	198.227
60.	0.0	25832.9	52.8	25885.6	198.866	50.317	VAPOR	50.317	PDC	0.000	0.000	1.884	1.884	14.700	197.673
90.	0.0	25775.9	53.2	25829.1	198.303	49.906	VAPOR	49.906	PDC	0.000	0.000	1.870	1.870	14.700	197.121
120.	0.0	25719.5	53.6	25773.0	197.742	49.499	VAPOR	49.499	PDC	0.000	0.000	1.855	1.855	14.700	196.571
150.	0.0	25663.4	53.9	25717.4	197.185	49.097	VAPOR	49.097	PDC	0.000	0.000	1.841	1.841	14.700	196.024
180.	0.0	25607.8	54.3	25662.1	196.630	48.699	VAPOR	48.699	PDC	0.000	0.000	1.826	1.826	14.700	195.480
210.	0.0	25552.7	54.7	25607.4	196.078	48.307	VAPOR	48.307	PDC	0.000	0.000	1.811	1.811	14.700	194.939
240.	0.0	25498.0	55.0	25553.0	195.529	47.918	VAPOR	47.918	PDC	0.000	0.000	1.798	1.798	14.700	194.401
270.	0.0	25443.8	55.3	25499.1	194.982	47.533	VAPOR	47.533	PDC	0.000	0.000	1.784	1.784	14.700	193.865
300.	0.0	25389.9	55.6	25445.6	194.438	47.153	VAPOR	47.153	PDC	0.000	0.000	1.770	1.770	14.700	193.331
330.	0.0	25336.5	56.0	25392.5	193.897	46.777	VAPOR	46.777	PDC	0.000	0.000	1.757	1.757	14.700	192.800
360.	0.0	25283.5	56.2	25339.8	193.358	46.405	VAPOR	46.405	PDC	0.000	0.000	1.743	1.743	14.700	192.272
390.	0.0	25231.0	56.5	25287.5	192.822	46.037	VAPOR	46.037	PDC	0.000	0.000	1.729	1.729	14.700	191.746
420.	0.0	25178.8	56.8	25235.6	192.289	45.673	VAPOR	45.673	PDC	0.000	0.000	1.716	1.716	14.700	191.223
450.	0.0	25127.1	57.1	25184.1	191.759	45.313	VAPOR	45.313	PDC	0.000	0.000	1.702	1.702	14.700	190.703
480.	0.0	25075.8	57.3	25133.1	191.231	44.958	VAPOR	44.958	PDC	0.000	0.000	1.689	1.689	14.700	190.185
510.	0.0	25024.8	57.5	25082.4	190.706	44.606	VAPOR	44.606	PDC	0.000	0.000	1.676	1.676	14.700	189.670
540.	0.0	24974.3	57.8	25032.1	190.183	44.258	VAPOR	44.258	PDC	0.000	0.000	1.664	1.664	14.700	189.157
570.	0.0	24924.2	58.0	24982.2	189.663	43.913	VAPOR	43.913	PDC	0.000	0.000	1.650	1.650	14.700	188.647
600.	0.0	24874.5	58.2	24932.7	189.146	43.573	VAPOR	43.573	PDC	0.000	0.000	1.638	1.638	14.700	188.140
630.	0.0	24825.1	58.4	24883.5	188.631	43.236	VAPOR	43.236	PDC	0.000	0.000	1.625	1.625	14.700	187.635
660.	0.0	24776.2	58.6	24834.8	188.119	42.903	VAPOR	42.903	PDC	0.000	0.000	1.614	1.614	14.700	187.132
690.	0.0	24727.6	58.8	24786.4	187.610	42.573	VAPOR	42.573	PDC	0.000	0.000	1.600	1.600	14.700	186.632
720.	0.0	24679.4	58.9	24738.4	187.103	42.247	VAPOR	42.247	PDC	0.000	0.000	1.588	1.588	14.700	186.135
750.	0.0	24631.6	59.1	24690.7	186.599	41.925	VAPOR	41.925	PDC	0.000	0.000	1.576	1.576	14.700	185.640
780.	0.0	24584.2	59.3	24643.4	186.097	41.606	VAPOR	41.606	PDC	0.000	0.000	1.565	1.565	14.700	185.147
810.	0.0	24537.1	59.4	24596.5	185.597	41.290	VAPOR	41.290	PDC	0.000	0.000	1.553	1.553	14.700	184.657
840.	0.0	24490.3	59.6	24549.9	185.100	40.978	VAPOR	40.978	PDC	0.000	0.000	1.540	1.540	14.700	184.169
870.	0.0	24444.0	59.7	24503.7	184.606	40.670	VAPOR	40.670	PDC	0.000	0.000	1.529	1.529	14.700	183.684

TITLE: EX. 3, CASE 3, 14-TON CYL W/ RUPTURED PIGTAIL (4 FT)

TIME (SEC)	***** CONDITION OF UFG IN CONTAINMENT *****				PATHWAY	INLET		FLOW RATE BASIS	***** CONDITION OF UFG EXHAUSTED *****					
	SOLID	LIQUID	MASS (LB) VAPOR	TOTAL		TEMP (DEG F)	PRES (PSIA)		RELEASE PHASE	PRES (PSIA)	SOLID	LIQUID	RELEASE RATE (LB/SEC) VAPOR	TOTAL
0.	0.0	25948.1	51.9	26000.0	0	200.000	51.152	VAPOR	51.152	PDC	0.000	1.754	14.700	198.784
30.	0.0	25895.1	52.3	25947.4	199.479	198.960	50.767	VAPOR	50.767	PDC	0.000	1.741	14.700	198.274
60.	0.0	25842.4	52.7	25895.1	198.960	198.444	50.386	VAPOR	50.386	PDC	0.000	1.728	14.700	197.765
90.	0.0	25790.2	53.1	25843.3	198.444	197.930	50.009	VAPOR	50.009	PDC	0.000	1.716	14.700	197.259
120.	0.0	25738.4	53.4	25791.8	197.930	197.419	49.635	VAPOR	49.635	PDC	0.000	1.704	14.700	196.756
150.	0.0	25686.9	53.8	25740.7	197.419	196.910	49.266	VAPOR	49.266	PDC	0.000	1.691	14.700	196.254
180.	0.0	25635.8	54.1	25690.0	196.910	196.403	48.900	VAPOR	48.900	PDC	0.000	1.679	14.700	195.755
210.	0.0	25585.1	54.5	25639.6	196.403	195.899	48.538	VAPOR	48.538	PDC	0.000	1.667	14.700	195.258
240.	0.0	25534.8	54.8	25589.6	195.899	195.397	48.179	VAPOR	48.179	PDC	0.000	1.654	14.700	194.763
270.	0.0	25484.9	55.1	25540.0	195.397	194.897	47.825	VAPOR	47.825	PDC	0.000	1.642	14.700	194.271
300.	0.0	25435.3	55.4	25490.7	194.897	194.400	47.474	VAPOR	47.474	PDC	0.000	1.630	14.700	193.781
330.	0.0	25386.1	55.7	25441.8	194.400	193.905	47.127	VAPOR	47.127	PDC	0.000	1.619	14.700	193.294
360.	0.0	25337.3	55.9	25393.2	193.905	193.413	46.783	VAPOR	46.783	PDC	0.000	1.607	14.700	192.808
390.	0.0	25288.8	56.2	25345.0	193.413	192.922	46.442	VAPOR	46.442	PDC	0.000	1.596	14.700	192.325
420.	0.0	25240.7	56.5	25297.2	192.922	192.434	46.106	VAPOR	46.106	PDC	0.000	1.584	14.700	191.844
450.	0.0	25192.9	56.7	25249.6	192.434	191.948	45.772	VAPOR	45.772	PDC	0.000	1.573	14.700	191.365
480.	0.0	25145.5	57.0	25202.5	191.948	191.465	45.442	VAPOR	45.442	PDC	0.000	1.562	14.700	190.889
510.	0.0	25098.4	57.2	25155.6	191.465	190.983	45.115	VAPOR	45.115	PDC	0.000	1.551	14.700	190.414
540.	0.0	25051.7	57.4	25109.1	190.983	190.504	44.791	VAPOR	44.791	PDC	0.000	1.540	14.700	189.942
570.	0.0	25005.3	57.6	25062.9	190.504	190.027	44.471	VAPOR	44.471	PDC	0.000	1.529	14.700	189.472
600.	0.0	24959.2	57.8	25017.0	190.027	189.552	44.154	VAPOR	44.154	PDC	0.000	1.518	14.700	189.004
630.	0.0	24913.5	58.0	24971.5	189.552	189.080	43.840	VAPOR	43.840	PDC	0.000	1.507	14.700	188.538
660.	0.0	24868.1	58.2	24926.3	189.080	188.610	43.529	VAPOR	43.529	PDC	0.000	1.497	14.700	188.075
690.	0.0	24823.0	58.4	24881.4	188.610	188.141	43.222	VAPOR	43.222	PDC	0.000	1.486	14.700	187.613
720.	0.0	24778.2	58.6	24836.8	188.141	187.675	42.917	VAPOR	42.917	PDC	0.000	1.476	14.700	187.154
750.	0.0	24733.8	58.7	24792.5	187.675	187.211	42.616	VAPOR	42.616	PDC	0.000	1.465	14.700	186.696
780.	0.0	24689.7	58.9	24748.6	187.211	186.750	42.317	VAPOR	42.317	PDC	0.000	1.454	14.700	186.241
810.	0.0	24645.9	59.1	24704.9	186.750	186.291	42.022	VAPOR	42.022	PDC	0.000	1.444	14.700	185.788
840.	0.0	24602.4	59.2	24661.6	186.291	185.834	41.729	VAPOR	41.729	PDC	0.000	1.434	14.700	185.338
870.	0.0	24559.3	59.4	24618.6	185.834		41.440	VAPOR	41.440	PDC	0.000	1.424	14.700	184.889

TITLE: EX. 4, CASE 1. RELEASE (EX. 2.2), FORCED VENT, AIRBORNE SOLIDS  
 DATA GENERATED BY FDRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

COMPARTMENT CONDITIONS

COMPARTMENT VOLUME = 500000. FT\*\*2  
 UMA PRODUCT = 7.903E+00 BTU/SEC-DEG F  
 SURFACE TEMPERATURE = 120.0 DEG F  
 COOLING RATE = 0.000E+00 BTU/SEC

TIME (SEC)	AIR V	H2O L	H2O V	HF L	HF V	COMPONENT MASS (LB)	UF6 S	UF6 L	UF6 V	UO2F2 S	TEMPERATURE (DEG F)	TEMPERATURE PRESSURE (PSIA)
0.0	3.548E+04	0.000E+00	4.630E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.7500
120.0	3.240E+04	0.000E+00	8.722E+01	0.000E+00	7.454E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	134.0796	14.7871
240.0	3.198E+04	0.000E+00	0.000E+00	0.000E+00	9.270E+02	0.000E+00	0.000E+00	0.000E+00	1.555E+03	3.213E+03	135.9586	14.7603
360.0	3.227E+04	0.000E+00	0.000E+00	0.000E+00	9.355E+02	0.000E+00	0.000E+00	0.000E+00	3.220E+03	3.087E+03	128.3078	14.7632
480.0	3.244E+04	0.000E+00	0.000E+00	0.000E+00	9.404E+02	0.000E+00	0.000E+00	0.000E+00	4.361E+03	3.004E+03	123.7446	14.7659
600.0	3.254E+04	0.000E+00	0.000E+00	0.000E+00	9.432E+02	0.000E+00	0.000E+00	0.000E+00	5.123E+03	2.949E+03	121.0188	14.7673
720.0	3.259E+04	0.000E+00	0.000E+00	0.000E+00	9.448E+02	0.000E+00	0.000E+00	0.000E+00	5.598E+03	2.913E+03	119.4511	14.7686
840.0	3.245E+04	0.000E+00	0.000E+00	0.000E+00	9.408E+02	0.000E+00	0.000E+00	0.000E+00	4.104E+03	2.875E+03	124.0808	14.7706
960.0	3.222E+04	0.000E+00	0.000E+00	0.000E+00	9.340E+02	0.000E+00	0.000E+00	0.000E+00	1.617E+03	2.839E+03	131.6553	14.7662
1080.0	3.216E+04	0.000E+00	1.120E+01	0.000E+00	9.073E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.730E+03	134.7454	14.7475
1200.0	3.326E+04	0.000E+00	1.371E+02	0.000E+00	6.597E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.797E+03	118.4066	14.7483
1320.0	3.400E+04	0.000E+00	2.282E+02	0.000E+00	4.786E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.181E+03	108.1649	14.7489
1440.0	3.449E+04	0.000E+00	2.940E+02	0.000E+00	3.467E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.744E+02	101.6697	14.7493
1560.0	3.482E+04	0.000E+00	3.415E+02	0.000E+00	2.509E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.074E+02	97.5195	14.7495
1680.0	3.504E+04	0.000E+00	3.756E+02	0.000E+00	1.814E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.323E+02	94.8546	14.7494
1800.0	3.518E+04	0.000E+00	4.001E+02	0.000E+00	1.312E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.175E+02	93.1375	14.7496
1920.0	3.528E+04	0.000E+00	4.177E+02	0.000E+00	9.479E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.423E+02	92.0294	14.7496
2040.0	3.534E+04	0.000E+00	4.304E+02	0.000E+00	6.849E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.312E+01	91.3131	14.7497
2160.0	3.539E+04	0.000E+00	4.395E+02	0.000E+00	4.949E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.092E+01	90.8528	14.7499
2280.0	3.541E+04	0.000E+00	4.461E+02	0.000E+00	3.575E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.985E+01	90.5538	14.7500
2400.0	3.543E+04	0.000E+00	4.508E+02	0.000E+00	2.983E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.606E+01	90.3688	14.7501
2520.0	3.545E+04	0.000E+00	4.542E+02	0.000E+00	1.866E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.705E+01	90.2307	14.7498
2640.0	3.546E+04	0.000E+00	4.567E+02	0.000E+00	1.348E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.115E+01	90.1489	14.7498
2760.0	3.546E+04	0.000E+00	4.584E+02	0.000E+00	9.735E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.293E+00	90.0959	14.7498
2880.0	3.547E+04	0.000E+00	4.597E+02	0.000E+00	7.032E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.770E+00	90.0695	14.7500
3000.0	3.547E+04	0.000E+00	4.606E+02	0.000E+00	5.079E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.120E+00	90.0433	14.7500
3120.0	3.547E+04	0.000E+00	4.613E+02	0.000E+00	3.669E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.041E+00	90.0302	14.7500
3240.0	3.547E+04	0.000E+00	4.618E+02	0.000E+00	2.650E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.335E+00	90.0171	14.7500
3360.0	3.547E+04	0.000E+00	4.621E+02	0.000E+00	1.914E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.729E-01	90.0171	14.7500
3480.0	3.547E+04	0.000E+00	4.623E+02	0.000E+00	1.383E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.709E-01	90.0171	14.7500
3600.0	3.547E+04	0.000E+00	4.625E+02	0.000E+00	9.989E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.734E-01	90.0041	14.7500



TITLE: EX. 4, CASE 1, RELEASE (EX. 2.2), FORCED VENT, AIRBORNE SOLIDS  
 DATA GENERATED BY FODRAFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 SOURCE TERM: SOURCE TERM MASS FLOW RATES, TEMPERATURE, AND PRESSURE WERE READ FROM DATA FILE.

TIME (SEC)	COMPONENT MASS FLOW RATE (LB/SEC)						UF6 S		UF6 V		UF6 L		UF6 V		UF6 L		UF6 V		UF6 L		TEMPERATURE PRESSURE (DEG F) (PSIA)			
	AIR	V	H2O	L	H2O	V	HF	L	HF	V	UF6	S	UF6	L	UF6	V	UF6	L	UF6	V	UF6	S	TEMPERATURE (DEG F)	PRESSURE (PSIA)
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
120.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
240.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
360.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
480.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
600.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
720.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000

TITLE: EX. 4, CASE 1. RELEASE (EX. 2.2), FORCED VENT, AIRBORNE SOLIDS

DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

EXHAUST STREAM (FORCED DRAFT)

RESISTANCE TERM = 3.798E-07 PSI-SEC\*\*2/LB/FT\*\*3

TIME (SEC)	AIR V	H20 L	H20 V	HF L	HF V	COMPONENT MASS FLOW RATE (LB/SEC)	UF6 S	UF6 L	UF6 V	UF6 W	TEMPERATURE (DEG F)	PRESSURE (PSIA)
0.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.7500
120.0	1.157E+02	0.000E+00	3.114E-01	0.000E+00	2.661E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.789E+00	134.0796	14.7871
240.0	9.284E+01	0.000E+00	0.000E+00	0.000E+00	2.691E+00	0.000E+00	0.000E+00	0.000E+00	4.513E+00	9.328E+00	135.9586	14.7603
360.0	9.364E+01	0.000E+00	0.000E+00	0.000E+00	2.715E+00	0.000E+00	0.000E+00	0.000E+00	9.343E+00	8.959E+00	128.3078	14.7632
480.0	9.465E+01	0.000E+00	0.000E+00	0.000E+00	2.744E+00	0.000E+00	0.000E+00	0.000E+00	1.272E+01	8.765E+00	123.7446	14.7659
600.0	9.503E+01	0.000E+00	0.000E+00	0.000E+00	2.759E+00	0.000E+00	0.000E+00	0.000E+00	1.496E+01	8.613E+00	121.0188	14.7673
720.0	9.555E+01	0.000E+00	0.000E+00	0.000E+00	2.770E+00	0.000E+00	0.000E+00	0.000E+00	1.641E+01	8.539E+00	119.4511	14.7686
840.0	9.850E+01	0.000E+00	0.000E+00	0.000E+00	2.855E+00	0.000E+00	0.000E+00	0.000E+00	1.245E+01	8.724E+00	124.0808	14.7706
960.0	9.811E+01	0.000E+00	0.000E+00	0.000E+00	2.844E+00	0.000E+00	0.000E+00	0.000E+00	4.925E+00	8.645E+00	131.6553	14.7662
1080.0	8.501E+01	0.000E+00	2.960E-02	0.000E+00	2.398E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.217E+00	134.7454	14.7475
1200.0	8.856E+01	0.000E+00	3.650E-01	0.000E+00	1.757E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.786E+00	118.4066	14.7483
1320.0	9.105E+01	0.000E+00	6.112E-01	0.000E+00	1.282E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.162E+00	108.1649	14.7489
1440.0	9.271E+01	0.000E+00	7.904E-01	0.000E+00	9.319E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.082E+00	101.6697	14.7493
1560.0	9.382E+01	0.000E+00	9.201E-01	0.000E+00	6.761E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.367E+00	97.5195	14.7495
1680.0	9.431E+01	0.000E+00	1.011E+00	0.000E+00	4.884E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.945E-01	94.8546	14.7494
1800.0	9.487E+01	0.000E+00	1.079E+00	0.000E+00	3.537E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.865E-01	93.1375	14.7496
1920.0	9.513E+01	0.000E+00	1.126E+00	0.000E+00	2.556E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.838E-01	92.0294	14.7496
2040.0	9.543E+01	0.000E+00	1.162E+00	0.000E+00	1.849E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.514E-01	91.3131	14.7497
2160.0	9.567E+01	0.000E+00	1.188E+00	0.000E+00	1.358E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.647E-01	90.8528	14.7499
2280.0	9.582E+01	0.000E+00	1.207E+00	0.000E+00	9.673E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.078E-01	90.5538	14.7501
2400.0	9.598E+01	0.000E+00	1.221E+00	0.000E+00	6.995E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.060E-02	90.3688	14.7501
2520.0	9.578E+01	0.000E+00	1.227E+00	0.000E+00	5.041E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.606E-02	90.2307	14.7498
2640.0	9.579E+01	0.000E+00	1.234E+00	0.000E+00	3.641E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.013E-02	90.1489	14.7488
2760.0	9.581E+01	0.000E+00	1.239E+00	0.000E+00	2.630E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.970E-02	90.0959	14.7498
2880.0	9.601E+01	0.000E+00	1.245E+00	0.000E+00	1.904E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.291E-02	90.0695	14.7500
3000.0	9.602E+01	0.000E+00	1.247E+00	0.000E+00	1.375E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.446E-03	90.0433	14.7500
3120.0	9.602E+01	0.000E+00	1.249E+00	0.000E+00	9.932E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.524E-03	90.0302	14.7500
3240.0	9.602E+01	0.000E+00	1.250E+00	0.000E+00	7.174E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.613E-03	90.0171	14.7500
3360.0	9.602E+01	0.000E+00	1.251E+00	0.000E+00	5.162E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.363E-03	90.0171	14.7500
3480.0	9.603E+01	0.000E+00	1.252E+00	0.000E+00	3.743E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.545E-03	90.0171	14.7500
3600.0	9.603E+01	0.000E+00	1.252E+00	0.000E+00	2.704E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.011E-03	90.0041	14.7500







TITLE: EX. 4, CASE 1. RELEASE (EX. 2.2), FORCED VENT, AIRBORNE SOLIDS  
 DATA GENERATED BY FOORFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT CONCENTRATIONS

TIME (SEC)	CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED MATERIAL (LB)				COMPARTMENT CONCENTRATIONS (LB/FT**3)	
	UF6	UO2F2	TOTAL U	HF	URANIUM	HF
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
120.0	0.000E+00	6.401E+02	4.946E+02	1.714E+02	4.237E-03	1.491E-03
240.0	1.915E+02	1.834E+03	1.546E+03	5.045E+02	7.068E-03	1.854E-03
360.0	1.041E+03	2.933E+03	2.971E+03	8.301E+02	9.126E-03	1.871E-03
480.0	2.382E+03	4.001E+03	4.702E+03	1.159E+03	1.054E-02	1.881E-03
600.0	4.058E+03	5.047E+03	6.644E+03	1.490E+03	1.149E-02	1.886E-03
720.0	5.953E+03	6.079E+03	8.723E+03	1.823E+03	1.207E-02	1.890E-03
840.0	7.844E+03	7.116E+03	1.080E+04	2.161E+03	9.992E-03	1.882E-03
960.0	8.861E+03	8.154E+03	1.229E+04	2.502E+03	6.575E-03	1.868E-03
1080.0	9.120E+03	9.173E+03	1.326E+04	2.837E+03	4.219E-03	1.815E-03
1200.0	9.120E+03	9.884E+03	1.380E+04	3.085E+03	2.778E-03	1.319E-03
1320.0	9.120E+03	1.036E+04	1.417E+04	3.266E+03	1.825E-03	9.572E-04
1440.0	9.120E+03	1.067E+04	1.441E+04	3.398E+03	1.197E-03	6.934E-04
1560.0	9.120E+03	1.087E+04	1.457E+04	3.494E+03	7.843E-04	5.018E-04
1680.0	9.120E+03	1.100E+04	1.467E+04	3.563E+03	5.136E-04	3.629E-04
1800.0	9.120E+03	1.109E+04	1.474E+04	3.614E+03	3.362E-04	2.623E-04
1920.0	9.120E+03	1.115E+04	1.478E+04	3.650E+03	2.200E-04	1.896E-04
2040.0	9.120E+03	1.119E+04	1.481E+04	3.676E+03	1.439E-04	1.370E-04
2160.0	9.120E+03	1.121E+04	1.483E+04	3.695E+03	9.415E-05	9.897E-05
2280.0	9.120E+03	1.123E+04	1.484E+04	3.709E+03	6.159E-05	7.150E-05
2400.0	9.120E+03	1.124E+04	1.485E+04	3.719E+03	4.028E-05	5.165E-05
2520.0	9.120E+03	1.125E+04	1.486E+04	3.726E+03	2.635E-05	3.731E-05
2640.0	9.120E+03	1.125E+04	1.486E+04	3.731E+03	1.723E-05	2.695E-05
2760.0	9.120E+03	1.125E+04	1.486E+04	3.735E+03	1.127E-05	1.947E-05
2880.0	9.120E+03	1.126E+04	1.486E+04	3.738E+03	7.373E-06	1.406E-05
3000.0	9.120E+03	1.126E+04	1.487E+04	3.740E+03	4.822E-06	1.016E-05
3120.0	9.120E+03	1.126E+04	1.487E+04	3.741E+03	3.154E-06	7.338E-06
3240.0	9.120E+03	1.126E+04	1.487E+04	3.742E+03	2.063E-06	5.301E-06
3360.0	9.120E+03	1.126E+04	1.487E+04	3.743E+03	1.349E-06	3.829E-06
3480.0	9.120E+03	1.126E+04	1.487E+04	3.743E+03	8.824E-07	2.668E-06
3600.0	9.120E+03	1.126E+04	1.487E+04	3.744E+03	5.771E-07	1.998E-06

TITLE: EX. 4, CASE 2. RELEASE (EX. 2.2), INDUCED VENT, AIRBORNE SOLIDS  
DATA GENERATED BY INDRFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

COMPARTMENT CONDITIONS

COMPARTMENT VOLUME = 500000. FT\*\*2  
LWA PRODUCT = 7.733E+00 BTU/SEC-DEG F  
SURFACE TEMPERATURE = 120.0 DEG F  
COOLING RATE = 0.000E+00 BTU/SEC

TIME (SEC)	AIR V	H20 L	H20 V	HF L	HF V	COMPONENT MASS (LB)						U02F2 S	TEMPERATURE (DEG F)	PRESSURE (PSIA)
						H20 L	H20 V	HF L	HF V	UF6 L	UF6 S			
0.0	3.524E+04	0.000E+00	4.599E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.6500
120.0	3.135E+04	0.000E+00	5.556E+01	0.000E+00	7.853E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	148.6713	14.6811
240.0	3.095E+04	0.000E+00	0.000E+00	0.000E+00	8.972E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	150.8196	14.6611
360.0	3.105E+04	0.000E+00	0.000E+00	0.000E+00	9.002E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	146.1227	14.6608
480.0	3.110E+04	0.000E+00	0.000E+00	0.000E+00	9.016E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	143.1848	14.6597
600.0	3.113E+04	0.000E+00	0.000E+00	0.000E+00	9.024E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	141.3893	14.6610
720.0	3.114E+04	0.000E+00	0.000E+00	0.000E+00	9.028E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	140.2905	14.6612
840.0	3.123E+04	0.000E+00	0.000E+00	0.000E+00	9.053E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	140.6654	14.6590
960.0	3.136E+04	0.000E+00	0.000E+00	0.000E+00	9.091E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	141.9990	14.6608
1080.0	3.146E+04	0.000E+00	0.000E+00	0.000E+00	9.119E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	142.8290	14.6592
1200.0	3.212E+04	0.000E+00	6.463E+01	0.000E+00	7.875E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	132.9291	14.6475
1320.0	3.317E+04	0.000E+00	1.755E+02	0.000E+00	5.716E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	117.1900	14.6484
1440.0	3.386E+04	0.000E+00	2.551E+02	0.000E+00	4.149E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	107.3898	14.6489
1560.0	3.432E+04	0.000E+00	3.123E+02	0.000E+00	3.011E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	101.1908	14.6493
1680.0	3.462E+04	0.000E+00	3.534E+02	0.000E+00	2.186E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	97.2302	14.6496
1800.0	3.482E+04	0.000E+00	3.831E+02	0.000E+00	1.587E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	94.7005	14.6500
1920.0	3.496E+04	0.000E+00	4.044E+02	0.000E+00	1.152E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	93.0491	14.6500
2040.0	3.505E+04	0.000E+00	4.198E+02	0.000E+00	8.359E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	91.9873	14.6501
2160.0	3.511E+04	0.000E+00	4.309E+02	0.000E+00	6.067E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	91.2959	14.6501
2280.0	3.515E+04	0.000E+00	4.389E+02	0.000E+00	4.404E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.8422	14.6501
2400.0	3.518E+04	0.000E+00	4.447E+02	0.000E+00	3.196E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.5454	14.6500
2520.0	3.520E+04	0.000E+00	4.489E+02	0.000E+00	2.320E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.3595	14.6500
2640.0	3.521E+04	0.000E+00	4.519E+02	0.000E+00	1.684E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.2360	14.6500
2760.0	3.522E+04	0.000E+00	4.541E+02	0.000E+00	1.222E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.1553	14.6500
2880.0	3.522E+04	0.000E+00	4.557E+02	0.000E+00	8.872E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.1020	14.6500
3000.0	3.523E+04	0.000E+00	4.568E+02	0.000E+00	6.440E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0626	14.6499
3120.0	3.523E+04	0.000E+00	4.577E+02	0.000E+00	4.674E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0494	14.6500
3240.0	3.523E+04	0.000E+00	4.583E+02	0.000E+00	3.393E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0363	14.6500
3360.0	3.523E+04	0.000E+00	4.587E+02	0.000E+00	2.462E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0232	14.6500
3480.0	3.523E+04	0.000E+00	4.590E+02	0.000E+00	1.787E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0102	14.6500
3600.0	3.523E+04	0.000E+00	4.592E+02	0.000E+00	1.297E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0102	14.6500

TITLE: EX. 4, CASE 2. RELEASE (EX. 2.2), INDUCED DRAFT, AIRBORNE SOLIDS  
 DATA GENERATED BY INDRAFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

INLET AIR STREAM (INDUCED DRAFT) RESISTANCE TERM = 4.026E-07 PSI-SEC\*\*2/LB/FT\*\*3  
 AMBIENT TEMPERATURE = 80.000 DEG F  
 AMBIENT PRESSURE = 14.700 PSIA

TIME (SEC)	AIR		H2O		L		HF		V		UO2F2		TEMPERATURE	
	V	L	H2O	L	HF	L	HF	V	UO2F2	S	(DEG F)	PSIA)		
0.0	9.396E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
120.0	5.781E+01	0.000E+00	7.545E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
240.0	8.285E+01	0.000E+00	1.081E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
360.0	8.319E+01	0.000E+00	1.086E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
480.0	8.435E+01	0.000E+00	1.101E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
600.0	8.304E+01	0.000E+00	1.084E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
720.0	8.277E+01	0.000E+00	1.080E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
840.0	8.508E+01	0.000E+00	1.110E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
960.0	8.321E+01	0.000E+00	1.086E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1080.0	8.487E+01	0.000E+00	1.108E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1200.0	9.628E+01	0.000E+00	1.257E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1320.0	9.547E+01	0.000E+00	1.246E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1440.0	9.494E+01	0.000E+00	1.239E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1560.0	9.460E+01	0.000E+00	1.235E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1680.0	9.438E+01	0.000E+00	1.232E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1800.0	9.397E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1920.0	9.397E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2040.0	9.388E+01	0.000E+00	1.225E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2160.0	9.386E+01	0.000E+00	1.225E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2280.0	9.391E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2400.0	9.400E+01	0.000E+00	1.227E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2520.0	9.392E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2640.0	9.392E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2760.0	9.393E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2880.0	9.394E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3000.0	9.402E+01	0.000E+00	1.227E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3120.0	9.395E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3240.0	9.395E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3360.0	9.396E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3480.0	9.396E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3600.0	9.396E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000

TITLE: EX. 4, CASE 2. RELEASE (EX. 2.2), INDUCED VENT, AIRBORNE SOLIDS

DATA GENERATED BY INDRFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

SOURCE TERM: SOURCE TERM MASS FLOW RATES, TEMPERATURE, AND PRESSURE WERE READ FROM DATA FILE.

TIME (SEC)	AIR		H2O		H2O		HF		HF		V		U02F2		TEMPERATURE		PRESSURE (PSIA)
	V	L	V	L	V	L	V	L	V	L	S	V	S	(DEG F)	(PSIA)		
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.727E+01	0.000E+00	0.000E+00	133.7805	14.7000	
120.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.716E+01	0.000E+00	0.000E+00	133.7805	14.7000	
240.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.702E+01	0.000E+00	0.000E+00	133.7805	14.7000	
360.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.685E+01	0.000E+00	0.000E+00	133.7805	14.7000	
480.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.663E+01	0.000E+00	0.000E+00	133.7805	14.7000	
600.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.631E+01	0.000E+00	0.000E+00	133.7805	14.7000	
720.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.575E+01	0.000E+00	0.000E+00	133.7805	14.7000	

TITLE: EX. 4, CASE 2. RELEASE (EX. 2.2), INDUCED VENT, AIRBORNE SOLIDS  
 DATA GENERATED BY INDRFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 EXHAUST BLOWER FLOW RATE = 80000.0 ACFM

TIME (SEC)	AIR V	H2O L	H2O V	HF L	HF V	COMPONENT MASS FLOW RATE (LB/SEC)	U02F2 S	TEMPERATURE (DEG F)	TEMPERATURE PRESSURE (PSIA)
0.0	9.396E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.6500
120.0	8.359E+01	0.000E+00	1.481E-01	0.000E+00	2.094E+00	0.000E+00	0.000E+00	148.6713	14.6811
240.0	8.254E+01	0.000E+00	0.000E+00	0.000E+00	2.393E+00	0.000E+00	0.000E+00	150.8196	14.6611
360.0	8.281E+01	0.000E+00	0.000E+00	0.000E+00	2.400E+00	0.000E+00	0.000E+00	146.1227	14.6608
480.0	8.294E+01	0.000E+00	0.000E+00	0.000E+00	2.404E+00	0.000E+00	0.000E+00	143.1848	14.6597
600.0	8.302E+01	0.000E+00	0.000E+00	0.000E+00	2.406E+00	0.000E+00	0.000E+00	141.3893	14.6610
720.0	8.305E+01	0.000E+00	0.000E+00	0.000E+00	2.407E+00	0.000E+00	0.000E+00	140.2905	14.6612
840.0	8.328E+01	0.000E+00	0.000E+00	0.000E+00	2.414E+00	0.000E+00	0.000E+00	140.6654	14.6590
960.0	8.363E+01	0.000E+00	0.000E+00	0.000E+00	2.414E+00	0.000E+00	0.000E+00	141.9990	14.6608
1080.0	8.389E+01	0.000E+00	0.000E+00	0.000E+00	2.432E+00	0.000E+00	0.000E+00	142.8290	14.6592
1200.0	8.565E+01	0.000E+00	1.724E-01	0.000E+00	2.100E+00	0.000E+00	0.000E+00	132.9291	14.6475
1320.0	8.844E+01	0.000E+00	4.680E-01	0.000E+00	1.524E+00	0.000E+00	0.000E+00	117.1900	14.6484
1440.0	9.029E+01	0.000E+00	6.802E-01	0.000E+00	1.106E+00	0.000E+00	0.000E+00	107.3898	14.6489
1560.0	9.151E+01	0.000E+00	8.328E-01	0.000E+00	8.030E-01	0.000E+00	0.000E+00	101.1908	14.6493
1680.0	9.232E+01	0.000E+00	9.425E-01	0.000E+00	5.829E-01	0.000E+00	0.000E+00	97.2302	14.6496
1800.0	9.286E+01	0.000E+00	1.078E+00	0.000E+00	4.231E-01	0.000E+00	0.000E+00	94.7005	14.6500
2040.0	9.346E+01	0.000E+00	1.119E+00	0.000E+00	2.229E-01	0.000E+00	0.000E+00	93.0491	14.6500
2160.0	9.363E+01	0.000E+00	1.149E+00	0.000E+00	1.618E-01	0.000E+00	0.000E+00	91.9873	14.6501
2280.0	9.373E+01	0.000E+00	1.170E+00	0.000E+00	1.174E-01	0.000E+00	0.000E+00	91.2959	14.6501
2400.0	9.381E+01	0.000E+00	1.186E+00	0.000E+00	8.524E-02	0.000E+00	0.000E+00	90.8422	14.6501
2520.0	9.386E+01	0.000E+00	1.197E+00	0.000E+00	6.187E-02	0.000E+00	0.000E+00	90.5454	14.6500
2640.0	9.389E+01	0.000E+00	1.205E+00	0.000E+00	4.491E-02	0.000E+00	0.000E+00	90.3595	14.6500
2760.0	9.391E+01	0.000E+00	1.211E+00	0.000E+00	3.259E-02	0.000E+00	0.000E+00	90.2360	14.6500
2880.0	9.393E+01	0.000E+00	1.215E+00	0.000E+00	2.366E-02	0.000E+00	0.000E+00	90.1553	14.6500
3000.0	9.394E+01	0.000E+00	1.218E+00	0.000E+00	1.717E-02	0.000E+00	0.000E+00	90.1020	14.6500
3120.0	9.395E+01	0.000E+00	1.220E+00	0.000E+00	1.246E-03	0.000E+00	0.000E+00	90.0626	14.6499
3240.0	9.395E+01	0.000E+00	1.222E+00	0.000E+00	9.047E-03	0.000E+00	0.000E+00	90.0494	14.6500
3360.0	9.395E+01	0.000E+00	1.223E+00	0.000E+00	6.567E-03	0.000E+00	0.000E+00	90.0363	14.6500
3480.0	9.396E+01	0.000E+00	1.224E+00	0.000E+00	4.766E-03	0.000E+00	0.000E+00	90.0232	14.6500
3600.0	9.396E+01	0.000E+00	1.225E+00	0.000E+00	3.460E-03	0.000E+00	0.000E+00	90.0102	14.6500





TITLE: EX. 4, CASE 2. RELEASE (EX. 2.2), INDUCED VENT, AIRBORNE SOLIDS  
 DATA GENERATED BY INDRAFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT CONCENTRATIONS

TIME (SEC)	CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED MATERIAL (LB)				COMPARTMENT CONCENTRATIONS (LB/FT**3)	
	UF6	UO2F2	TOTAL U	HF	URANIUM	HF
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
120.0	0.000E+00	4.906E+02	3.791E+02	1.314E+02	4.460E-03	1.571E-03
240.0	2.756E+02	1.499E+03	1.345E+03	4.148E+02	7.471E-03	1.794E-03
360.0	1.211E+03	2.463E+03	2.722E+03	7.024E+02	9.644E-03	1.800E-03
480.0	2.628E+03	3.388E+03	4.395E+03	9.907E+02	1.120E-02	1.803E-03
600.0	4.385E+03	4.288E+03	6.279E+03	1.279E+03	1.229E-02	1.805E-03
720.0	6.373E+03	5.171E+03	8.306E+03	1.568E+03	1.300E-02	1.806E-03
840.0	8.363E+03	6.044E+03	1.033E+04	1.857E+03	1.107E-02	1.811E-03
960.0	9.570E+03	6.913E+03	1.181E+04	2.148E+03	7.677E-03	1.818E-03
1080.0	1.009E+04	7.780E+03	1.284E+04	2.439E+03	5.217E-03	1.824E-03
1200.0	1.016E+04	8.611E+03	1.352E+04	2.722E+03	3.448E-03	1.575E-03
1320.0	1.016E+04	9.195E+03	1.397E+04	2.938E+03	2.266E-03	1.143E-03
1440.0	1.016E+04	9.579E+03	1.427E+04	3.094E+03	1.489E-03	8.298E-04
1560.0	1.016E+04	9.832E+03	1.446E+04	3.208E+03	9.788E-04	6.023E-04
1680.0	1.016E+04	9.997E+03	1.459E+04	3.291E+03	6.433E-04	4.372E-04
1800.0	1.016E+04	1.011E+04	1.468E+04	3.351E+03	4.228E-04	3.173E-04
1920.0	1.016E+04	1.018E+04	1.473E+04	3.394E+03	2.779E-04	2.303E-04
2040.0	1.016E+04	1.023E+04	1.477E+04	3.426E+03	1.826E-04	1.672E-04
2160.0	1.016E+04	1.028E+04	1.481E+04	3.449E+03	1.200E-04	1.213E-04
2280.0	1.016E+04	1.028E+04	1.481E+04	3.465E+03	7.888E-05	8.807E-05
2400.0	1.016E+04	1.029E+04	1.482E+04	3.477E+03	5.184E-05	6.393E-05
2520.0	1.016E+04	1.030E+04	1.483E+04	3.486E+03	3.407E-05	4.640E-05
2640.0	1.016E+04	1.030E+04	1.483E+04	3.492E+03	2.239E-05	3.368E-05
2760.0	1.016E+04	1.031E+04	1.483E+04	3.497E+03	1.472E-05	2.445E-05
2880.0	1.016E+04	1.031E+04	1.483E+04	3.500E+03	9.673E-06	1.774E-05
3000.0	1.016E+04	1.031E+04	1.484E+04	3.503E+03	6.357E-06	1.288E-05
3120.0	1.016E+04	1.031E+04	1.484E+04	3.505E+03	4.178E-06	9.348E-06
3240.0	1.016E+04	1.031E+04	1.484E+04	3.506E+03	2.746E-06	6.785E-06
3360.0	1.016E+04	1.031E+04	1.484E+04	3.507E+03	1.805E-06	4.925E-06
3480.0	1.016E+04	1.031E+04	1.484E+04	3.508E+03	1.186E-06	3.575E-06
3600.0	1.016E+04	1.031E+04	1.484E+04	3.508E+03	7.795E-07	2.595E-06



TITLE: EX. 4, CASE 3. RELEASE (EX. 2.2), FORCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

COMPARTMENT CONDITIONS

COMPARTMENT VOLUME = 50000. FT\*\*2  
 DWA PRODUCT = 7.903E+00 BTU/SEC-DEG F  
 SURFACE TEMPERATURE = 120.0 DEG F  
 COOLING RATE = 0.000E+00 BTU/SEC

TIME (SEC)	AIR V	H2O L	H2O V	HF L	HF V	COMPONENT MASS (LB)	U02F2 S	U02F2 S	TEMPERATURE (DEG F)	TEMPERATURE PRESSURE (PSIA)
0.0	3.548E+04	0.000E+00	4.630E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.7500
120.0	3.351E+04	0.000E+00	2.621E+02	0.000E+00	3.893E+02	0.000E+00	0.000E+00	1.431E+03	118.3174	14.7714
240.0	3.230E+04	0.000E+00	1.283E+02	0.000E+00	6.514E+02	0.000E+00	0.000E+00	2.303E+03	136.2934	14.7693
360.0	3.158E+04	0.000E+00	3.935E+01	0.000E+00	8.280E+02	0.000E+00	0.000E+00	2.833E+03	147.3134	14.7680
480.0	3.132E+04	0.000E+00	0.000E+00	0.000E+00	9.079E+02	0.000E+00	0.000E+00	3.005E+03	150.6106	14.7626
600.0	3.141E+04	0.000E+00	0.000E+00	0.000E+00	9.105E+02	0.000E+00	0.000E+00	2.919E+03	148.2761	14.7617
720.0	3.147E+04	0.000E+00	0.000E+00	0.000E+00	9.122E+02	0.000E+00	0.000E+00	2.865E+03	146.9060	14.7631
840.0	3.156E+04	0.000E+00	0.000E+00	0.000E+00	9.149E+02	0.000E+00	0.000E+00	2.835E+03	146.1753	14.7606
960.0	3.284E+04	0.000E+00	1.278E+02	0.000E+00	6.681E+02	0.000E+00	0.000E+00	1.877E+03	125.6005	14.7474
1080.0	3.372E+04	0.000E+00	2.217E+02	0.000E+00	4.852E+02	0.000E+00	0.000E+00	1.234E+03	112.6702	14.7483
1200.0	3.431E+04	0.000E+00	2.894E+02	0.000E+00	3.517E+02	0.000E+00	0.000E+00	8.100E+02	104.5255	14.7489
1320.0	3.470E+04	0.000E+00	3.382E+02	0.000E+00	2.546E+02	0.000E+00	0.000E+00	5.310E+02	99.3438	14.7493
1440.0	3.496E+04	0.000E+00	3.733E+02	0.000E+00	1.842E+02	0.000E+00	0.000E+00	3.478E+02	96.0259	14.7495
1560.0	3.513E+04	0.000E+00	3.985E+02	0.000E+00	1.332E+02	0.000E+00	0.000E+00	2.277E+02	93.8922	14.7495
1680.0	3.524E+04	0.000E+00	4.166E+02	0.000E+00	9.627E+01	0.000E+00	0.000E+00	1.490E+02	92.5164	14.7497
1800.0	3.532E+04	0.000E+00	4.297E+02	0.000E+00	6.957E+01	0.000E+00	0.000E+00	9.750E+01	91.6398	14.7500
1920.0	3.537E+04	0.000E+00	4.390E+02	0.000E+00	5.026E+01	0.000E+00	0.000E+00	6.379E+01	91.0611	14.7500
2040.0	3.541E+04	0.000E+00	4.457E+02	0.000E+00	3.631E+01	0.000E+00	0.000E+00	4.173E+01	90.6941	14.7501
2160.0	3.543E+04	0.000E+00	4.506E+02	0.000E+00	2.623E+01	0.000E+00	0.000E+00	2.729E+01	90.4474	14.7500
2280.0	3.544E+04	0.000E+00	4.540E+02	0.000E+00	1.895E+01	0.000E+00	0.000E+00	1.785E+01	90.2935	14.7500
2400.0	3.545E+04	0.000E+00	4.563E+02	0.000E+00	1.369E+01	0.000E+00	0.000E+00	1.168E+01	90.1848	14.7498
2520.0	3.546E+04	0.000E+00	4.583E+02	0.000E+00	9.888E+00	0.000E+00	0.000E+00	7.637E+00	90.1316	14.7500
2640.0	3.547E+04	0.000E+00	4.596E+02	0.000E+00	7.143E+00	0.000E+00	0.000E+00	4.995E+00	90.0786	14.7500
2760.0	3.547E+04	0.000E+00	4.606E+02	0.000E+00	5.160E+00	0.000E+00	0.000E+00	3.267E+00	90.0523	14.7500
2880.0	3.547E+04	0.000E+00	4.612E+02	0.000E+00	3.727E+00	0.000E+00	0.000E+00	2.137E+00	90.0391	14.7500
3000.0	3.547E+04	0.000E+00	4.617E+02	0.000E+00	2.692E+00	0.000E+00	0.000E+00	1.398E+00	90.0261	14.7500
3120.0	3.547E+04	0.000E+00	4.621E+02	0.000E+00	1.945E+00	0.000E+00	0.000E+00	9.142E-01	90.0131	14.7500
3240.0	3.547E+04	0.000E+00	4.623E+02	0.000E+00	1.405E+00	0.000E+00	0.000E+00	5.979E-01	90.0131	14.7500
3360.0	3.547E+04	0.000E+00	4.625E+02	0.000E+00	1.015E+00	0.000E+00	0.000E+00	3.911E-01	90.0131	14.7500
3480.0	3.547E+04	0.000E+00	4.626E+02	0.000E+00	7.329E-01	0.000E+00	0.000E+00	2.558E-01	90.0131	14.7500
3600.0	3.547E+04	0.000E+00	4.627E+02	0.000E+00	5.294E-01	0.000E+00	0.000E+00	1.673E-01	90.0131	14.7500

TITLE: EX. 4, CASE 3. RELEASE (EX. 2.2), FORCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

INLET AIR BLOWER

FLOW RATE = 0.0 ACM  
 AMBIENT TEMPERATURE = 80.000 DEG F  
 AMBIENT PRESSURE = 14.700 PSIA

TIME (SEC)	AIR	COMPONENT MASS FLOW RATE (LB/SEC)						U02F2 S	TEMPERATURE (DEG F)	PRESSURE (PSIA)
		H20	L	HF	V	UF6	S			
0.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
120.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
240.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
360.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
480.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
600.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
720.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
840.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
960.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1080.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1200.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1320.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1440.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1560.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1680.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1800.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
1920.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2040.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2160.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2280.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2400.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2520.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2640.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2760.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
2880.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
3000.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
3120.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
3240.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
3360.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
3480.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	
3600.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000	

TITLE: EX. 4, CASE 3. RELEASE (EX. 2.2), FORCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

SOURCE TERM: SOURCE TERM MASS FLOW RATES, TEMPERATURE, AND PRESSURE WERE READ FROM DATA FILE.

TIME (SEC)	AIR						COMPONENT MASS FLOW RATE (LB/SEC)						TEMPERATURE		TEMPERATURE PRESSURE					
	V	H20	L	H20	V	H20	HF	L	HF	V	UF6	S	UF6	L	UF6	V	UF6	S	(DEG F)	(PSIA)
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.727E+01	0.000E+00	0.000E+00	133.7805	14.7000
120.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.716E+01	0.000E+00	0.000E+00	133.7805	14.7000
240.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.702E+01	0.000E+00	0.000E+00	133.7805	14.7000
360.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.685E+01	0.000E+00	0.000E+00	133.7805	14.7000
480.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.663E+01	0.000E+00	0.000E+00	133.7805	14.7000
600.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.631E+01	0.000E+00	0.000E+00	133.7805	14.7000
720.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.575E+01	0.000E+00	0.000E+00	133.7805	14.7000

TITLE: EX. 4, CASE 3. RELEASE (EX. 2.2), FORCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 EXHAUST STREAM (FORCED DRAFT) RESISTANCE TERM = 3.798E-07 PSI-SEC\*\*2/LB/FT\*\*3

TIME (SEC)	AIR V	H20 L	H20 V	HF L	HF V	COMPONENT MASS FLOW RATE (LB/SEC)	UF6 S	UF6 L	UF6 V	UO2F2 S	TEMPERATURE (DEG F)	PRESSURE (PSIA)
0.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.7500
120.0	1.089E+02	0.000E+00	8.517E-01	0.000E+00	1.265E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.651E+00	118.3174	14.7714
240.0	1.037E+02	0.000E+00	4.120E-01	0.000E+00	2.092E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.397E+00	136.2934	14.7693
360.0	1.006E+02	0.000E+00	1.254E-01	0.000E+00	2.638E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.029E+00	147.3134	14.7680
480.0	9.557E+01	0.000E+00	0.000E+00	0.000E+00	2.770E+00	0.000E+00	0.000E+00	0.000E+00	5.756E-01	9.169E+00	150.6106	14.7626
600.0	9.467E+01	0.000E+00	0.000E+00	0.000E+00	2.744E+00	0.000E+00	0.000E+00	0.000E+00	1.685E+00	8.798E+00	148.2761	14.7617
720.0	9.555E+01	0.000E+00	0.000E+00	0.000E+00	2.770E+00	0.000E+00	0.000E+00	0.000E+00	2.357E+00	8.698E+00	146.9060	14.7631
840.0	9.488E+01	0.000E+00	0.000E+00	0.000E+00	2.750E+00	0.000E+00	0.000E+00	0.000E+00	5.001E-02	8.523E+00	146.1753	14.7606
960.0	8.707E+01	0.000E+00	3.388E-01	0.000E+00	1.772E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.976E+00	125.6005	14.7474
1080.0	9.007E+01	0.000E+00	5.920E-01	0.000E+00	1.296E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.296E+00	112.6702	14.7483
1200.0	9.207E+01	0.000E+00	7.767E-01	0.000E+00	9.439E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.174E+00	104.5255	14.7489
1320.0	9.340E+01	0.000E+00	9.104E-01	0.000E+00	6.854E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.429E+00	99.3438	14.7493
1440.0	9.429E+01	0.000E+00	1.007E+00	0.000E+00	4.968E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.380E-01	96.0259	14.7495
1560.0	9.464E+01	0.000E+00	1.074E+00	0.000E+00	3.588E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.134E-01	93.8922	14.7495
1680.0	9.511E+01	0.000E+00	1.124E+00	0.000E+00	2.598E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.021E-01	92.5164	14.7497
1800.0	9.568E+01	0.000E+00	1.164E+00	0.000E+00	1.885E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.641E-01	91.6398	14.7500
1920.0	9.577E+01	0.000E+00	1.189E+00	0.000E+00	1.361E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.727E-01	91.0611	14.7500
2040.0	9.593E+01	0.000E+00	1.208E+00	0.000E+00	9.838E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.131E-01	90.6941	14.7501
2160.0	9.593E+01	0.000E+00	1.220E+00	0.000E+00	7.103E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.390E-02	90.4474	14.7500
2280.0	9.599E+01	0.000E+00	1.230E+00	0.000E+00	5.132E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.835E-02	90.2935	14.7500
2400.0	9.580E+01	0.000E+00	1.234E+00	0.000E+00	3.699E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.155E-02	90.1848	14.7498
2520.0	9.601E+01	0.000E+00	1.241E+00	0.000E+00	2.677E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.068E-02	90.1316	14.7500
2640.0	9.602E+01	0.000E+00	1.244E+00	0.000E+00	1.934E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.352E-02	90.0786	14.7500
2760.0	9.602E+01	0.000E+00	1.247E+00	0.000E+00	1.397E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.845E-03	90.0523	14.7500
2880.0	9.602E+01	0.000E+00	1.249E+00	0.000E+00	1.009E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.785E-03	90.0391	14.7500
3000.0	9.602E+01	0.000E+00	1.250E+00	0.000E+00	7.288E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.784E-03	90.0261	14.7500
3120.0	9.602E+01	0.000E+00	1.251E+00	0.000E+00	5.264E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.475E-03	90.0131	14.7500
3240.0	9.603E+01	0.000E+00	1.252E+00	0.000E+00	3.802E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.618E-03	90.0131	14.7500
3360.0	9.603E+01	0.000E+00	1.252E+00	0.000E+00	2.747E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.059E-03	90.0131	14.7500
3480.0	9.603E+01	0.000E+00	1.252E+00	0.000E+00	1.984E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.923E-04	90.0131	14.7500
3600.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	1.433E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.528E-04	90.0131	14.7500





TITLE: EX. 4, CASE 3. RELEASE (EX. 2.2), FORCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT CONCENTRATIONS

TIME (SEC)	CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED MATERIAL (LB)			COMPARTMENT CONCENTRATIONS (LB/FT**3)		
	UF6	TOTAL U	HF	URANIUM	HF	HF
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
120.0	0.000E+00	2.330E+02	8.073E+01	0.000E+00	2.212E-03	7.785E-04
240.0	0.000E+00	1.037E+03	2.851E+02	0.000E+00	3.560E-03	1.303E-03
360.0	0.000E+00	2.030E+03	1.569E+03	5.709E+02	4.379E-03	1.656E-03
480.0	1.303E+01	3.147E+03	2.441E+03	2.963E+03	4.899E-03	1.816E-03
600.0	1.559E+02	4.226E+03	3.370E+03	1.234E+03	5.268E-03	1.821E-03
720.0	4.014E+02	5.280E+03	4.352E+03	1.566E+03	5.477E-03	1.824E-03
840.0	6.233E+02	6.313E+03	5.300E+03	1.898E+03	4.404E-03	1.830E-03
960.0	6.234E+02	7.055E+03	5.874E+03	2.148E+03	2.900E-03	1.336E-03
1080.0	6.234E+02	7.546E+03	6.253E+03	2.331E+03	1.907E-03	9.704E-04
1200.0	6.234E+02	7.870E+03	6.503E+03	2.464E+03	1.252E-03	7.035E-04
1320.0	6.234E+02	8.083E+03	6.668E+03	2.562E+03	8.206E-04	5.093E-04
1440.0	6.234E+02	8.224E+03	6.777E+03	2.632E+03	5.375E-04	3.684E-04
1560.0	6.234E+02	8.316E+03	6.848E+03	2.683E+03	3.519E-04	2.664E-04
1680.0	6.234E+02	8.376E+03	6.894E+03	2.720E+03	2.303E-04	1.925E-04
1800.0	6.234E+02	8.415E+03	6.925E+03	2.747E+03	1.507E-04	1.391E-04
1920.0	6.234E+02	8.441E+03	6.945E+03	2.765E+03	9.859E-05	1.005E-04
2040.0	6.234E+02	8.458E+03	6.958E+03	2.780E+03	6.449E-05	7.262E-05
2160.0	6.234E+02	8.469E+03	6.966E+03	2.790E+03	4.218E-05	5.247E-05
2280.0	6.234E+02	8.476E+03	6.972E+03	2.797E+03	2.759E-05	3.790E-05
2400.0	6.234E+02	8.481E+03	6.976E+03	2.802E+03	1.805E-05	2.738E-05
2520.0	6.234E+02	8.484E+03	6.978E+03	2.806E+03	1.180E-05	1.978E-05
2640.0	6.234E+02	8.486E+03	6.980E+03	2.809E+03	7.721E-06	1.429E-05
2760.0	6.234E+02	8.488E+03	6.981E+03	2.811E+03	5.050E-06	1.032E-05
2880.0	6.234E+02	8.488E+03	6.982E+03	2.812E+03	3.303E-06	7.454E-06
3000.0	6.234E+02	8.489E+03	6.982E+03	2.813E+03	2.160E-06	5.384E-06
3120.0	6.234E+02	8.489E+03	6.982E+03	2.814E+03	1.413E-06	3.889E-06
3240.0	6.234E+02	8.490E+03	6.982E+03	2.815E+03	9.241E-07	2.809E-06
3360.0	6.234E+02	8.490E+03	6.982E+03	2.815E+03	6.044E-07	2.029E-06
3480.0	6.234E+02	8.490E+03	6.982E+03	2.815E+03	3.933E-07	1.466E-06
3600.0	6.234E+02	8.490E+03	6.982E+03	2.815E+03	2.585E-07	1.059E-06

TITLE: EX. 4, CASE 4. RELEASE (EX. 2.2), INDUCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY INDRFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

COMPARTMENT CONDITIONS

COMPARTMENT VOLUME = 500000. FT\*\*2  
 UXA PRODUCT = 7.733E+00 BTU/SEC-DEG F  
 SURFACE TEMPERATURE = 120.0 DEG F  
 COOLING RATE = 0.000E+00 BTU/SEC

TIME (SEC)	AIR V	H2O L	H2O V	H2O H	H2O V	H2O H	COMPONENT MASS (LB)	UF6 S	UF6 L	UF6 V	UF6 S	UF6 L	UF6 V	UO2F2 S	TEMPERATURE (DEG F)	TEMPERATURE PRESSURE (PSIA)
0.0	3.524E+04	0.000E+00	4.599E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.6500
120.0	3.322E+04	0.000E+00	2.523E+02	0.000E+00	4.026E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.479E+03	119.0574	14.6681
240.0	3.191E+04	0.000E+00	1.050E+02	0.000E+00	6.918E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.441E+03	138.7703	14.6669
360.0	3.108E+04	0.000E+00	1.279E+00	0.000E+00	8.982E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.060E+03	151.5805	14.6660
480.0	3.121E+04	0.000E+00	0.000E+00	0.000E+00	9.046E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.939E+03	147.9825	14.6606
600.0	3.130E+04	0.000E+00	0.000E+00	0.000E+00	9.073E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.853E+03	145.5106	14.6597
720.0	3.135E+04	0.000E+00	0.000E+00	0.000E+00	9.089E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.795E+03	143.9634	14.6588
840.0	3.143E+04	0.000E+00	0.000E+00	0.000E+00	9.112E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.761E+03	143.6034	14.6593
960.0	3.225E+04	0.000E+00	8.026E+01	0.000E+00	7.565E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.154E+03	131.0129	14.6476
1080.0	3.325E+04	0.000E+00	1.867E+02	0.000E+00	5.491E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.415E+03	116.0086	14.6484
1200.0	3.391E+04	0.000E+00	2.632E+02	0.000E+00	3.986E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.302E+02	106.6472	14.6490
1320.0	3.435E+04	0.000E+00	3.181E+02	0.000E+00	2.893E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.113E+02	100.7183	14.6493
1440.0	3.465E+04	0.000E+00	3.576E+02	0.000E+00	2.100E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.018E+02	96.9272	14.6496
1560.0	3.484E+04	0.000E+00	3.861E+02	0.000E+00	1.524E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.641E+02	94.4881	14.6495
1680.0	3.497E+04	0.000E+00	4.066E+02	0.000E+00	1.106E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.735E+02	92.9118	14.6496
1800.0	3.506E+04	0.000E+00	4.214E+02	0.000E+00	8.030E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.141E+02	91.8911	14.6496
1920.0	3.511E+04	0.000E+00	4.320E+02	0.000E+00	5.828E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.496E+01	91.2332	14.6499
2040.0	3.515E+04	0.000E+00	4.397E+02	0.000E+00	4.230E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.927E+01	90.8073	14.6501
2160.0	3.518E+04	0.000E+00	4.453E+02	0.000E+00	3.071E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.238E+01	90.5266	14.6500
2280.0	3.520E+04	0.000E+00	4.493E+02	0.000E+00	2.229E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.128E+01	90.3421	14.6500
2400.0	3.521E+04	0.000E+00	4.522E+02	0.000E+00	1.618E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.399E+01	90.2311	14.6500
2520.0	3.522E+04	0.000E+00	4.543E+02	0.000E+00	1.174E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.192E+00	90.1499	14.6500
2640.0	3.522E+04	0.000E+00	4.559E+02	0.000E+00	8.523E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.041E+00	90.0967	14.6500
2760.0	3.523E+04	0.000E+00	4.570E+02	0.000E+00	6.186E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.970E+00	90.0704	14.6500
2880.0	3.523E+04	0.000E+00	4.578E+02	0.000E+00	4.490E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.609E+00	90.0443	14.6500
3000.0	3.523E+04	0.000E+00	4.583E+02	0.000E+00	3.259E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.715E+00	90.0312	14.6500
3120.0	3.523E+04	0.000E+00	4.588E+02	0.000E+00	2.366E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.127E+00	90.0181	14.6500
3240.0	3.523E+04	0.000E+00	4.591E+02	0.000E+00	1.717E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.408E-01	90.0181	14.6500
3360.0	3.523E+04	0.000E+00	4.593E+02	0.000E+00	1.246E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.868E-01	90.0181	14.6500
3480.0	3.523E+04	0.000E+00	4.594E+02	0.000E+00	9.046E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.200E-01	90.0051	14.6500
3600.0	3.523E+04	0.000E+00	4.595E+02	0.000E+00	6.566E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.103E-01	90.0051	14.6500





TITLE: EX. 4, CASE 4. RELEASE (EX. 2.2), INDUCED VENT, SOLIDS TO FLOOR

DATA GENERATED BY INDRFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

SOURCE TERM: SOURCE TERM MASS FLOW RATES, TEMPERATURE, AND PRESSURE WERE READ FROM DATA FILE.

TIME (SEC)	AIR		H2O		H2O		HF		HF		V		UF6		UF6		UF6		TEMPERATURE (DEG F)	PRESSURE (PSIA)
	V	L	V	L	V	L	V	L	V	L	V	L	V	L	V	L	V	L		
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
120.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
240.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
360.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
480.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
600.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000
720.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	133.7805	14.7000

TITLE: EX. 4, CASE 4. RELEASE (EX. 2.2), INDUCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY INDRAFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 EXHAUST BLOWER FLOW RATE = 80000.0 ACFM

TIME (SEC)	AIR V	H20 L	H20 V	COMPONENT MASS FLOW RATE (LB/SEC)				U02F2 S	TEMPERATURE (DEG F)	PRESSURE (PSIA)
				HF L	HF V	UF6 L	UF6 S			
0.0	9.396E+01	0.000E+00	1.226E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.6500
120.0	8.859E+01	0.000E+00	6.729E-01	0.000E+00	1.074E+00	0.000E+00	0.000E+00	0.000E+00	119.0574	14.6681
240.0	8.309E+01	0.000E+00	2.800E-01	0.000E+00	1.845E+00	0.000E+00	0.000E+00	0.000E+00	138.7703	14.6669
360.0	8.289E+01	0.000E+00	3.409E-03	0.000E+00	2.395E+00	0.000E+00	0.000E+00	0.000E+00	151.5805	14.6660
480.0	8.321E+01	0.000E+00	0.000E+00	0.000E+00	2.412E+00	0.000E+00	0.000E+00	0.000E+00	147.9825	14.6606
600.0	8.346E+01	0.000E+00	0.000E+00	0.000E+00	2.419E+00	0.000E+00	0.000E+00	0.000E+00	145.5106	14.6597
720.0	8.361E+01	0.000E+00	0.000E+00	0.000E+00	2.424E+00	0.000E+00	0.000E+00	0.000E+00	143.9654	14.6588
840.0	8.382E+01	0.000E+00	0.000E+00	0.000E+00	2.430E+00	0.000E+00	0.000E+00	0.000E+00	143.6034	14.6593
960.0	8.399E+01	0.000E+00	2.140E-01	0.000E+00	2.017E+00	0.000E+00	0.000E+00	0.000E+00	131.0129	14.6476
1080.0	8.867E+01	0.000E+00	4.980E-01	0.000E+00	1.464E+00	0.000E+00	0.000E+00	0.000E+00	116.0086	14.6484
1200.0	9.044E+01	0.000E+00	7.018E-01	0.000E+00	1.063E+00	0.000E+00	0.000E+00	0.000E+00	106.6472	14.6490
1320.0	9.161E+01	0.000E+00	8.483E-01	0.000E+00	7.714E-01	0.000E+00	0.000E+00	0.000E+00	100.7183	14.6493
1440.0	9.239E+01	0.000E+00	9.537E-01	0.000E+00	5.599E-01	0.000E+00	0.000E+00	0.000E+00	96.9272	14.6496
1560.0	9.291E+01	0.000E+00	1.030E+00	0.000E+00	4.064E-01	0.000E+00	0.000E+00	0.000E+00	94.4881	14.6495
1680.0	9.325E+01	0.000E+00	1.084E+00	0.000E+00	2.950E-01	0.000E+00	0.000E+00	0.000E+00	92.9118	14.6496
1800.0	9.348E+01	0.000E+00	1.124E+00	0.000E+00	2.141E-01	0.000E+00	0.000E+00	0.000E+00	91.8911	14.6496
1920.0	9.364E+01	0.000E+00	1.152E+00	0.000E+00	1.554E-01	0.000E+00	0.000E+00	0.000E+00	91.2332	14.6499
2040.0	9.374E+01	0.000E+00	1.173E+00	0.000E+00	1.128E-01	0.000E+00	0.000E+00	0.000E+00	90.8073	14.6501
2160.0	9.381E+01	0.000E+00	1.187E+00	0.000E+00	8.188E-02	0.000E+00	0.000E+00	0.000E+00	90.5266	14.6500
2280.0	9.386E+01	0.000E+00	1.198E+00	0.000E+00	5.943E-02	0.000E+00	0.000E+00	0.000E+00	90.3421	14.6500
2400.0	9.389E+01	0.000E+00	1.206E+00	0.000E+00	4.314E-02	0.000E+00	0.000E+00	0.000E+00	90.2311	14.6500
2520.0	9.391E+01	0.000E+00	1.212E+00	0.000E+00	3.131E-02	0.000E+00	0.000E+00	0.000E+00	90.1499	14.6500
2640.0	9.393E+01	0.000E+00	1.216E+00	0.000E+00	2.273E-02	0.000E+00	0.000E+00	0.000E+00	90.0967	14.6500
2760.0	9.394E+01	0.000E+00	1.219E+00	0.000E+00	1.650E-02	0.000E+00	0.000E+00	0.000E+00	90.0704	14.6500
2880.0	9.394E+01	0.000E+00	1.221E+00	0.000E+00	1.197E-02	0.000E+00	0.000E+00	0.000E+00	90.0443	14.6500
3000.0	9.395E+01	0.000E+00	1.222E+00	0.000E+00	8.691E-03	0.000E+00	0.000E+00	0.000E+00	90.0312	14.6500
3120.0	9.395E+01	0.000E+00	1.223E+00	0.000E+00	6.308E-03	0.000E+00	0.000E+00	0.000E+00	90.0181	14.6500
3240.0	9.395E+01	0.000E+00	1.224E+00	0.000E+00	4.579E-03	0.000E+00	0.000E+00	0.000E+00	90.0181	14.6500
3360.0	9.395E+01	0.000E+00	1.225E+00	0.000E+00	3.323E-03	0.000E+00	0.000E+00	0.000E+00	90.0181	14.6500
3480.0	9.396E+01	0.000E+00	1.225E+00	0.000E+00	2.412E-03	0.000E+00	0.000E+00	0.000E+00	90.0051	14.6500
3600.0	9.396E+01	0.000E+00	1.225E+00	0.000E+00	1.751E-03	0.000E+00	0.000E+00	0.000E+00	90.0051	14.6500





TITLE: EX. 4, CASE 4. RELEASE (EX. 2.2), INDUCED VENT, SOLIDS TO FLOOR  
 DATA GENERATED BY INDRFT -- AN INDUCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT CONCENTRATIONS

TIME (SEC)	CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED MATERIAL (LB)				COMPARTMENT CONCENTRATIONS (LB/FT**3)	
	UF6	UO2F2	TOTAL U	HF	URANIUM	HF
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
120.0	0.000E+00	2.516E+02	1.944E+02	6.739E+01	2.287E-03	8.052E-04
240.0	0.000E+00	8.886E+02	6.867E+02	2.447E+02	3.772E-03	1.384E-03
360.0	0.000E+00	1.775E+03	1.372E+03	5.007E+02	4.729E-03	1.796E-03
480.0	1.014E+02	2.735E+03	2.182E+03	7.895E+02	5.369E-03	1.809E-03
600.0	3.692E+02	3.661E+03	3.079E+03	1.079E+03	5.812E-03	1.815E-03
720.0	7.477E+02	4.564E+03	4.033E+03	1.370E+03	6.087E-03	1.818E-03
840.0	1.119E+03	5.452E+03	4.970E+03	1.661E+03	5.047E-03	1.822E-03
960.0	1.157E+03	6.276E+03	5.633E+03	1.938E+03	3.328E-03	1.513E-03
1080.0	1.157E+03	6.840E+03	6.068E+03	2.146E+03	2.187E-03	1.098E-03
1200.0	1.157E+03	7.210E+03	6.355E+03	2.296E+03	1.438E-03	7.971E-04
1320.0	1.157E+03	7.454E+03	6.543E+03	2.405E+03	9.449E-04	5.786E-04
1440.0	1.157E+03	7.614E+03	6.667E+03	2.485E+03	6.210E-04	4.200E-04
1560.0	1.157E+03	7.788E+03	6.748E+03	2.542E+03	4.081E-04	3.048E-04
1680.0	1.157E+03	7.834E+03	6.836E+03	2.614E+03	1.763E-04	1.666E-04
1800.0	1.157E+03	7.864E+03	6.859E+03	2.636E+03	1.159E-04	1.166E-04
1920.0	1.157E+03	7.883E+03	6.875E+03	2.652E+03	7.615E-05	8.461E-05
2040.0	1.157E+03	7.896E+03	6.885E+03	2.664E+03	5.004E-05	6.141E-05
2280.0	1.157E+03	7.905E+03	6.891E+03	2.672E+03	3.289E-05	4.457E-05
2400.0	1.157E+03	7.910E+03	6.895E+03	2.679E+03	2.162E-05	3.235E-05
2520.0	1.157E+03	7.914E+03	6.898E+03	2.683E+03	1.421E-05	2.348E-05
2640.0	1.157E+03	7.916E+03	6.900E+03	2.686E+03	9.337E-06	1.705E-05
2760.0	1.157E+03	7.918E+03	6.901E+03	2.689E+03	6.136E-06	1.237E-05
2880.0	1.157E+03	7.919E+03	6.902E+03	2.690E+03	4.033E-06	8.980E-06
3000.0	1.157E+03	7.920E+03	6.903E+03	2.691E+03	2.651E-06	6.518E-06
3120.0	1.157E+03	7.920E+03	6.903E+03	2.692E+03	1.742E-06	4.731E-06
3240.0	1.157E+03	7.920E+03	6.903E+03	2.693E+03	1.145E-06	3.434E-06
3360.0	1.157E+03	7.921E+03	6.903E+03	2.693E+03	7.525E-07	2.493E-06
3480.0	1.157E+03	7.921E+03	6.904E+03	2.694E+03	4.945E-07	1.809E-06
3600.0	1.157E+03	7.921E+03	6.904E+03	2.694E+03	3.250E-07	1.313E-06

TITLE: EX. 5. REPEAT OF EX. 4.1 W/ RELEASE (EX. 2) SEGMENTED  
 DATA GENERATED BY F00RFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

INLET AIR BLOWER

FLOW RATE = 0.0 ACFM  
 AMBIENT TEMPERATURE = 80.000 DEG F  
 AMBIENT PRESSURE = 14.700 PSIA

TIME (SEC)	AIR V	H20 L	H20 V	COMPONENT MASS FLOW RATE (LB/SEC)						U02F2 S	TEMPERATURE (DEG F)	PRESSURE (PSIA)
				HF L	HF V	UF6 S	UF6 L	UF6 V	UF6 S			
0.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
120.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
240.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
360.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
480.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
600.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
720.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
840.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
960.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1080.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1200.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1320.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1440.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1560.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1680.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1800.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
1920.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2040.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2160.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2280.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2400.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2520.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2640.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2760.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
2880.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3000.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3120.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3240.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3360.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3480.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000
3600.0	9.603E+01	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	80.0000	14.7000

TITLE: EX. 5. REPEAT OF EX. 4.1 W/ RELEASE (EX. 2) SEGMENTED  
 DATA GENERATED BY FOOTRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

COMPARTMENT CONDITIONS

COMPARTMENT VOLUME = 500000. FT\*\*2  
 UVA PRODUCT = 7.903E+00 BTU/SEC-DEG F  
 SURFACE TEMPERATURE = 120.0 DEG F  
 COOLING RATE = 0.000E+00 BTU/SEC

TIME (SEC)	AIR V	H2O L	H2O V	H2O U	HF L	HF V	COMPONENT MASS (LB)	UF6 L	UF6 S	UF6 V	UF6 U	UF6 UO2F2 S	TEMPERATURE (DEG F)	TEMPERATURE PRESSURE (PSIA)
0.0	3.548E+04	0.000E+00	0.000E+00	4.630E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.7500
120.0	3.240E+04	0.000E+00	0.000E+00	8.779E+01	0.000E+00	7.443E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.738E+03	134.0015	14.7871
240.0	3.198E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.270E+02	0.000E+00	0.000E+00	0.000E+00	1.551E+03	3.213E+03	3.213E+03	135.9653	14.7603
360.0	3.227E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.355E+02	0.000E+00	0.000E+00	0.000E+00	3.217E+03	3.088E+03	3.088E+03	128.3547	14.7646
480.0	3.244E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.404E+02	0.000E+00	0.000E+00	0.000E+00	4.351E+03	3.004E+03	3.004E+03	123.7788	14.7667
600.0	3.254E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.433E+02	0.000E+00	0.000E+00	0.000E+00	5.130E+03	2.949E+03	2.949E+03	120.9825	14.7673
720.0	3.261E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.454E+02	0.000E+00	0.000E+00	0.000E+00	5.789E+03	2.915E+03	2.915E+03	118.8497	14.7690
840.0	3.245E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.406E+02	0.000E+00	0.000E+00	0.000E+00	4.062E+03	2.874E+03	2.874E+03	124.2249	14.7705
960.0	3.222E+04	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.339E+02	0.000E+00	0.000E+00	0.000E+00	1.589E+03	2.839E+03	2.839E+03	131.7506	14.7662
1080.0	3.217E+04	0.000E+00	0.000E+00	1.324E+01	0.000E+00	9.033E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.714E+03	2.714E+03	134.4666	14.7474
1200.0	3.327E+04	0.000E+00	0.000E+00	1.386E+02	0.000E+00	6.568E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.787E+03	1.787E+03	118.2330	14.7483
1320.0	3.401E+04	0.000E+00	0.000E+00	2.293E+02	0.000E+00	4.765E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.174E+03	1.174E+03	108.0553	14.7489
1440.0	3.450E+04	0.000E+00	0.000E+00	2.948E+02	0.000E+00	3.451E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.699E+02	7.699E+02	101.5999	14.7493
1560.0	3.482E+04	0.000E+00	0.000E+00	3.420E+02	0.000E+00	2.498E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.045E+02	5.045E+02	97.4747	14.7495
1680.0	3.504E+04	0.000E+00	0.000E+00	3.760E+02	0.000E+00	1.806E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.303E+02	3.303E+02	94.8434	14.7500
1800.0	3.518E+04	0.000E+00	0.000E+00	4.004E+02	0.000E+00	1.306E+02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.162E+02	2.162E+02	93.1303	14.7500
1920.0	3.528E+04	0.000E+00	0.000E+00	4.179E+02	0.000E+00	9.436E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.415E+02	1.415E+02	92.0248	14.7499
2040.0	3.534E+04	0.000E+00	0.000E+00	4.306E+02	0.000E+00	6.818E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.257E+01	9.257E+01	91.3101	14.7499
2160.0	3.539E+04	0.000E+00	0.000E+00	4.396E+02	0.000E+00	4.926E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.056E+01	6.056E+01	90.8509	14.7500
2280.0	3.541E+04	0.000E+00	0.000E+00	4.462E+02	0.000E+00	3.559E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.961E+01	3.961E+01	90.5526	14.7500
2400.0	3.543E+04	0.000E+00	0.000E+00	4.509E+02	0.000E+00	2.571E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.591E+01	2.591E+01	90.3666	14.7501
2520.0	3.545E+04	0.000E+00	0.000E+00	4.543E+02	0.000E+00	1.857E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.695E+01	1.695E+01	90.2413	14.7500
2640.0	3.546E+04	0.000E+00	0.000E+00	4.567E+02	0.000E+00	1.342E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.109E+01	1.109E+01	90.1598	14.7500
2760.0	3.546E+04	0.000E+00	0.000E+00	4.585E+02	0.000E+00	9.690E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.250E+00	7.250E+00	90.1064	14.7500
2880.0	3.547E+04	0.000E+00	0.000E+00	4.597E+02	0.000E+00	7.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.742E+00	4.742E+00	90.0666	14.7500
3000.0	3.547E+04	0.000E+00	0.000E+00	4.606E+02	0.000E+00	5.056E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.102E+00	3.102E+00	90.0404	14.7500
3120.0	3.547E+04	0.000E+00	0.000E+00	4.613E+02	0.000E+00	3.652E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.029E+00	2.029E+00	90.0272	14.7500
3240.0	3.547E+04	0.000E+00	0.000E+00	4.618E+02	0.000E+00	2.638E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.327E+00	1.327E+00	90.0272	14.7500
3360.0	3.547E+04	0.000E+00	0.000E+00	4.621E+02	0.000E+00	1.906E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.678E-01	8.678E-01	90.0142	14.7500
3480.0	3.547E+04	0.000E+00	0.000E+00	4.623E+02	0.000E+00	1.377E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.676E-01	5.676E-01	90.0142	14.7500
3600.0	3.547E+04	0.000E+00	0.000E+00	4.625E+02	0.000E+00	9.943E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.712E-01	3.712E-01	90.0142	14.7500



TITLE: EX. 5. REPEAT OF EX. 4.1 W/ RELEASE (EX. 2) SEGMENTED  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.

SOURCE TERM: UF6 LIQUID

INCRE- MENT	DURATION (SEC)	MASS (LB)	TEMPERATURE (DEG F)	PRESSURE (PSIA)	LIQUID
1	200.0	6709.0	189.600		LIQUID
2	200.0	6639.0	188.700		LIQUID
3	200.0	6538.0	187.300		LIQUID
4	140.0	4728.0	185.100		LIQUID
5	40.0	977.0	183.000		LIQUID
TOTAL	780.0	25591.0			

FLASH BASIS: ISENTHALPIC  
 UF6 MOLECULAR WEIGHT = 352.025

TIME (SEC)	COMPONENT MASS FLOW RATE (LB/SEC)						TEMPERATURE PRESSURE (PSIA)								
	AIR	V	H2O	L	HF	V	UF6	S	UF6	V	UF6	S	UF6	V	UF6
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.637E+01	0.000E+00	1.717E+01	0.000E+00	133.8915	14.7500		
120.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.637E+01	0.000E+00	1.717E+01	0.000E+00	133.8915	14.7500		
240.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.627E+01	0.000E+00	1.693E+01	0.000E+00	133.9108	14.7587		
360.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.627E+01	0.000E+00	1.693E+01	0.000E+00	133.9108	14.7587		
480.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.612E+01	0.000E+00	1.657E+01	0.000E+00	133.9257	14.7654		
600.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.682E+01	0.000E+00	1.695E+01	0.000E+00	133.9298	14.7673		
720.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.682E+01	0.000E+00	1.695E+01	0.000E+00	133.9298	14.7673		

TITLE: EX. 5. REPEAT OF EX. 4.1 W/ RELEASE (EX. 2) SEGMENTED  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 EXHAUST STREAM (FORCED DRAFT) RESISTANCE TERM = 3.798E-07 PSI-SEC\*\*2/LB/FT\*\*3

TIME (SEC)	AIR				COMPONENT MASS FLOW RATE (LB/SEC)				RESISTANCE TERM				TEMPERATURE			
	U	V	H20	L	H20	V	HF	L	HF	U	V	U02F2	S	(DEG F)	(PSIA)	
0.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	1.253E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	90.0000	14.7500	
120.0	1.157E+02	0.000E+00	0.000E+00	0.000E+00	3.135E-01	0.000E+00	2.638E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.776E+00	9.776E+00	134.0015	14.7871	
240.0	9.285E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.691E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.502E+00	9.329E+00	135.9653	14.7603	
360.0	9.473E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.746E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.443E+00	9.063E+00	128.3547	14.7646	
480.0	9.528E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.762E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.278E+01	8.824E+00	123.7788	14.7667	
600.0	9.501E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.754E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.498E+01	8.611E+00	120.9825	14.7673	
720.0	9.561E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.771E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.697E+01	8.545E+00	118.8497	14.7690	
840.0	9.848E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.855E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.233E+01	8.722E+00	124.2249	14.7705	
960.0	9.810E+01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.844E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.838E+00	8.644E+00	131.7506	14.7662	
1080.0	8.499E+01	0.000E+00	0.000E+00	0.000E+00	3.498E-02	0.000E+00	2.386E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.170E+00	7.170E+00	134.4666	14.7474	
1200.0	8.860E+01	0.000E+00	0.000E+00	0.000E+00	3.690E-01	0.000E+00	1.749E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.758E+00	4.758E+00	118.2330	14.7483	
1320.0	9.108E+01	0.000E+00	0.000E+00	0.000E+00	6.141E-01	0.000E+00	1.276E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.144E+00	3.144E+00	108.0553	14.7489	
1440.0	9.273E+01	0.000E+00	0.000E+00	0.000E+00	7.925E-01	0.000E+00	9.278E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.070E+00	2.070E+00	101.5999	14.7493	
1560.0	9.383E+01	0.000E+00	0.000E+00	0.000E+00	9.216E-01	0.000E+00	6.730E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.359E+00	1.359E+00	97.4747	14.7495	
1680.0	9.487E+01	0.000E+00	0.000E+00	0.000E+00	1.018E+00	0.000E+00	4.890E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.944E-01	8.944E-01	94.8434	14.7500	
1800.0	9.523E+01	0.000E+00	0.000E+00	0.000E+00	1.084E+00	0.000E+00	3.534E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.853E-01	5.853E-01	93.1303	14.7500	
1920.0	9.542E+01	0.000E+00	0.000E+00	0.000E+00	1.130E+00	0.000E+00	2.552E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.827E-01	3.827E-01	92.0248	14.7499	
2040.0	9.562E+01	0.000E+00	0.000E+00	0.000E+00	1.165E+00	0.000E+00	1.845E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.504E-01	2.504E-01	91.3101	14.7499	
2160.0	9.578E+01	0.000E+00	0.000E+00	0.000E+00	1.190E+00	0.000E+00	1.333E-01	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.639E-01	1.639E-01	90.8509	14.7500	
2280.0	9.588E+01	0.000E+00	0.000E+00	0.000E+00	1.208E+00	0.000E+00	9.635E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.072E-01	1.072E-01	90.5526	14.7500	
2400.0	9.595E+01	0.000E+00	0.000E+00	0.000E+00	1.221E+00	0.000E+00	6.963E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.018E-02	7.018E-02	90.3666	14.7501	
2520.0	9.599E+01	0.000E+00	0.000E+00	0.000E+00	1.230E+00	0.000E+00	5.029E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.590E-02	4.590E-02	90.2413	14.7500	
2640.0	9.600E+01	0.000E+00	0.000E+00	0.000E+00	1.237E+00	0.000E+00	3.632E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.001E-02	3.001E-02	90.1598	14.7500	
2760.0	9.601E+01	0.000E+00	0.000E+00	0.000E+00	1.241E+00	0.000E+00	2.624E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.963E-02	1.963E-02	90.1064	14.7500	
2880.0	9.601E+01	0.000E+00	0.000E+00	0.000E+00	1.245E+00	0.000E+00	1.895E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.284E-02	1.284E-02	90.0666	14.7500	
3000.0	9.602E+01	0.000E+00	0.000E+00	0.000E+00	1.247E+00	0.000E+00	1.369E-02	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.396E-03	8.396E-03	90.0404	14.7500	
3120.0	9.602E+01	0.000E+00	0.000E+00	0.000E+00	1.249E+00	0.000E+00	9.887E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.492E-03	5.492E-03	90.0272	14.7500	
3240.0	9.602E+01	0.000E+00	0.000E+00	0.000E+00	1.250E+00	0.000E+00	7.142E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.592E-03	3.592E-03	90.0272	14.7500	
3360.0	9.602E+01	0.000E+00	0.000E+00	0.000E+00	1.251E+00	0.000E+00	5.159E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.349E-03	2.349E-03	90.0142	14.7500	
3480.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	1.252E+00	0.000E+00	3.726E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.536E-03	1.536E-03	90.0142	14.7500	
3600.0	9.603E+01	0.000E+00	0.000E+00	0.000E+00	1.252E+00	0.000E+00	2.632E-03	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.005E-03	1.005E-03	90.0142	14.7500	





TITLE: EX. 5. REPEAT OF EX. 4.1 W/ RELEASE (EX. 2) SEGMENTED  
 DATA GENERATED BY FODRFT -- A FORCED DRAFT VENTILATION SYSTEM TRANSIENT COMPARTMENT MODEL.  
 URANIUM AND HF RELEASE SUMMARY AND COMPARTMENT CONCENTRATIONS

TIME (SEC)	CUMULATIVE MATERIAL RELEASED OR FORMED FROM RELEASED MATERIAL (LB)				COMPARTMENT CONCENTRATIONS (LB/FT**3)	
	UF6	UO2F2	TOTAL U	HF	URANIUM	HF
0.0	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
120.0	0.000E+00	6.384E+02	4.933E+02	1.709E+02	4.231E-03	1.489E-03
240.0	1.913E+02	1.832E+03	1.545E+03	5.041E+02	7.063E-03	1.854E-03
360.0	1.039E+03	2.931E+03	2.968E+03	8.296E+02	9.123E-03	1.871E-03
480.0	2.379E+03	3.999E+03	4.699E+03	1.159E+03	1.053E-02	1.881E-03
600.0	4.053E+03	5.045E+03	6.639E+03	1.490E+03	1.150E-02	1.887E-03
720.0	5.978E+03	6.075E+03	8.737E+03	1.822E+03	1.233E-02	1.891E-03
840.0	7.887E+03	7.115E+03	1.083E+04	2.161E+03	9.936E-03	1.881E-03
960.0	8.892E+03	8.153E+03	1.231E+04	2.501E+03	6.536E-03	1.868E-03
1080.0	9.142E+03	9.169E+03	1.327E+04	2.836E+03	4.195E-03	1.807E-03
1200.0	9.142E+03	9.876E+03	1.381E+04	3.083E+03	2.762E-03	1.314E-03
1320.0	9.142E+03	1.034E+04	1.418E+04	3.263E+03	1.814E-03	9.529E-04
1440.0	9.142E+03	1.065E+04	1.441E+04	3.394E+03	1.190E-03	6.903E-04
1560.0	9.142E+03	1.086E+04	1.457E+04	3.490E+03	7.797E-04	4.995E-04
1680.0	9.142E+03	1.099E+04	1.467E+04	3.559E+03	5.106E-04	3.612E-04
1800.0	9.142E+03	1.108E+04	1.474E+04	3.609E+03	3.342E-04	2.611E-04
1920.0	9.142E+03	1.113E+04	1.479E+04	3.645E+03	2.187E-04	1.887E-04
2040.0	9.142E+03	1.117E+04	1.482E+04	3.671E+03	1.431E-04	1.364E-04
2160.0	9.142E+03	1.120E+04	1.483E+04	3.690E+03	9.360E-05	9.852E-05
2280.0	9.142E+03	1.121E+04	1.485E+04	3.704E+03	6.122E-05	7.118E-05
2400.0	9.142E+03	1.122E+04	1.486E+04	3.714E+03	4.005E-05	5.142E-05
2520.0	9.142E+03	1.123E+04	1.486E+04	3.721E+03	2.619E-05	3.714E-05
2640.0	9.142E+03	1.123E+04	1.486E+04	3.726E+03	1.713E-05	2.683E-05
2760.0	9.142E+03	1.124E+04	1.487E+04	3.730E+03	1.121E-05	1.938E-05
2880.0	9.142E+03	1.124E+04	1.487E+04	3.733E+03	7.329E-06	1.400E-05
3000.0	9.142E+03	1.124E+04	1.487E+04	3.735E+03	4.794E-06	1.011E-05
3120.0	9.142E+03	1.124E+04	1.487E+04	3.736E+03	3.135E-06	7.305E-06
3240.0	9.142E+03	1.124E+04	1.487E+04	3.737E+03	2.051E-06	5.276E-06
3360.0	9.142E+03	1.124E+04	1.487E+04	3.738E+03	1.341E-06	3.811E-06
3480.0	9.142E+03	1.124E+04	1.487E+04	3.738E+03	8.772E-07	2.753E-06
3600.0	9.142E+03	1.124E+04	1.487E+04	3.739E+03	5.737E-07	1.989E-06

